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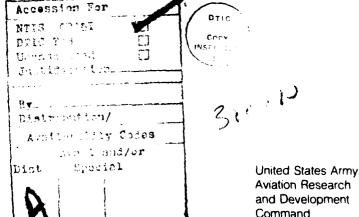


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### PERFORMANCE AND LOADS DATA FROM A WIND TUNNEL TEST OF A FULL-SCALE, COAXIAL, HINGELESS ROTOR HELICOPTER

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### SUMMARY

A test of a full-scale XH-59A Advancing Blade Concept Helicopter was conducted in Ames Research Center's 40- by 80-Foot Wind Tunnel. The helicopter was tested with the rotor on and off, rotor hub fairings on and off, interrotor shaft fairing on and off, rotor instrumentation module on and off, and auxiliary propulsion thrust on and off. The investigation was accomplished over an advance ratio range of 0.25 to 0.45 with the rotor on and from 60 to 180 knots with the rotor off. This report presents data on aerodynamic forces and moments, rotor loads, rotor control positions and vibration for the XH-59A as well as the aerodynamic performance of the isolated rotor.

### List of Symbols

a	speed of sound, ft/sec
A <sub>1</sub>	longitudinal cyclic blade pitch, deq
ь	total number of rotor blades
B <sub>1</sub>	lateral cyclic blade pitch, deg
c.75	blade chord at 75% radius, ft
C <sub>DR/σ</sub>	rotor drag coefficient, rotor drag/ $_{\rho}S(\Omega R)^2$
C <sub>LR/σ</sub>	rotor lift coefficient, rotor lift/ $\rho S(\Omega R)^2$
C <sub>MX</sub> / <sub>σ</sub>	rotor rolling moment coefficient, rotor rolling
	$moment/\rho S(\Omega R)^2R$
C <sub>MY</sub> / <sub>o</sub>	rotor pitching moment coefficient, rotor pitching
	$moment/\rho S(\Omega R)^2R$
C <sub>MZ</sub> / <sub>o</sub>	rotor yawing moment coefficient, rotor yawing
	$moment/\rho S(\Omega R)^2 R$
C <sub>p/o</sub>	rotor power coefficient, total turboshaft
	engine power/ $\rho$ S( $\Omega$ R) $^3$
C <sub>po/σ</sub>	rotor nonideal power coefficient
CYR/o	rotor side force coefficient, rotor side force/ ${}_{\rho}S(\Omega R)^2$
	drag, 1b
L	lift, 1b
R	rolling moment, ft-1b
M	pitching moment, ft-lb
<sup>M</sup> at	advancing tip Mach number, $M_{at} = M_{tun} + M_{tip}$
Mtip	rotor tip rotational Mach number, $\Omega R/a$
M <sub>tun</sub>	free stream Mach number, M <sub>tun</sub> = V/a
N	yawing moment, ft-1b
q	free stream dynamic pressure, $\rho V^2/2$ , $1b/ft^2$

### List of Symbols (continued)

r	local blade radius, ft
R	rotor radius, ft
S	rotor reference area, S = bc.75R
V	free stream velocity, ft/sec
Υ	side force, lb
α	angle of attack, deg
α <sub>5</sub>	shaft angle of attack, deg
μ	rotor advance ratio, $V/\Omega R$
Ω	rotor rotational speed, rad/sec
ψ	blade azimuth, deg, counter-clockwise is positive as
	viewed from above, zero with instrumented blade pointing aft
ρ	air density, slugs/ft <sup>3</sup>
σ	rotor solidity, $\sigma = b c.75/\pi R$
θ	rotor blade pitch, deg

### Subscripts

u	upper rotor
£.	lower rotor
( )'	prime, differential between upper and lower rotors

### INTRODUCTION

The high-speed capability of modern helicopters can be limited by the rapid increase in rotor power requirements that accompanies retreating blade stall and advancing blade compressibility drag. In order to reduce the compressibility drag the rotor's rotational speed must be reduced, but this only aggravates the problem of retreating blade stall.

One solution to this dilemma is to use two counter-rotating rotors with each lifting predominantly on its advancing side. Since the retreating side of each rotor is unloaded, blade stall is less of a problem and the rotor's rotational speed can be reduced, which helps alleviate compressibility drag as well. Two XH-59A Demonstration/Research Helicopters were built by Sikorsky Aircraft under Army Sponsorship using this Advancing Blade Concept (ABC). A three-view drawing of the helicopter as modified for wind tunnel testing is presented as figure 1. Readers who desire additional information on the ABC concept are referred to references 1-6.

One disadvantage of this configuration is the large parasite drag of the rotor hubs and inter-rotor shaft. The hub drag is proportional to the hub's swept frontal area (reference 7) and the ABC, with two hubs instead of one, has twice the hub swept frontal area of a conventional helicopter of similar (hingeless) construction. In addition to this is the drag due to the inter-rotor shaft. In an effort to reduce the hub's parasite drag a 1/5-scale model wind tunnel test was conducted to identify the drag reduction potential of fairing the rotor hubs and inter-rotor shaft of the XH-59A (reference 8). Many fairing configurations were tested and one was selected for full-scale wind tunnel testing.

This report presents the results of a full-scale wind tunnel test of an XH-59A helicopter conducted in Ames Research Center's 40- by 80-Foot Wind Tunnel. The objectives of the test were to (1) provide advanced technology data necessary for assessment of a potentially viable mission-oriented ABC vehicle, including hub drag reduction and rotor/tail/propulsion system interference alleviation, and (2) provide data with which to interpret, clarify, and augment flight test results as well as provide a base for correlation of existing 1/5-scale model test data. The test was conducted over an advance ratio range of 0.25 to 0.45 with the rotor on and from 60 to 180 knots with the rotor off. Data is presented for aerodynamic forces and moments, rotor control positions, rotor structural loads, and vibration of the XH-59A as well as the aerodynamic performance of the isolated rotor.

### EXPERIMENTAL EQUIPMENT AND PROCEDURES

### Description of Wind Tunnel and Balance

The 40- by 80-Foot Wind Tunnel is of the closed-throat, single-return type with a speed capability extending to 180 knots. Model forces and moments were measured by a six-component mechanical balance. Balance sensitivities were as follows:

Scale	Sensitivity
Lift*, 1b	5
Drag, 1b	1
Side Force*, 1b	1
Pitching Moment, ft-1b	160
Rolling Moment, ft-1b	85
Yawing Moment, ft-1b	24

<sup>\*</sup>two balances used to measure total force

### Description of Model

General - Several photographs of the ABC installed in the wind tunnel test section are presented as figure 2. Note the fairings installed over the rotor hubs and inter-rotor shaft in figures 2(a) and 2(b). The helicopter was modified by the addition of two struts and fairings in place of the main landing gear so that it could be mounted on the wind tunnel's strut model support system. Figure 2(f) presents a close-up view of the model support struts. The helicopter's pitch attitude (rotor shaft angle of attack) was remotely controlled using an extendable nose strut. The three struts which support the model on the wind tunnel balance were faired to minimize the extraneous airloads applied to the balance. The midpoint between the two rotors was 5 feet above the tunnel centerline. Power for the rotors was supplied by two PT6T-3 turboshaft engines producing a total of 1500 HP. The nacelle-mounted engines for auxiliary propulsion were J60-P3A turbojets which produce 3000 lbs. of thrust each. General specifications of the XH-59A are presented in Table 1.

Six rotor controls were remotely operated from the control room by electromechanical actuators. The six rotor controls were collective, lateral cyclic, and longitudinal cyclic for each rotor. The relationships between these controls and the rotor blade pitch were as follows:

Collective:  $\theta_0 = \frac{\theta_{0u} + \theta_{0l}}{2}$ Longitudinal Cyclic:  $A_1 = \frac{A_{1u} + A_{1l}}{2}$ Lateral Cyclic:  $B_1 = B_{1u} + B_{1l}$ 

$$\theta_0' = \theta_{0u} - \theta_{0l}$$

$$A_1' = A_{1u} \sim A_{1\ell}$$

$$B_1' = B_{1u} - B_{1\ell}$$

Therefore the blade pitch on the upper rotor was:

$$\theta_U = (\theta_0 + \theta_0') - (A_1 + A_1') \cos \psi_U - (B_1 + B_1') \sin \psi_U$$
 blade pitch on the lower rotor was:

$$\theta_{\ell} = (\theta_0 - \theta_0) - (A_1 - A_1') \cos \Psi_{\ell} - (B_1 - B_1') \sin \Psi_{\ell}$$

Rotor Blades - The XH-59A used three 18-foot radius rotor blades on each rotor. The upper rotor rotated in the counter-clockwise direction, and the lower rotor rotated in the clockwise direction. The upper and lower rotors were indexed such that when the instrumented blade of the upper rotor was at  $\psi = 0^{\circ}$ , the instrumented blade of the lower rotor was at  $\psi = 300^{\circ}$ . The rotor blades were attached to the hubs without flap or lead-lag hinges, using only pitch bearings. The blades were attached with 3° of precone and 1.4° of prelag. The blades were tapered in both planform and thickness. The planform taper was linear with a rotor chord to tip chord ratio of 2:1. A drawing of the blade in plan view is presented as figure 3. The spanwise variation of blade thickness to chord ratio is presented as figure 4. The airfoil contour at 20% radius was a NACA 63(230)224A airfoil tapering in thickness to a NACA 63(230)-213A airfoil at 62% radius. This transitioned to a NACA 23012(64) airfoil at 72% radius which was held constant to the tip (fig. 3). The blades had -10° of nonlinear twist. The twist distribution is presented as figure 5. The

primary structural element in the blades was a full span titanium spar with boron composite reinforcement bonded to the upper and lower surfaces of the spar to increase the flapwise stiffness. A honeycomb core covered with a fiberglass skin was attached to the spar to give the blades their aerodynamic shape. Figure 6 presents a drawing of a typical blade section. The blade's natural frequency diagram is presented as figure 7. The spanwise distribution of rotor blade properties are given in Table 2.

### Description of Hub Fairings

Figure 8 presents a sketch of the rotor hub fairings that were tested. The upper and lower rotor hub fairings were 31.8% thick ellipsoids. These fairings had a diameter of 4.17 feet. The inter-rotor shaft fairing was a 43% thick NACA 4-digit series symmetric airfoil. The inter-rotor shaft fairing was mounted to the upper and lower rotor hubs with bearings and was free to rotate about the rotor centerline. It was expected that the fairing would, therefore, rotate to a trailing edge aft orientation, aligned with the free stream. However, it was noted during the wind tunnel test that the fairing did not align itself with the wind and was skewed about 30° relative to the free stream either to the left or to the right. This failure to align itself was evident when testing both with the hubs rotating and the hubs not rotating when testing with the rotor blades off. The skew also continued when testing with the rotor blades on. In an effort to eliminate the skew of the inter-rotor shaft fairing, an extended trailing edge tab was attached to the fairing (see fig. 8). However, the skew continued in spite of the extended trailing edge tab.

An aerodynamic configuration which is free to pivot about a point aft of its aerodynamic center is inherently unstable about its pivot. The pivot of the inter-rotor shaft fairing was at the 30% chord location. It is to be

expected that the inter-rotor shaft fairing would not line up with the wind if its aerodynamic center is forward of 30% of chord. It was reported in reference 9 that a NACA 0035 airfoil had an aerodynamic center located 16% of chord aft of the leading edge. Although the inter-rotor shaft fairing's airfoil section was a slightly thicker NACA 0043, ref. 9 indicates that the trend is for the aerodynamic center to move forward with increasing thickness. Thus, the available evidence indicates that the aerodynamic center of the inter-rotor shaft fairing was at least as far forward as 16% of chord aft of the leading edge. The failure of the inter-rotor shaft fairing to properly align itself with the free stream was, therefore, a result of the aerodynamic center being forward of the pivot point. The extended trailing edge tab had little effect on the orientation of the inter-rotor shaft fairing. The reason was that the trailing edge tab was not long enough to move the aerodynamic center aft of the pivot point.

Figure 9 presents a sketch of the unfaired rotor hub with the rotor blades off and also shows the instrumentation can. The instrumentation can housed signal conditioning equipment and slip rings used for acquiring data in the rotating frame of reference.

### Instrumentation and Data Reduction

Wind tunnel wall corrections have been applied to the forces and moments measured by the wind tunnel balance. This wall correction is based on conventional fixed wing techniques, for a wing of span equal to the rotor diameter (reference 10). The wall correction was an incremental change in the angle of

attack that was proportional to the lift:

$$\Delta \alpha = 0.00235 \, \frac{L}{q}$$

where the constant, 0.00235 deg/ft<sup>2</sup>, was determined based on rotor and wind tunnel geometric parameters. This incremental angle,  $\Delta\alpha$ , was added to the geometric angle of attack,  $\alpha_S$ , to obtain the corrected rotor disk angle of attack in free air,  $\alpha$ .

$$\alpha = \alpha_S + \Delta \alpha$$

Balance forces and moments were then resolved to this new wind-axis system.

Tare corrections were analytically determined to account for forces and moments produced by the exposed model support struts (references 11, 12). The exposed tips of the wind tunnel model support system struts were estimated to have a total parasite drag area of  $3.35 \, \text{ft}^2$ . The fairings around the model's support struts (extending from the tips of the wind tunnel model support system struts to the ABC's main landing gear wheel wells, see fig. 2(f)) were modelled as low aspect ratio wings (AR = 1.26). An explanation of the equations used to correct the measured forces and moments for the effects of the strut fairings is presented in Appendix I. The forces and moments produced by the J60 auxiliary propulsion engines have also been subtracted out of the data presented here. The thrust was calculated from a thrust versus exhaust pressure ratio calibration which was performed in an engine test cell before the wind tunnel test. An explanation of the equations used to correct for the thrust of the J60 engines is presented in Appendix II.

All aerodynamic forces and moments are presented in wind axes. The axis center for rotor forces and moments was on the centerline of the inter-rotor shaft halfway between the two rotors. In aircraft coordinates this position

would be:

Fuselage Station = 300

Water Line = 215

Butt Line = 0

All other aerodynamic forces and moments were resolved to the aircraft's center of gravity, whose location is shown on fig. 1. In aircraft coordinates, the center of gravity is located at:

Fuselage Station = 294.7

Water Line = 158

Butt Line = 0

Positive directions of forces and moments are shown in figure 10.

Engine torques were measured using pressure transducers plumbed to the engine torque pressure outputs. These torques were multiplied by the engine output shaft's rotational speed to obtain the power output. A nonideal power coefficient was computed as follows:

$$C_{po}/\sigma = C_p/\sigma - \sigma(C_{LR}/\sigma)^2/2\mu + \mu C_{DR}/\sigma$$

The parameter  $C_{po}$  is obtained by subtracting the propulsive or parasite power and the ideal induced power from  $C_p$ ; therefore, it is equal to the sum of the rotor profile power and nonideal induced power losses.

The aerodynamic forces and moments of the isolated rotor were obtained by subtracting the forces and moments due to the fuselage from the total measured.

The forces and moments due to the fuselage were determined from testing with the rotor blades off. This "tare" due to the fuselage was described by polynomial equations in  $\alpha$  and q after the forces and moments due to the J60 engines had been removed. These equations are given in Table 3. These tares were obtained with the instrumentation can installed on the inter-rotor shaft, no hub fairings, and the hubs rotating. However, several rotor-on runs were conducted with the hub fairings installed in place of the instrumentation can. The fuselage tares obtained with the instrumentation can were also used to calculate the rotor forces for these runs. Therefore, the effect of substituting the hub fairings for the instrumentation can is included in the rotor forces and moments since the fuselage aerodynamic tares used to calculate the rotor forces and moments were obtained with the instrumentation can installed.

The instrumentation parameters considered in this report are listed in Table 4, including units and positive directions. The actual radial locations of the blade bending gages are given in Table 5 and are shown on a drawing of the rotor blade in fig. 3. The signals from the parameters listed in Table 4 were sampled and digitized 64 times per revolution. The time history was smoothed and filtered by eliminating subharmonics and harmonics above 10/rev; and a correction for the Bessel filters in the amplifiers was applied.

Due to various problems encountered during the wind tunnel test, the mean values of the blade pitch data ( $\theta_0$  and  $\Delta\theta_0$ ) are not reliable from run to run. However, the increments of collective and differential collective pitch within a run are reliable.

### OPERATING CONDITIONS

The ABC's performance and loads data were acquired over an advance ratio range of 0.25 to 0.45 with the rotor on and from 60 to 180 knots with the rotor off. For the rotor-on runs, the rotor speed was adjusted to give the desired tip Mach number,  $M_{\mbox{tip}}$ , and the tunnel speed was adjusted to obtain the desired advance ratio,  $\mu$ . Data were then acquired for a matrix of shaft angles,  $\alpha_{\mbox{S}}$ , and rotor lift coefficients,  $C_{\mbox{LR/}\sigma}$ . The operating conditions at which the data were acquired are shown in figure 11.

Several hub fairing configurations were tested, and runs were conducted both with the rotor blades on and with the rotor blades off. Table 6 presents a key to the configuration that was tested in each run. Rotor-on testing was conducted over an angle of attack range of  $0^{\circ}$  to  $10^{\circ}$ . Rotor-off testing was conducted over an angle of attack range of  $-10^{\circ}$  to  $+10^{\circ}$  and a yaw angle range of  $-15^{\circ}$  to  $+14^{\circ}$ . The auxiliary propulsion engines were operated at flight idle for all runs except for run 10.

### **RESULTS**

### Performance Data

The performance data are tabulated in Section A. A dictionary of the parameters is provided in Table 7. The data are organized by run number.

### Control and Loads Data

The control and loads data are tabulated in Section B. The oscillatory (one-half peak-to-peak) and mean loads, the blade pitch control settings, and the one-half peak-to-peak accelerations are presented. A dictionary of the parameters is presented in Table 8. The data are organized by run number.

### Detailed Loads Data

Detailed loads data are given in Section C. The first 10 harmonics and the time history over one revolution are presented for the blade bending moments, pitch link loads, and upper rotor shaft stress. A dictionary of the parameters is provided in Tables 7 and 8. The pitch link load given in the detailed loads presentation is that of the red, instrumented blade. As previously noted, when the instrumented blade of the upper rotor was at  $\psi = 0^{\circ}$ , the instrumented blade of the lower rotor was at  $\psi = 300^{\circ}$ .

### Plotted Data

Selected performance and loads data are plotted in Section D. A dictionary of the parameters is provided in Tables 7 and 8. Fuselage aerodynamic characteristics, rotor performance, rotor loads, and airframe vibration plots are presented. The data points are designated by circles on the plots. The majority of the plots present isograms for a particular quantity as a function of rotor lift and rotor drag, at a given advance ratio. The contours are interpolated from the values of the quanity at the data points. The parameter  $\varepsilon_V$  in the upper left-hand corner of the plots is the rms error of the estimate of the quantity at the data points based on the interpolated contours.

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# TABLE 1. XH-59A GENERAL SPECIFICATIONS

Aircraft Length (rotor turning)	41.7	£
Fuselage Length	40.8	<b>:</b> ;
Rotor Radius, R	18.0	Į.
Number of Rotors	2	
Blades per Rotor	es .	
Rotor Separation	2.5	£
Blade Tip Chord	0.938	£
Blade Taper Ratio	2:1	
Blade Twist (nonlinear)	-10	deg
Total Rotor Solidity, σ	0.1267	
Rotor Reference Area, S	128.965	ft2
Blade Precone Angle	က	qeg
Blade Prelag Angle	1.4	deg
Shaft Tilt	0	qeg
Design Rotor Tip Speed	920	ft/sec
Rotor Drive System Power	1500	윺
Tail Surface Area - Horizontal	09	ft2
- Vertical	30	ft <sup>2</sup>
Horizontal Tail Incidence	-5	deg
Power Plants - Lift	(2) PT6T-3	16T-3
- Thrust	(2) J60-P3A	50-P3A

TABLE 2. SPANWISE DISTRIBUTION OF ROTOR BLADE PROPERTIES

7/R	Weight, 1b/ft	r/R	Flapwise Stiffness EIf, 1b-ft × 10 <sup>-3</sup>	r/R	Chordwise Stiffness EIc, 1b-ft x 10
•	0.	0.	5,970	0.	5,970
0.030	116.40	0.092	5,790	0.092	5,970
0.092	116.40	0.144	3,330	0.115	4,380
0.092	26.40	0.202	1,940	0.173	3,190
0.115	21.60	0.259	1,361	0.288	2,290
0.173	16.80	0.345	875	0.403	1,750
0.288	11.40	0.403	299	0.518	1,472
0.403	8.16	0.518	361	0.691	1,000
0.576	5.04	0.634	194	0.864	556
0.737	3.36	0.748	111	1.0	389
0.737	5.04	1.0	99		
0.939	3.84				
0.939	12.24				
0.973	12.23				
0.973	14.88				
1.0	14.88				

TABLE 2. CONTINUED

7/R	Torsional Stiffness GJ, 16-fi x 10-3	r/R	Torsional Inertia, I, 1b-ft <sup>2</sup> /ft
o.	4,785	0.	1.458
0.093	4,785	0.116	1,458
0.125	3,993	0.116	1.225
0.174	2,326	0.139	1.225
0.231	1,528	0.139	1.033
0.289	1,111	0.162	1.033
0.347	778	0.162	1.175
0.405	507	0.23	1.125
0.463	330	0.40	0.650
0.521	208	09.0	0.375
0.579	134	0.944	0.151
0.694	29	0.979	0.151
0.810	35	0.979	0.136
0.926	22	1.0	0.136
1.0	21		

TABLE 3. EQUATIONS FOR FUSELAGE AERODYNAMIC TARES

For q < 50 1b/ft<sup>2</sup>

~-	8	a2	ဗီ	0	q <sup>2</sup>	i I		8	g <sub>2</sub>	g <sub>3</sub>	0	q <sup>2</sup>
0.00638	-0.00057	-0.06653	-0.00160	0.01217	0.05991	l	0.00079	-0.00005	-0.01700	-0.00030	-0.00336	0.00714
-0.59206	-0.01789	4,74413	0.11532	-0.38280	-3.43062		0.07984	-0.00328	2,66738	0.03859	0.39236	-1.11131
0.00095	0.00168	-0.04500	0.00054	-0.00470	0,00422		0.00221	-0.00166	-0.00494	0.00075	-0.00512	0.00356
0,0000	0.05235	0.26388	-0.00874	-0.03260	-0.14750		0.01511	0.05188	-0.08872	-0.00645	0.01682	0.04250
5.41970	0.03287	-38.59377	-0,08140	1,57295	0.06086		5.17748	0.00113	-42.96387	-0.13112	1.00925	-0.16395
10.76035	23.46913	-130.64588	-1.40292	-2.68051	61.30223	> 50 1b/ft <sup>2</sup>	-6.72088	21.57190	-124.43791	-0.64084	-13.78191	47.21218
		"				For q >			N			
حاد ٰ	010	ΣÍσ	>10	<b>≥</b>  0	<b>≈</b> 10	Fo	, ~10 I	مام	<b>E</b>  U	<b>≻</b>  0	<b>≥</b>  0	210

TABLE 4. LIST OF INSTRUMENTATION PARAMETERS

Parameter		Units	Positive Direction
Upper rotor chordwise	chordwise bending moment, .1R	ft-1b	tip aft
Upper rotor	nding moment,	ft-lb	tip up
•	. 2R	ft-lb	tip up
	. 3R	ft-lb	tip up
	. 6R	ft-1b	tip up
Upper rotor	rotor red blade pitch link load*	92	, leading edge
	yellow blade pitch link load	- P	tension, leading edge up
	rotor blue blade pitch link load	اً وا	leading edge
	shaft stress	l lb/in <sup>2</sup>	tension
	rotor blade root pitch	ded	leading edge up
	rotor chordwise bending moment, .1R	ft-1b	
Lower rotor		ft-1b	tip up
	. 2R	ft-1b	tip up
	. 3R	ft-1b	tip up
	.6R	ft-lb	
Lower rotor	red blade pitch link load*	92	
Lower rotor	Lower rotor yellow blade pitch link load	df.	leading
Lower rotor blue blade	blue blade pitch link load	ط و	tension, leading edge up
Lower rotor blade root	blade root pitch	deg	dn abp
#1 PT6 torque	ue	ft-lb	power to rotor
#2 PT6 torque	ue	ft-1b	power to rotor
Gearbox vertical accel	tical acceleration	5,6	
Gearbox lateral accel	eral acceleration	s,6	
Gearbox lon	Gearbox longitudinal acceleration	s, 6	
Left vertic	al fin vertical acceleration	9,6	
Horizontal	Horizontal stabilizer vertical acceleration	s,6	
Left aft su	Left aft support strut lateral acceleration	s,6	
#1 J60 vert	ical acceleration	s 6	
#Z JbU vertical	icai acceleration	s.6	

\*the red blade was the instrumented blade for both rotors.

TABLE 5. BLADE BENDING GAGE LOCATIONS

r/R	0,1026 0,1991 0,3009 0,6019
NOMINAL STATION	. 1R . 2R . 3R

TABLE 6. CONFIGURATION KEY

RUNS	HUB FAIRING	INTER-ROTOR SHAFT FAIRING	INSTRUMENTATION CAN
Rotor Blades off			
10,12	uo	uo	off
13	uo	off	off
15	off	off	off
17,18	off	off	uo
Rotor Blades			
21,23,24,25	off	off	uo
28,29,30	uo	uo	off

# TABLE 7. PERFORMANCE DATA PARAMETERS

LABEL	PARAMETER
ALFS,C	angle of attack in free air, $lpha$ , deg
ALFS,U	shaft angle of attack, $\alpha_{\!\scriptscriptstyle S}$ , deg
ANXL/R	inclination of thrust vector from vertical,
	positive forward, deg
BAR	atmospheric barometric pressure, in Hg
CDR/S,R	rotor drag coefficient, ${\sf CDR}/\sigma$
CLR/S,R	rotor lift coefficient, $CLR/\sigma$
CMX/S,R	rotor rolling moment coefficient, $C_{MX/\sigma}$
CMY/S,R	rotor pitching moment coefficient, $CMY/\sigma$
CMZ/S,R	rotor yawing moment coefficient, $CMZ/\sigma$
CP/S	rotor power coefficient, $Cp/\sigma$
CP0/S	rotor nonideal power coefficient, $Cp_0/\sigma$
CYR/S,R	rotor side force coefficient, $CYR/\sigma$
DRAG	aircraft drag, lb
DRAG/Q	aircraft drag/q, ft <sup>2</sup>
DRAG,R	rotor drag, 1b
E3	upper rotor hub fairing
E4	lower rotor hub fairing
10	instrumentation can

## TABLE 7. CONTINUED

PARAMETER

total power output of PT6 engines, horsepower	total thrust of J60 auxiliary propulsion engines, lb	effective aircraft lift/drag, including equivalent	drag of PT6 power. L/DE $\approx$ lift/(drag +(550xHP/V))	effective rotor lift/drag, including equivalent drag	of PT6 power. L/D,R $\approx$ rotor lift/(rotor drag + (550xHp/V))	aircraft lift, 1b	aircraft lift/q, ft <sup>2</sup>	rotor lift, 1b	advancing tip Mach number, Mat	free stream Mach number, Mtun	rotor tip speed, ΩR	aircraft pitching moment, M, ft-1b	aircraft pitching moment/q, ft $^3$	rotor pitching moment, ft-1b	aircraft yaw angle	free stream dynamic pressure, q, lb/ft <sup>2</sup>	free stream density multiplied by 100, slugs/ft $^3$
4	,1 THRUST	1 /DF	10/1	1 /D.R		LIFT	L1FT/0	LIFT,R	MAT	MTUN	OMEG*R	РІТСН	PITCH/Q	PITCH,R	PSI	QPSF	RH0100

## TABLE 7. CONTINUED

PARAMETER

ROLL	aircraft rolling moment, £, ft-lb
ROLL/Q	aircraft rolling moment/q, ft $^3$
ROLL,R	rotor rolling moment, ft-lb
RPM	rotor rotational speed, rev/min
RPM,%	rotor rational speed expressed as percent
	of nominal value, RPM/343.6
54	inter-rotor shaft fairing
SIDE	aircraft side force, Y, lb
SIDE/Q	aircraft side force/q, ft $^3$
SIDE,R	rotor side force, lb
TEMP	free stream temperature, deg farenheit
TIPM	rotor rotational Mach number, M <sub>tip</sub>
TORQ	total rotor shaft torque, except for transmission
	losses, TORQ = HP x550/ $\Omega$ , ft-lb
VKTS	free stream velocity, knots
V/0R	rotor advance ratio, u
YAW	aircraft yawing moment, N, ft-lb
YAW/Q	aircraft yawing moment/q, ft $^3$
YAW,R	rotor yawing moment, ft-lb

TABLE 8. CONTROL AND LOADS DATA PARAMETERS

LABEL	PARAMETER
АГРН	angle of attack in free air, α, deg
A1	mean cosine component of blade pitch, $\mathtt{A_{l}}$ , deg
AlP	differential cosine component of blade pitch, $A_1^{\ \ }$ , deg
81	mean sine component of blade pitch, $\mathtt{B}_\mathtt{l}$ , deg
81P	differential sine component of blade pitch $\mathtt{B}_1$ ', deq
500	cosine component of fourier series
GB LNAC	gearbox longitudinal acceleration, one-half peak-to-peak, g's
GB LTAC	gearbox lateral acceleration, one-half peak-to-peak, g's
GB VTAC	gearbox vertical acceleration, one-half peak-to-peak, g's
HARMONIC	harmonic number of fourier series
HST VTAC	horizontal stabilizer vertical acceleration, one-half peak-
	to-peak, g's
LAS LTAC	left aft support strut lateral acceleration, one-half peak-
	to-peak, g's
LRCB	lower rotor chordwise bending, ft-lb
LRN1	lower rotor normal bending .1R, ft-lb
LRN2	lower rotor normal bending .2R, ft-1b
LRN3	lower rotor normal bending .3R, ft-lb

## TABLE 8. CONTINUED

PARAMETER

lower rotor normal bending .6R, ft-lb	lower rotor green blade pitch link load, lb	lower rotor red blade pitch link load, lb	lower rotor yellow blade pitch link load, lb	left vertical fin vertical acceleration, one-half	peak-to-peak, g's	mean load	one-half peak-to-peak oscillatory load	blade azimuth angle, ↓, deg	sine component of fourier series	mean blade root pitch, $\theta_0$ , deg	differential collective, $\theta_0$ ', deg	upper rotor chordwise bending, ft-1b	upper rotor normal bending .1R, ft-lb	upper rotor normal bending .2R, ft-lb	upper rotor normal bending .3R, ft-lb	upper rotor normal bending .6R, ft-lb
LRN6	LRGPL	LRRPL	LRYPL	LVF VTAC		¥	08	PSI	NIS	THETA	THETAP	URCB	URN1	URN2	URN3	URN6

TABLE 8. CONTINUED

PARAMETER

upper rotor blue blade pitch link load, lb	upper rotor red blade pitch link load, lb	upper rotor yellow blade pitch link load, lb	upper rotor shaft bending stress, $1b/in^2$	free stream velocity, knots	rotor advance ratio, μ	#1 J60 vertical acceleration, one-half peak-to-peak, g's	#2 J60 vertical acceleration, one-half peak-to-peak, g's	#1 PT6 engine output torque before reduction gearing, ft-lb	#2 PT6 engine output torque before reduction gearing. ft-lb
URBPL	URRPL	URYPL	URSB	VKTS	V/0R	#1J VTAC	#23 VTAC	#10	#20

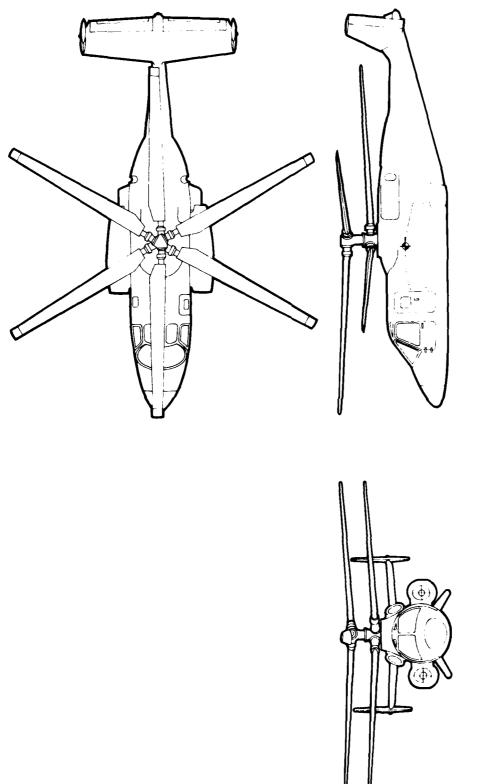


Figure 1. 3—VIEW DRAWING OF ABC

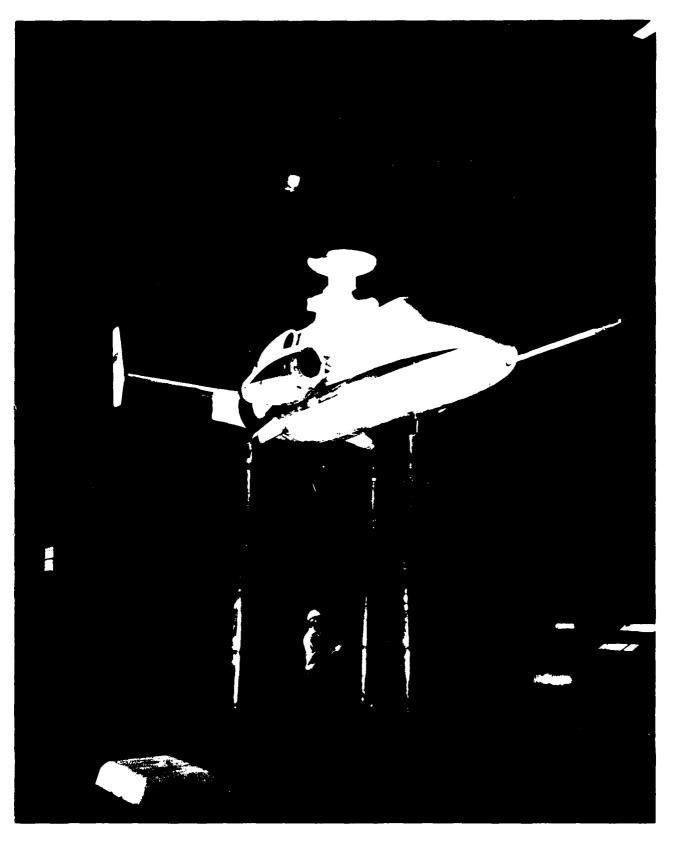


Figure 2(a). Front View of ABC with Hub Fairings Installed

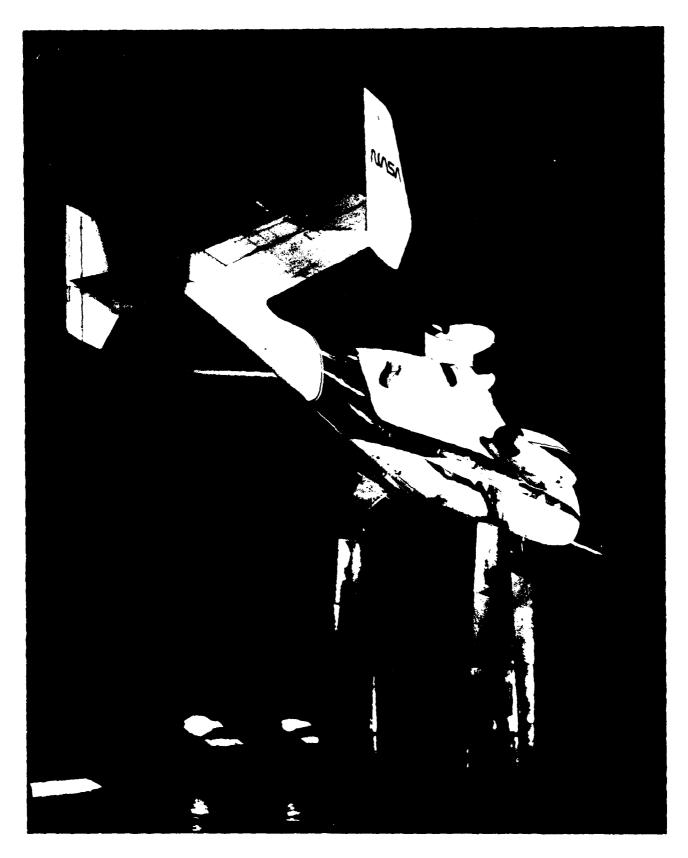


Figure 2(b). Rear View of ABC with Hub Fairings Installed 32



Figure 2(c). Front View of ABC with Instrumentation Can Installed



Figure 2(d). Side View of ABC with No Hub Fairings Installed



Figure 2(e), Close-up View of Rotor Hubs



Figure 2(f). Close-up View of Model Support Struts

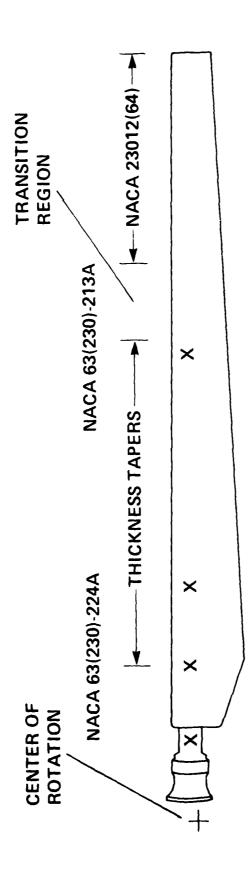
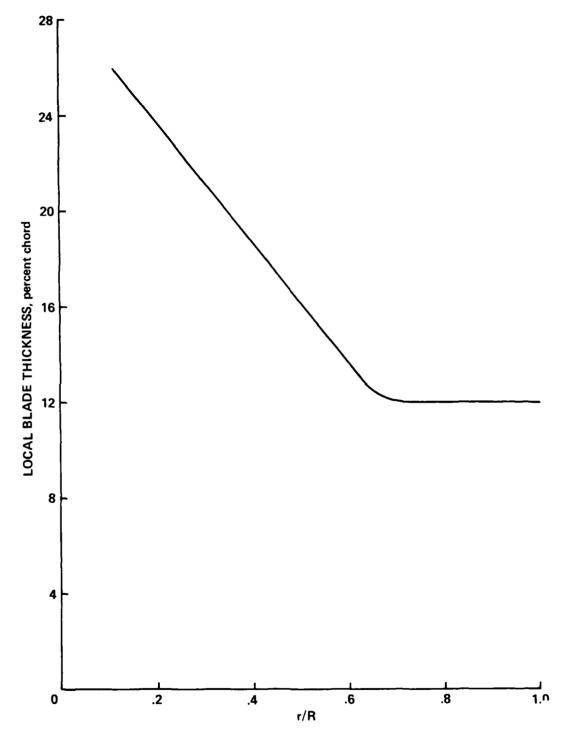


Figure 3. SKETCH OF ROTOR BLADE

X = BENDING GAGES



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Figure 4. BLADE THICKNESS DISTRIBUTION

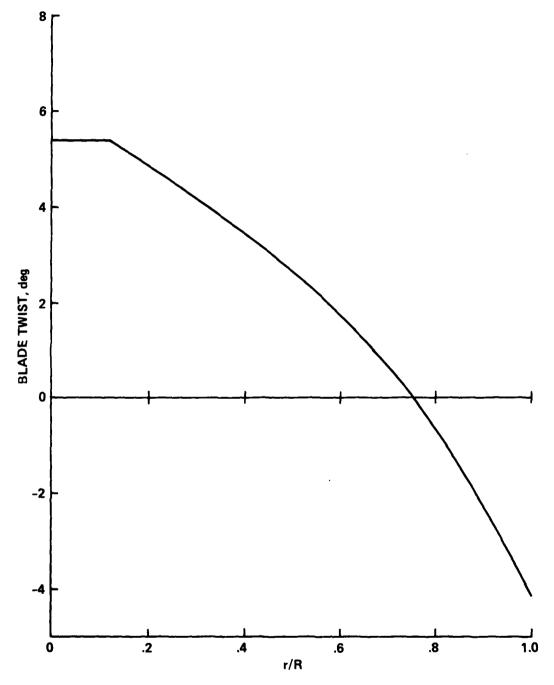


Figure 5. BLADE TWIST DISTRIBUTION

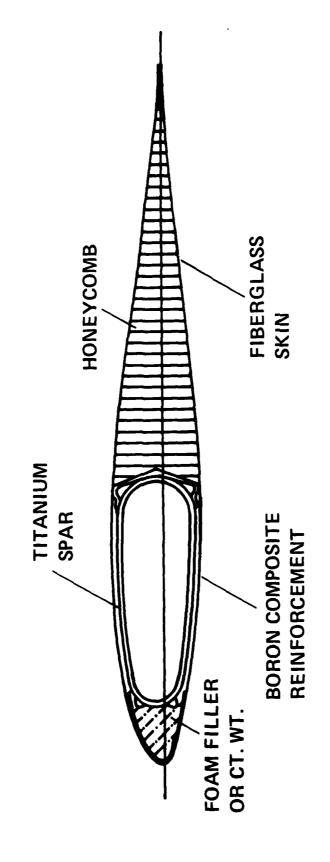


Figure 6. TYPICAL BLADE CROSS SECTION

f

## HARMONIC ORDER, cycles/rev

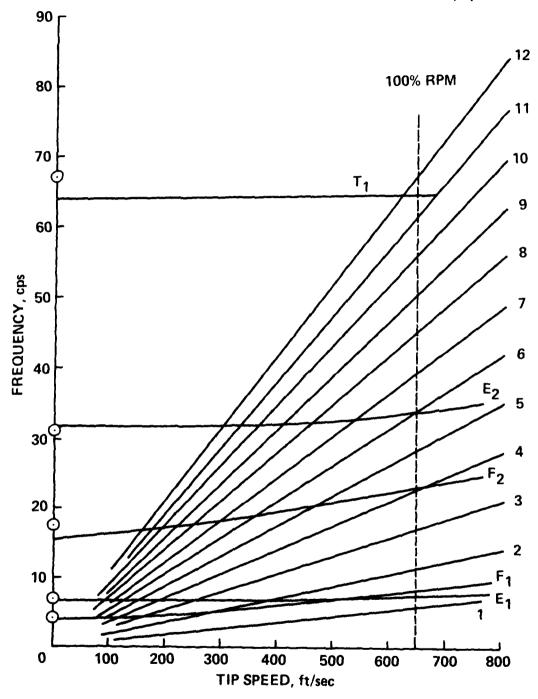


Figure 7. BLADE NATURAL FREQUENCY DIAGRAM

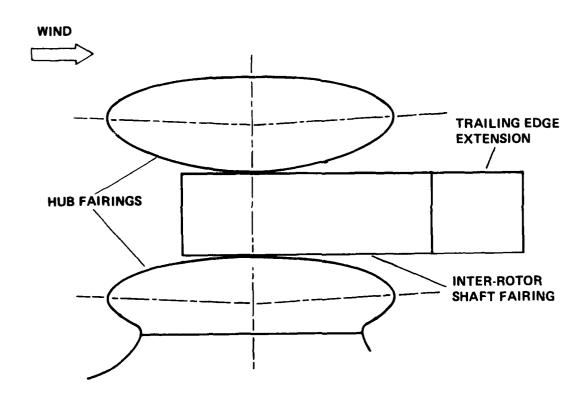


Figure 8. SKETCH OF HUB FAIRINGS

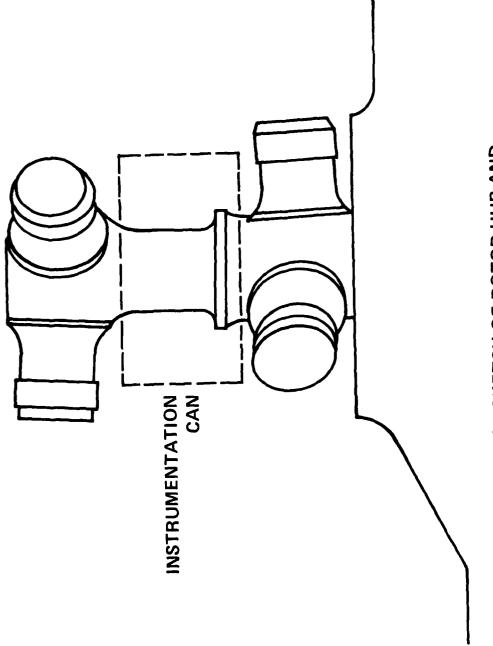


Figure 9. SKETCH OF ROTOR HUB AND INSTRUMENTATION CAN

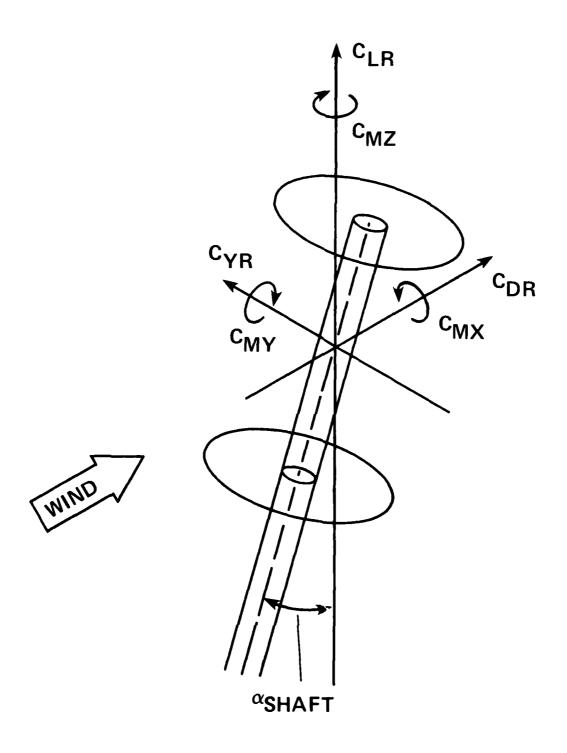


Figure 10. SKETCH OF FORCES AND MOMENTS SHOWING POSITIVE DIRECTIONS

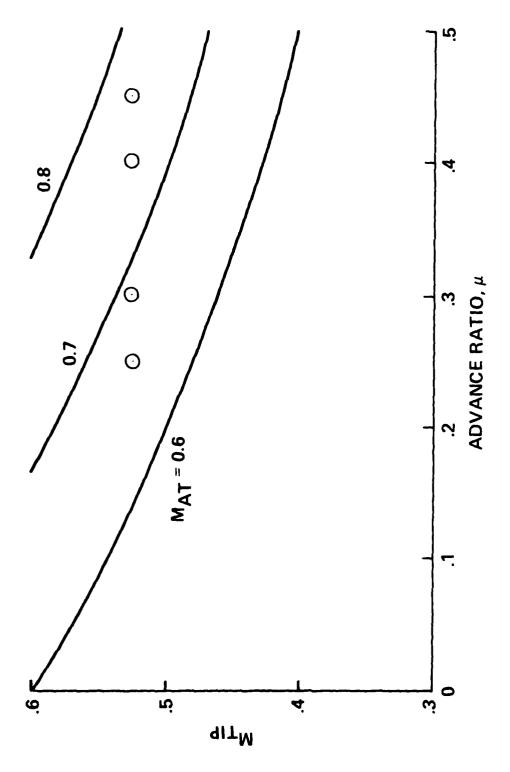


Figure 11. ROTOR OPERATING CONDITIONS

## APPENDIX I

Equations Used to Correct for Forces and Moments Produced by Exposed Model

Support Struts.

The strut fairings were canted 34° down relative to the horizontal. The lift and drag forces on the fairings were calculated as follows:

 $\psi = yaw \ angle, \ deg, \ positive \ nose \ right$   $\alpha = corrected \ angle \ of \ attack$  "RF" subscript denotes right strut fairing "LF" subscript denotes left strut fairing  $\alpha_{RF} = \cos 34^{\circ} \ \alpha + \sin 34^{\circ} \ \psi$   $\alpha_{LF} = \cos 34^{\circ} \ \alpha - \sin 34^{\circ} \ \psi$   $C_{LRF} = 0.02698 \ \alpha_{RF} + 1.8 \sin \alpha_{RF} \ | \sin \alpha_{RF} |$   $C_{LLF} = 0.02698 \ \alpha_{LF} + 1.8 \sin \alpha_{LF} \ | \sin \alpha_{LF} |$   $Lift_{RF} = 5.22 \ q \ C_{LRF}$   $Lift_{LF} = 5.22 \ q \ C_{LRF}$   $Lift_{LF} = 5.22 \ q \ C_{LLF}$   $C_{DLF} = 0.02698 \ \alpha_{RF} \ tan \ (\alpha_{RF}/2) + 1.8 \sin \alpha_{RF} \ | \sin \alpha_{RF} | \ (induced)$   $+ 0.02002 + 0.016457 \ C_{LRF}^2 \ (profile)$   $C_{DLF} = 0.02698 \ \alpha_{LF} \ tan \ (\alpha_{LF}/2) + 1.8 \sin \alpha_{LF} \ | \sin \alpha_{LF} | \ (induced)$   $+ 0.02002 + 0.016457 \ C_{LLF}^2 \ (profile)$   $D_{rag_{RF}} = 5.22 \ q \ C_{DRF}$ 

DragLF = 5.22 q CDLF

The corrections made to the aircraft forces and moments due to the lift and drag on the fairings were as follow:

Rolling Moment<sub>C</sub> = Rolling Moment<sub>U</sub> + cos 34° Lift<sub>RF</sub> (ycos  $\psi$  -Xsin  $\psi$  cos  $\alpha$ )  $-\cos 34° \text{ Lift}_{LF} \text{ (Ycos } \psi + \text{Ysin } \psi \text{ cos } \alpha\text{)} + \sin 34° \text{ Zcos } \alpha$   $\text{(Lift}_{RF} - \text{Lift}_{LF}\text{)}$ 

Yawing Moment<sub>C</sub> = Yawing Moment<sub>U</sub> - DragRF (cos  $\psi$  -Xsin  $\psi$  cos  $\alpha$ ) + DragLF (Ycos  $\psi$  +Xsin  $\psi$  cos  $\alpha$ ) + 2 DragRFI XI sin  $\psi$  cos  $\alpha$ - YT cos  $\psi$  (DragRFT - DragLFT) + XT sin  $\psi$  cos  $\psi$  (DragRFT - DragLFT) - DragNT XN sin  $\alpha$ 

The dimensions X,  $X_T$ ,  $X_N$  etc. are the distances (in feet) between the aircraft moment resolving center (aircraft c.g.) and the locations of the various lift and drag producing components, such as the strut fairing, the strut fairing tip, etc.

$$X = 4.845$$
 ft  $X_T = 4.683$  ft  $Y = 2.925$  ft  $Y_T = 4.167$  ft  $Z_T = 4.4$  ft  $Z_T = 4.976$  ft  $Z_N = 8.4$  ft  $Z_N = 4.25$  ft

## APPENDIX II

Equations Used to Correct for the Thrust of the J60 Engines.

The J60 engines on the ABC were calibrated in an engine test cell before the wind tunnel test. This calibration defined the relationship between static thrust and exhaust pressure ratio (EPR). During the wind tunnel test, the measured EPR and the test cell calibration were used to calculate the static thrust of each engine. This value for the static thrust was analytically corrected to account for the effect on the thrust of the nonzero velocity in the tunnel.

Thrust =  $\delta (T_{EPR} + \Delta T_M)$  (1bs)

where  $\delta$  = barometric pressure (in Hg)/29.92

TEPR = static thrust calculated from thrust vs. EPR calibration, lbs

 $\Delta T_{\mbox{\scriptsize M}}$  = correction to thrust due to nonzero wind velocity, lbs The value of TEPR as a function of the measured EPR was determined by a linear interpolation between the nearest two values of EPR and TEPR in the following table:

EPR	EPR
1.0 1.063 1.129 1.198 1.267 1.337 1.410 1.486 1.564 1.641 1.719 1.796 1.873 1.948 2.022 2.098	0 200 400 600 800 1000 1200 1400 1600 2000 2200 2400 2600 2800 3000

The value of  $\Delta T_M$  was also determined by linear interpolation. The interpolation for tunnel Mach number,  $M_{tun}$ , was performed first and the interpolation for EPR was performed next.

 $\Delta T_M$  as a Function of  $M_{tun}$  and EPR

			М	tun				
		0	0.05	0.1	0.15	0.2	0.25	0.3
	1.0 1.1 1.2 1.3 1.4-2.0 2.1	0	0	0	0	0	0	0
	1.1	0	-22	-40	-54	-64	-72	-72
	1.2	0	-40	-71	-96	-113	-127	-127
EPR	1.3	0	-57	-101	-135	-160	-179	-179
	1.4-2.0	0	-64	-114	-155	-183	-202	-205
	2.1	0	-64	-114	-155	-183	-202	-192

After the thrust of each J60 engine had been calculated by the above method, the forces and moments produced by the engines were removed from the measured forces and moments using the following equations:

"c" means corrected

"u" means uncorrected

 $Lift_{C} = Lift_{U} - sin \alpha (T_{R} + T_{L})$ 

 $Drag_{C} = Drag_{U} + cos \alpha (T_{R} + T_{L})$ 

Pitching Moment<sub>C</sub> = Pitching Moment<sub>U</sub> =  $(T_R + T_L)$  (1.88 sin  $\alpha$  cos  $\alpha$  + cos  $\alpha$  (1.21 + 1.88 sin  $\alpha$ )

Rolling Moment<sub>C</sub> = Rolling Moment<sub>u</sub> - 4.42 ( $T_L + T_R$ ) sin  $\alpha$ 

Yawing Moment<sub>C</sub> = Yawing Moment<sub>U</sub> =  $4.42 (T_R + T_L) \cos \alpha$ 

Three errors are evident in these equations which have not been corrected in the data presented in this paper.

- (1) the underlined "-" sign in the pitching moment equation should be a "+" sign and the underlined "+" sign should be a "-" sign.
- (2) the underlined "-" sign in the yawing moment equation should be a "+" sign.
- (3) the effect on the aircraft forces and moments due to aircraft yaw angle changes have not been included in these equations.

The effect of these errors on the data presented here has been evaluated, and in no case does the effect of any error exceed 2% of the data presented. The only exception to this is in Run 10, where significant amounts of auxiliary propulsion thrust were used.

## SECTION A Aircraft Performance Data

ES -

IT CODE										
CONSTRAINT	TEMP RHO100	79.0	80.0 0.2257	80.0 0.2257	80.0 0.2257	80.0 0.2257	80.0 0.2257	80.0 0.2257	90.0	91.0
SEQUENCE OF	PITCH/Q YAM/3 ROLL/Q	-209.0 20.3 5.5	-106.3 13.7 3.9	15.4 4.4 0.4	105.1 -0.3 1.9	220.8 -3.6 4.6	361.1 -6.4 2.1	462. -6.3 4.8	110.6 -5.8 7.3	183.6 -5.6 6.4
THE FOLLOWING	DR AG / Q L I F T / Q SI DE / Q	16.76 25.71 -0.22	15.96 11.67 -0.37	15.73 -0.44 -0.22	16.05 -14.09 0.31	17.14 ~28.08 0.59	18.90 -44.30 0.53	21.93 -57.43 0.95	16.11 -15.42 -0.59	16.63 -23.04 -0.30
SATISFIED	RPM J THRUST BAR	343.0 0. 29.96	343.0 0. 29.96	343.0 0. 29.96	342.9 0. 29.96	342.8 0. 29.96	342•7 0• 29•96	342.6 0. 29.96	342•3 0• 29•96	342•6 0• 29•96
GROJP OF POINTS	ALFS, U ALFS, C PSI	5.0 5.1 0.0	2.5 2.5 0.0	0000	-2.5 -2.5 0.0	-5.0 -5.1 0.0	-7.5 -7.6 0.0	-9.8	-2.5 -2.5 0.0	-3.8 -3.9 0.0
DATA IN THE FULLOWING SI	NATS MTUN GPSF	113.7 0.1766 45.3	119.0 0.1769 45.5	113.8 0.1767 45.4	119.0 0.1769 45.5	119.10.1771	119.0 0.1770 45.5	118.7 0.1765 45.3	173.4 0.2639 94.8	178.3 0.2035 98.5
A IN THE		5 ri	4	2	w		ဆ	σ	10	p.
DAT		P T P	P	P	<b>⊢</b> 54	10	F d	T d	F d	2

TEMP	79.0	80.0	84.0	87.0	88.0	90.0	92.0	93.0	94•0	96.0
RH0100	0.2250	0.2246	0.2190	0.2178	0.2175		0.2159	0.2155	0•2152	0.2144
PITCH/Q	390.5	475.3	0.5	197.6	120.4	-103.8	-219.3	-364.9	-360.5	-368.2
YAW/G	-9.5	-3.4	-1.5	-6.7	-4.4	3.0	6.0	8.6	4.1	-1.3
ROLL/Q	6.4	1.2	8.6	11.9	7.9	10.9	8.1	10.9	14.4	14.8
DRAG/Q	17.61	21.43	14.62	15.36	14.96	14.71	15.09	16.51	17.76	17.21
LIFT/Q	-44.71	-57.12	-2.89	-22.78	-15.40	9.31	22.68	34.10	50.01	49.76
SIDE/Q	0.00	0.24	-0.49	-0.44	-0.61	-0.57	-0.60	-0.02	0.30	-0.07
RPM	342.9	342.9	343.3	343.1	343.0	343.2	343.3	343.4	343.4	22.2
J THRUST	140.	136.	18.	8.	12.	19.	19.	21.	18.	17.
BAR	29.81	29.81	29.81	29.81	29.81	29.81	29.81	29.81	29.81	29.81
ALFS,U ALFS,C PSI	-7.5 -7.6 0.0	-9.8 -10.0	0.0	-3.8 0.0	-2.5 -2.5 0.0	2.5	5.0 5.1 0.0	7.5	10.0	10.0
WATS	119.0	118.8	179.2	178.6	178.6	178.7	178.9	178.8	174.7	178.9
MTUN	0.1772	0.1766	0.2666	0.2649	0.2647	0.2644	0.264 <u>1</u>	0.2637	0.2634	0.2632
PSF	45.4	45.1	103.2	99.0	98.8	93.6	98.4	98.1	97.9	97.7
	0 .1	F1	12	13	14	£:	16	17	<b>8</b>	0.
	1 d	4	ď	<b>L</b> a	56	F d	d.	d.	r a	L a

TEMP KHÜLÖÜ	98.0 0.2136	• 60	0.2133	0.21 <i>77</i> 90.0 0.2165	91.0 0.2161 90.0 0.2203	90.0	0.2206 89.0 0.2207
PITCH/Q YAW/U RULL/Q	-278.2 4.9 13.9	-169.9 4.0 12.3 -97.0	14 18	132.2	205.3 -10.5 7.5 450.9 -4.9	389.3	11.3 111.6 -2.2 10.3
DRAG/Q LI FT/Q SI DE/Q	16.06 37.23 -0.52	14.91 24.15 -0.15		14.41	14.86 -23.75 -0.57 -21.38 -55.56	16.62	14.80 -29.03 -0.31 14.00 -14.24 -0.49
RPN J THRUST BAR	18.0 22. 29.81	20 N · ·	24.0 23. 29.81	29.78 29.78 18.3 15.	, <u> </u>	18•3 127• 29•78	18.3 131. 29.78 18.3 141. 29.78
ALFS,U ALFS,C PSI	7.5 7.6 0.0	ν. ν. υ υ ο υ	C C C C	000 000	0 8 6 0 8 6 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-7.5 -7.6 0.0	1.8.0 1.2.0 1.2.0 0.00
VKTS ATUN DPSF	179.2 0.2631 97.7	179.1 0.2630 97.6	179.2 0.2629 97.5	177.9 0.2639 98.2 178.3 0.2638	178.3 0.2635 97.9 119.5 0.1761	119.8 0.1765 45.0	120.0 0.1770 45.3 119.6 0.1764
	50	۲۵ د	22	23 23	25 26	27	29
	14		<b>4</b>	E. 57	1 d t	4	14

TEMP RH0100	89.0 0.2207	89.0 0.2207	89.0 0.2207	89.0 0.2207	90.0	89.0 0.2207	89.0 0.2237	76.0	77.0 0.2256	78.0 0.2252
PITCH/U YAW/O RULL/U	9.1 0.0 11.4	-88.0 4.6 11.1	-199.8 8.9 12.2	-312.2 7.3 14.6	-435.9 4.9 13.9	12.8 12.0 11.6	3111.2 2.6 1077.6	-288.0 17.1 22.0	-413.3 12.3 19.7	-285.8 12.8 22.1
DRAG/Q L1F1/Q SI DE/Q	13.67 -1.11 -0.55	13.74	14.49 25.01 0.27	15.69 39.04 -0.11	17.01 52.51 -0.27	14.63 -2.00 0.78	161.54 -305.05 95.92	15.37 25.56 0.48	18.30 51.39 0.57	16.65 38.54 0.26
RPM J THRUST BAR	18.3 143. 29.78	18.3 148. 29.78	18.3 148. 29.78	18.3 148. 29.78	18.3 147. 29.78	18•3 0• 29•78	18.3 0. 29.78	344.2 170. 2°.79	344•3 168• 29•79	344.2 166. 25.79
ALFS, U ALFS, C PSI	000	0 2 2 0 0 5 0 5 0 5	5.0	7.5	10.0	000	000	10.0	10.0	7.5 7.6 0.0
VKTS STUN PSF	119.8 0.1766 45.1	119.5 0.1762 44.9	119.3 0.1759 4+.7	119.4 0.1761 44.8	119.5 0.1762 44.8	119.5 0.1762 44.9	6.0 0.0388	119.5 0.1784 46.0	119.6 0.1784 46.0	113.7 0.1783 45.9
			32	<i>ዜ</i> ን ዜን	34	35	36	n m	Í	ι <b>c</b> /
	PT	9	Ld	<b>⊢</b>	58	<b>⊢</b> <b>0</b> .	La d	Š E	P T	Pd

9 0 0	9.0	0 * 4	0.4	0.0	36	36	32	•0	• 0 58	0.4 4.
TEMP RHG100	79	80 0.22	80	81 0.22	0.22	0.22	83.0.22	91.0.21	92.	93
PIICH/U YAN/U ROLL/Q	-198.6 13.7 20.8	-93.0 10.5 19.2	7.3 6.4 20.7	114.9 6.4 19.1	242.0 -0.5 17.5	387.4 -1.7 21.5	469.4 -2.3 11.7	206.0 -5.1 17.2	138.5 -2.1 21.1	21.1 -0.2 16.7
DRAG/U LIFT/C SIDE/U	15.40 25.57 0.72	14.75 12.08 0.89	14.63 -0.66 1.01	15.04 -14.16 1.01	15.92 -29.83 1.80	17.79 -45.22 2.03	21.81 -56.81 2.03	15.14 -23.98 0.77	14.73 -15.28 0.45	14.27
RPM J THKUST BAR	344.1 166. 29.79	344.0 164. 29.79	2.3.9 161. 29.79	343.8 157. 29.79	343.8 149. 29.79	343.8 143. 29.79	343.6 137. 29.79	343.7 12. 29.79	343.8 14. 29.79	343.9 21. 29.79
ALFS,U ALFS,C PSI	5.0 5.1 0.0	C 2 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	0000	-2.5	-5.0	17.5	-10.0	-3.8 -3.9	-2.5 -2.5 0.0	0.00
VKTS MTUN MS 40	114.6 0.1780 45.8	119.8 0.1782 45.9	119.5 0.1776 45.6	119.4 0.1775 45.5	114.5 0.1775 45.5	119.3 0.1771 45.3	113.9 0.1763 44.9	178.5 0.2638 98.2	178.6 0.2637 93.0	178.2 0.2628 97.4
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TEMP RH0100	95.0 0.2148	97.0 0.2140	97.0 0.2140	98.0 0.2136	101.0	102.0	103.0	103.0 0.2118	104.0 0.2114	105.0
PITCH/U YAM/U RULL/G	-93.8 0.7 18.0	-169.3 4.0 15.2	-266.2 7.2 15.1	-360.6 2.9 14.8	30.4 -5.8 12.8	-364.6 -0.7 14.2	-270.1 0.5 13.3	-160.9 -1.8 12.4	-81.1 -3.0 12.3	149.1 -5.9 15.6
URAG/Q L1FT/Q S1DE/Q	14.42 9.76 0.11	15.14 23.99 -0.13	16.35 36.91 -0.34	17.86 49.21 -0.50	13.55	17.13 49.42 -1.67	15.65 36.54 -1.56	14.34 23.04 -1.15	13.62 8.88 -0.48	13.96 -17.22 -0.43
RPM J THRUST BAR	344.0 24. 29.80	344.1 23. 29.80	344.1 24. 29.80	344.2 23. 29.80	31.5 21. 29.80	31.5 20. 29.80	2.0 23. 25.80	18•6 25• 29•80	18•6 25• 29•80	18.6 16. 29.80
ALFS,U ALFS,C PSI	2.5 2.5 0.0	5.0 5.1 0.0	7.5	10.00	300	10.0	7.577.6	5.0 5.1 0.0	0.22° 0.00°	-2.5 -2.5 0.0
VKTS MTUN PPSF	178.3 0.2624 97.2	175.4 0.2622 97.0	178.3 0.2620 90.9	178.3 0.2618 95.7	178.8 0.2518 96.7	178.0 0.2514 90.4	178.9 0.2616 96.6	178.7 0.2012 90.3	178.8 0.2011 96.2	179.U U.2612 96.3
	9	7.	16	<u>c</u> .	20	21	<b>£</b> ;	٤,	77	<b>(</b> )
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						<b></b>	0.15			2.2
TEMP RH0100	105.0 0.2110	103.0 0.2154	102.0 0.2158	101.0	101.0	100.0 0.2165	100.0	99.0	99.0 0.2169	99.0 0.2169
PITCH/LL YAW/L RULL/J	209.2 -4.8 12.1	430.4 -3.6 12.0	370.6 -5.8 16.0	243.5 -4.4 20.1	122.0 -2.1 19.7	9.1 0.4 14.2	-97.8 5.4 19.8	-202.4 5.6 17.6	-310.6 7.0 23.1	-417.8 2.6 20.3
URAG/Q LIFT/Q SIDE/Q	14.45 -24.14 -0.43	21.26 -54.81 0.64	16.51 -44.85 0.78	14.75 -29.74 0.16	13.88 -15.99 -0.27	13.49 -2.26 -0.59	13.55 10.90 -1.04	14.21 23.68 -1.00	15.55 37.57 -1.48	17.18 50.19 -1.14
RPM J THFUST BAR	18.6 14. 29.80	18.6 135. 29.80	18.6 139. 29.80	18.6 144. 29.80	18.6 147. 29.80	18.6 149. 24.80	18.6 153. 29.80	18.6 156. 29.80	18.6 157. 29.80	18.6 157. 29.80
ALFS,U ALFS,C PSI	1 1 41 41 3 8 0 3	8°5°	17.5	7.0 0.0	-2.5 -2.5 0.0	300	2.5 0.0	5.0 5.1 0.0	7.5 7.6 0.0	10.0
ATUN LPSF	178.8 0.2609 90.1	119.0 0.1733 43.5	119.5 0.1741 43.9	119.6	119.7	213.6 0.1747 44.2	119.5	119.4	119.4 0.1745 44.1	119.2 0.1743 43.9
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TEMP RH0100	98.0	73.0 0.2294	74.0	75.0	75.0 0.2286	76.0	0.2277	0.2277	78.0 0.2273	79.0 0.2269
PITCH/Q Yaw/Q Roll/Q	11.6 3.2 20.6	1.2	-455.2 1.4 7.8	-315.6 9.5 5.2	-206.6 6.8 5.7	-106.8 6.3 6.1	8 4 4 0 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	119.8 4.0 11.6	220.3 6.4 8.5	367.1 2.5 8.0
URAG/Q LIFT/Q SIDE/Q	14.35	15.06 -4.10 1.08	18.79 49.16 0.83	17.19 36.91 0.67	15.87 22.08 0.45	15.21 3.96 3.65	15.10 -4.33 0.82	15.50 -17.13 0.78	16.56 -31.13 0.89	18.09 -46.46 1.07
RPM J THRUST BAR	18.6 0. 29.80	4-0	344.9 166. 30.07	344.9 164. 30.07	344°8 168° 30°07	344.7 165. 30.07	344.6 162. 30.07	344.5 159. 30.07	344.4 151. 30.07	344.3 140. 30.07
ALFS,U ALFS,C PSI	000	000	10.0	7.5	5.0000000000000000000000000000000000000	0.55	000	-2.5 -2.5 J.u	3 4 3	-7.5 -7.6 0.0
NUTE NOTE A	119.4	119.1 0.1782 46.3	119.7 0.1790 46.7	119.5 0.1785 46.5	119.1 0.1780 46.2	119.2 J.1779 46.2	119.2 0.1773 46.1	119.2 0.1777 45.1	119.2 0.1775 40.0	119.2 0.1774 45.9
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TEMP RH0100	68.0 0.2335		n	70.0 0.2327	73.0	74.0	0.2299 0.2295	75.U 0.2295
PITCH/Q YAM/G KOLL/Q	15.9 2.2 27.9	-114.5 0.5 24.0 -174.0	255.1 -253.7 0.0 29.8	-344.3 5.9 22.4	-+14.0 11.1 17.4	-444.1 5.4 9.1 -321.1	NN 8444	-121.4 5.4 0.6
DRAG/U LIFT/Q SIDE/Q	16.92 -7.69 0.08	16.74 5.41 -0.08 16.42	17.09 30.95 -1.09	18.06 44.10 -1.26	20.35 60.96 -1.27	20.98 53.82 -0.60	40.81 -0.72 18.41 25.59 0.68	17.61 12.38 -0.08
RPM L THRUST BAR	343.5 254. 30.00	343.6 253. 30.00	30.00 343.5 257. 36.00	343.4 254. 30.00	400	343.6 226. 30.00 343.6	229. 30.03 343.5 225. 34.00	343.5 223. 36.00
ALFS,U ALFS,C PSI	1.2 2.5 0.5 0.5	330 55 000 84	0.00 0.00 0.00	7.5 7.6 0.0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	10.0 10.1 0.0 7.5	00 0H0	2.5 2.5 0.0
VATS ATUR APSF	0.0904 0.0904 12.1	000.0 0.0001 12.0 12.0	12.0 0.0899 11.9	0.00 0.00 0.00 0.11	59.00 6980.00 8.11	40.0 40.1345 26.5 49.9	2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	09.8 0.1340 20.4
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ТЕМР	75.0	78.0	79.0	82.0	82.0	83.0	83.0	84.0	84.0	84.0
РНU100	0.2294	0.2282	0.2277	0.2251	0.2250	0.2246	0.7246	0.2242	0.2242	0.2243
PITCH/E	-42.5	69.2	176.9	392.3	312.8	180.9	77.3	-19.9	-115.7	-231.3
YAW/E	4.9	-4.3	-8.7	-3.2	-5.5	-2.5	1.3	2.6	6.6	9.5
RULL/E	749.5	4410.1	11.5	12.8	16.3	17.5	16.6	17.9	139.0	699.1
DRAG/Q	17.43	17.54	18.20	23.51	19.41	17.82	16.92	16.57	16.68	17.39
LIFT/Q	-1.13	-12.81	-27.20	-54.88	-43.73	-29.22	-15.36	-3.50	8.99	22.61
SIDE/Q	0.64	0.42	0.61	-0.02	0.52	0.48	0.57	0.53	0.42	0.24
RPM	343.4	343.3	343•3	343.3	343.3	343.4	343.4	343.4	343.5	343.5
J THRUST	223.	214.	208•	136.	137.	144.	146.	154.	157.	157.
BAR	30.00	30.00	29• 99	29.99	29.99	29.99	29.99	29.99	29.99	29.99
ALFS, U ALFS, C PSI	000	12.5	0.0	8 · 6 - 6 · 6 - 0 · 0	-7.5 -7.6 0.0	-5.0 -5.1 0.0	12.5	200	2 . 5 0 . 5 0 . 5	5.10
VKTS	93.2	9.00	49.9	119.2	119.7	119.8	119.7	1:3.5	119.4	113.3
ATUN	0.1340	0.1338	0.1337	0.1770	0.1777	0.1777	0.1776	0.1771	0.1769	
1PSF	26.6	0.5.38	26.2	45.6	45.9	45.9	45.9	45.6	45.6	
	3	ali er	<u>ل</u> چا	7:	හ ළඹ	C F:	نڙ	<b>C</b> .	25	23
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TEMP RH0100 85.0	85.U 0.2238	86.U 0.2234	86.0 0.2234	87.0 0.2230	87.0 0.2230	84.0 0.2226	88.J 0.2226	88.U 0.2226	89.0 0.2222
PITCH/W YAM/D RULL/Q -344.7 14.8	18.9 -496.5 14.1 16.2	-157.6 295.0 -144.1	-111.1 235.4 -107.1	-80.2 196.3 -82.2	158.6 148.9 156.9	-36.6 101.7 206.9	-26.0 53.0 -24.9	-31.7 -25.0 6.9	-55.7 -80.4 22.2
URAG/U LIFT/Q SIDE/Q 18.64 36.90	0 0 20	23.28 5.85 -40.76	21.03 2.98 -33.18	19.50 0.88 -26.25	16.37 0.00 -19.89	17.53 -2.20 -12.44	16.89 -2.98 -5.82	16.77 -2.97 7.15	17.23 -1.10 13.65
KP KUS BA BA 43.		343°3 155• 29°99	343.3 157. 29.99	342.3 155. 29.99	343.3 157. 29.99	343.3 153. 29.99	343 • 3 154 • 29 • 99	343.3 152. 29.49	342.3 154. 25.99
ALFS, U ALFS, U PS I 7.5		0.00	0.0	0.01	0.0	0.0-0	20.0	0.50	0.00
119.4 1768	45.5 113.3 0.1766 45.4	119.2 0.1762 45.2	119.3 0.1764 45.3	119.3 3.1763 45.2	219 • 4 49 • 4 49 • 49 • 3	119.6 G.:7c6 45.4	119.5 0.1764 45.3	119.7 0.1767 45.4	119.7 0.1765 65.3
75 Id	pi siy	PT 26		e 66		PT 3ز			6: 10

TEMP	89.0	90.0	90.0	90.0	90.0	78.0	81.0	82.0	83.0	83.0
RHU100	0.2222	0.2218	0.2218	0.2218	0.2218		0.2236	0.2233	0.2229	0.2229
FULL/G	-84.7	-101.4	-146.1	-176.0	-15.2	1445.7	-331.U	-210.7	-99.4	9.3
	-126.1	-176.8	-225.8	-252.8	-0.1	4.0	8.5	4.8	3.1	1.6
	41.1	69.5	96.8	119.3	12.6	5.5	5.9	5.4	1.9	9.3
URAG/U	17.99	19.09	20.62	21.90	17.46	20.10	18.60	17.44	16.87	16.76
LIFT/U	0.55	1.76	4.39	6.39	-5.93	47.24	34.81	20.93	7.53	-4.16
SIDE/Q	20.47	27.36	34.64	38.97	0.40	-0.06	-0.32	0.20	0.34	0.47
RP4	343.2	343.4	343.4	343.3	4•6	344.9	344.7	344.6	344.4	344.2
J THEUST	151.	150.	150.	150.	0•	107.	109.	113.	108.	101.
BAR	29.99	29.93	29.99	29.99	29.99	29.99	29.99	29.99	29.99	29.99
ALFS,U ALFS,C PSI	00°C	0.00	0.0 0.0 12.5	0.0	000	10.0	7.5 7.6 0.0	5.0 5.1	2.5	0.0-0
AKT UN	119.3	119.9	120.0	119.3	123.0	149.4	149.7	149.3	149.5	149.4
MT UN	0.1767	0.1767	0.1768	0.1765	0.1768	0.2230	0.2228	0.2220	0.2220	0.2219
EP SE	45.4	45.4	45.5	45.3	45.5	71.5	71.4	70.9	70.9	70.8
	34	ar. e.	36	5	8	۵. r	4	ιν	<b>↓</b>	7
	F	Lo	<b>L</b> a	PI	E 67	8 € F P P P P P P P P P P P P P P P P P P	L d	P d	19	PT

TEMP	84.0	85.0	91.0	93.0	94.0	96.0	97.0	98.0	99.0	103.U
PHU100	0.2225	0.2220		0.2169	0.2165	0.2157	0.2153	0.2150	0.2146	0.2131
PITCH/Q	93.0	205.7	154.7	94.1	-11.1	-115.5	-248.4	-305.7	-399.3	-427.2
YAm/Q		-5.5	-5.9	-6.4	-0.9	-1.3	6.2	5.7	1.0	-5.1
RULL/Q		7.0	8.7	9.7	8.2	6.7	8.4	13.8	10.2	11.9
DRAG/U	17.10	18.06	17.50	17.08	16.68	16.80	17.36	18.61	19.98	19.67
LIFT/Q	-17.31	-30.13	-25.10	-18.77	-5.82	5.32	17.70	35.20	47.86	47.94
SIDE/U	0.89	0.44	0.83	0.63	0.18	0.53	-0.32	-0.64	-0.21	-1.41
RPM	344.1	344•1	344•0	344•U	344.2	344.2	344.3	344•3	344.3	14.1
J THRUST	93.	87•	10•	15•	25.	24.	25.	29•	25.	24.
BAR	29.99	29•99	29•99	29•99	29.99	29.99	29.99	29•99	29.99	29.99
ALFS.U ALFS.C PSI	-2.5 -2.5 0.0	-5.0 -5.1 0.0	8.8.9 0.0	.2. 0.0 0.0	0.00	2.5 2.5 0.0	5.0 5.0 0.0	7.5 7.6 0.0	10.0	0.00 0.00
VKTS	149.3	149.5	177.9	178.5	178.9	179.0	178.9	178.8	174.8	178.8
MIUN	0.2217	0.2217	U.2629	0.2633	0.2630	0.2633	0.2629	0.2625	0.2623	0.2614
FSF	70.7	70.7	98.2	98.4	98.7	94.4	98.2	97.9	97.7	97.1
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	<b>a.</b>	9	4	PT	68	G.	<u>-</u>	1 a	L d	F 9

TEMP RHU100	103.0 0.2131	104.0 0.2128	105.0 0.2125	106.0 0.2120	106.0	107.0	104.0 0.2163	103.0 0.2166	102.0 0.2170	101.0
PITCH/G YAW/G RULL/G	-321.4 -3.6 6.3	-265.J -4.7 5.6	-124.6 -7.5 6.2	110.0	8 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	138.9 -6.2 d.3	378.7 -3.4 14.3	306.1 -6.4 12.2	179.1 -8.6 9.5	96.0 6.3.0
DRAS/4 LIFT/Q SIDE/Q	18.46 34.81 -1.32	17.53 17.97 -0.83	16.96 4.29 -0.03	16.95 -7.72 0.35	17.29 -19.26 0.61	17.55 -24.59 0.53	23.60 -54.13 0.91	19.42 -43.49 1.34	17.71 -30.85 1.22	17.09 -17.54 1.00
RPM J THKUST BAR	14•1 30• 29•99	14•1 28• 29•99	14•1 29• 29•99	14.1 24. 29.99	14.1 15. 29.99	14.1 8. 25.99	14•1 136• 29•97	14.1 141. 29.97	14.1 144. 29.97	14.1 153. 29.97
ALFS, U ALFS, C PSI	7.5 7.6 0.0	0	0.0 0.0 0.0	0.0	12.5	8 3 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8 • 6 - 6 • 6 - 0 • 0	-7.5 -7.6 0.0	1.5.0	-2.5 -2.5 0.0
NTT NUT NO PER SE	173.2 0.2605 90.5	178.4 0.2606 96.5	177.7 0.2592 35.5	178.6 0.2604 96.4	178.5 0.2602 96.2	178.4 0.2599 90.0	119.2 0.1735 43.8	119.7 0.1742 44.2	119.6 U.1743 44.2	119.4 0.1742 44.2
	a. F	(f.	52 10	12 La	PT 22		7ā la			

TEMP RHO100	100.0 0.2178	9 Pm	99.0 0.2182	99.0 0.2182	48.0 0.2186	no4	98.0 0.2185	93.0 0.2235	91.0 0.2243	88.0 0.2255
PITCH/Q YAM/Q ROLL/Q	10.1	-104.2 -1.9 3.7	-230.3 -1.2 9.0	-355.5 4.5 23.8	-486.2 4.5 22.5	-0.1 6.4 3.5	-12.1 6.8 1.4	1636.7 -2771.7 -4543.9	744.5 -1304.1 -2452.5	-330.3 -2037.9 349.5
DRAG/Q LIFT/Q SIDE/Q	16.77 -5.99 0.72	16.74 6.67 0.36	17.42 21.03 -0.32	18.63 35.96 -1.22	19.95 48.11 -1.08	16.91 -4.29 0.41	17.70 -5.10 0.82	95.95 -358.87 215.43	-350.61 -61.01 79.35	-142.51 117.32 -4.69
RPM J THRUST BAR	14.1 158. 29.97	14.1 164. 29.97	14.1 163. 29.97	14.1 167. 29.97	14•1 167• 29•97	344.8 163. 24.97	344.4 0. 29.96	4.3 151. 29.96	4•3 593• 29•96	4•3 1176• 29•96
ALFS.U ALFS.C PSI	0.0	2.5 2.5 0.0	0.0 0.0 0.0	7.5	10.0	000	200	000	200	202
VKTS MTUN 4PSF	119.3	119.4 0.1744 44.2	119.2 0.1741 44.1	113°2 0°1742 44°2	119.3	119.2	118.9 0.1740 44.0	6.6 0.097 1.0	7.2 0.1105	3.1 0.1120
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ND TENDERS OF THE SECOND SECON	LAN DO	v) <u>Z</u> u, ∷	<b></b> ∨	ANA	08.46.79 L1FT.70 SI DE 72	TCH/ YAW/ OLL/	<b>₩</b> 0
0 6 6 6 7 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	505	000	4.3 1684. 29.96	-62.78 -62.78	-325.1 -3063.9 1352.7	69.0 0.2251
2.5.5.0 0.0185 0.5.0	12.6 .0185 0.5	300	000	4.3 22.30. 29.96	-42.97 68.88 -70.88	-501.1 -2367.2 34980.5	90.0 0.2247
14.9 0.0214 0.37	14.9 .0213 .0.7	000	000	4.3 2651. 29.96	16.36 49.66 -86.59	-414.4 -2346.2 1415.5	91.0
3.6 0.0127 0.3.2	3.6 .0127 0 3.2		၀၀၁	4.3 132. 29.96	-77.88 -63.11 -8.42	8 <b>u7.7</b> 314.3 256.6	91.0 0.2243
7.7 0. 0.0113 0. 0.2 0.	7.7 .0113 0.0		000	4•3 559• 29•96	-172.03 0.00 31.84	691.6 -67.9 -1207.3	90.0 0.2247
3.6 0.0127 0.2 0.2	3.6 U. .0127 0. 0.2 0.		000	4•3 1124• 29•96	-277.53 63.11 -67.35	3157.7 -924.6 -764.4	90.00
9.5 0.0139 0.3 0.3	9.5 .u139 0. 0.3 0.		000	4.3 1689. 29.96	-302.25 52.29 -118.58	1279.0 -1700.5 -612.0	89.0 0.2251
13.6 0. 0.0156 0. 3.4 0.	13.6 .0156 0.4		000	4.3 2140. 29.96	-210.19 41.59 -172.00	789.8 -1570.9 34.8	89.0
14.0 0.02.06 0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.	14.0 0 0206 0 0.6 0	505	000	4•3 2643• 29•96	-18.97 47.54 -87.20	-183.6 -798.6 -589.5	89.0 0.2251

DATA IN THE FOLLOWING GROUP OF POINTS SATISFIED THE FOLLOWING SEQUENCE OF CONSTRAINT CODES -

S,R Theg S,R J THRUST S,R CP/S	00	56 180. 33 2963. 48 229. 34 0.001602 88 0.003864 80 263. 79 263. 17 2.002323 93 0.004979	448. 51 7330. 06 215. 18 0.003962 04 0.007234	55 803. 63 13785. 08 215. 00 0.007045
CLR/S COR/S CAR/S CAY/S	CMX/S.P. 0.025602 0.001314 0.000024 0.021004 0.000204	0.071956 0.009033 0.011234 0.011234 0.001088 -0.005280 0.010579 0.000717 0.136714	1207 1207 013C 30C9 1746 9005	0.139755 0.012863 0.190208 0.190100
LIFT, R ORAG, R SIDE, R PITCH, R YAW, P	LL: 665 137 137 102 401 400	7393 978 978 5624 599 1997 1091 1091 744 6738	-3407. 17414. 1341. 23190. -269.	14317. 1327. 21. 26860.
LIFT ORAG SIDE PITCH YAW	2697. 600. 14. 5327. -462.	8148 1429 7373 7373 1309 1309 1598 1598	13233. 1849. 1819. 12199. -224.	15158. 1335. 13927.
BAR TEMP RHD100 L706 L708	29.78 24.0 0.220 1.75 2.48	29.78 96.0 0.2193 3.90 4.66 -7.2 79.78 98.0 0.2185	29.78 99.78 99.0 0.2181 3.81 4.19	29.78 132.0 0.2169 3.19
VKTS ATUN OPSF ALFS,U	•	89.4 0.1369 25.0 5.0 5.0 90.0 0.1314 25.2	0.1311 0.1311 255.0 5.0 6.2	89.9 0.1303 25.0
V/OR YAT TEG#R TIPA	APMY 0.24R9 0.6570 0.5261 371.3	0.7504 6.6535 0.6535 0.5227 319.8 93.1 0.6550 604.9 0.5235		6.2448 0.6546 607.5 0.5238
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VZOR VKTS BAR  "AT MTUN TEMP  CMEG*P 2PSF PHO100  TIPM ALFS,U L/DE  RPM ALFS,C L/D,P  RPM? PSI ANXL/R	89.8 29.78 64 0.1306 103.0 .2 24.9 0.2165 57 7.5 3.90 .7 8.3 4.47	490     90.0     29.78       568     0.1309     103.0       0.3     25.0     0.2165       259     7.5     3.92       3.8     8.3     4.50       4.2     0.0     -9.9	489 90.0 29.78 568 0.1309 103.0 259 25.0 0.2165 259 8.5 4.10 4.63 6.32 4.63 6.32 4.63 6.32 4.63 6.32 4.63 6.32 4.63 6.32 4.63 6.32 5.45 0.1309 104.0 8.3 25.0 0.2161 2.7 8.8 4.32	90 90.0 29.78 51 0.1308 104.0 .2 25.0 0.2161 7.5 3.59 .7 9.0 3.78
LIFT ORAG SIDE PITCH YAW ROLL	8746. 1370. 48. 3769. 448.	8756. 1872. 47. 3814. 455.	10456. 2124. 2124. 4831. 969. -900. 13383. 2508. 6189. 1520.	15772. 2802. 106. 8352. 2071.
LIFT, R DRAG, R STOE, R P ITCH, R YAW, R R CLL, R	7655. 1340. 60. 14479. 380.	7661. 1340. 59. 14568. 384.	9340. 1590. 51. 16362. 789. -1271. 12230. 1971. 19300. 1440.	14598. 2261. 120. 22844. 2066.
CLR/S, R COR/S, R CYR/S, R CMZ/S, R CMZ/S, P	0.073627 0.012891 0.000579 0.144598 0.000782	0.073642 0.012878 0.000569 0.144594 0.000773	0.085785 0.015282 0.000487 0.173484 0.100908 -0.002818 0.118578 0.019107 0.000489 0.222691 0.001264 -0.003399	0.140575 0.021790 0.001157 0.259676 0.002261
HP TCPQST CP/S CP/S	103. 1673. 220. 0.000894	101. 1630. 217. 0.096071	118. 1914. 220. 0.001022 0.004825 239. 3884. 217. 0.002092	440. 7145. 219. 0.003825

	V/OR MAT OWEG*R TIP4 PPH RPM	VKTS MTUN QPSF ALFS,U ALFS,C	BAR TEMP RH0100 L/DE L/D+R ANXL/R	LIFT DRAG SIDE PITCH YAW RULL	LIFT,R DRAG,R SIDE,R PITCH,R YAW,R ROLL,R	CLR/S,R CDR/S,R CYR/S,R CMY/S,P CMZ/S,R	HP TORQ J THRUST CP/S CP/S,R
16	0.2424 0.6715 627.9 0.5405 333.1	90.2 0.1310 25.0 10.0 10.9	29.78 104.0 0.2161 3.69 4.04	8972. 2317. -8. 1734. 105.	7533. 1751. 10. 14879. 7.	0.068552 0.015932 0.000094 0.166465 0.000116	31. 4 <b>96.</b> 224. 0.000251 0.004112
17	0.2264 0.7169 679.0 0.5845 360.2	91.1 0.1323 25.5 10.0 11.1	29.78 134.0 0.2161 3.83 4.12	11800. 2960. 188. 7988. 396. 5038.	10301. 2380. 207. 22245. 545.	0.080180 0.018521 0.001609 0.194973 0.002150	33. 482. 213. 0.000208
e I	0.2497 0.6550 668.8 0.5241 323.0	90.1 C.1309 25.0 5.0 5.3	29.78 104.0 0.2161 3.98 4.75	8438. 1424. 64. 6119. -198.	7651. 923. 68. 14638. -53.	0.074042 0.008931 0.000662 0.111838 0.000506	190. 3001. 216. 0.001662 0.003892
	0.6825 0.6825 609.8 0.5249 273.5	108.5 0.1576 36.0 5.0 5.0 0.0	29.78 105.0 0.2150 3.07 5.32	8115. 1615. 2968. 614.	7154. 917. 29. 13246. 356.	0.069378 0.338895 0.300379 0.197164 0.000497	142. 2311. 213. 0.001245
0 0 F	0.2°02 0.6778 592.1 0.5232 314.1	105.0 0.1546 35.8 0.0 0.2	29.96 76.0 0.2281 1.60 2.75	2524 2534 353 5576 334	2576. 215. 10. 6946. -597.	0.024990 0.092090 0.024646 -0.000280	232. 3884. 272. 0.002093 0.002119

HP TORQ J THRUST CP/S CPO/S,R	882. 14517. 218. 0.007816	512. 8393. 220. 0.004506 0.009187	324. 5274. 211. 0.002807 0.004684 343. 5586. 166. 0.002008	499. 8166. 133. 7.074461 0.007471
CLR/S,R CDR/S,R CYR/S,R CMY/S,R CMZ/S,R	0.131272 0.015558 0.003635 0.221195 0.001454	0.117088 0.015644 0.001782 0.205606 0.001012	0.084788 0.006269 0.001322 0.093852 0.093852 0.005979 0.07109 0.091436 0.091436	0.103872 0.707539 0.701295 0.117563 0.060718
LIFT, R DPAG, R SIDE, R PITCH, R YAW, R RUL, R	13546. 1605. 375. 25339. -4046.	12116. 1621. 133. 21804. -501.	3850. 654. 138. 20008. -510. -145. 8084. 736. 149. 18717. 232.	11173. 767. 132. 23174. -138.
LIFT JRAG SIDE PITCH YAW RCLL	15076. 2356. 364. 5691. -4106.	13620. 2365. 122. 3961. -311.	9355. 1324. 151. 12140. -391. 1037. 8676. 1931. 262.	11802. 1961. 144. 11351. -59.
RAP TEMP PH1100 L/DE L/DE ANXL/R	29.96 93.0 0.2210 2.99 3.16	29.96 96.0 0.2198 3.47 3.81	29.06 97.0 0.2194 4.06 5.42 -4.2 -7.0 9.2176 9.32 5.32	29.96 102.0 0.2157 3.94 5.87
VKTS YTUN QPSF ALFS+U ALFS+C	107.0 0.1572 36.1 7.5 8.5	107.0 0.1567 35.8 7.5 8.4	107.8 0.1577 36.3 2.5 3.1 0.0 142.6 0.2090 62.0 2.8	143.0 0.2087 (7.8 72.8 0.0
V/08 WAT CAFG#R P I P 4 P P R P	0.3003 C.68C7 601.7 9.5235 319.2	0.2949 0.64403 604-1 0.5242 320.5	0.2995 0.6842 60463 0.5765 0.5765 0.2467 0.7755 0.5775 0.5775	0.3992 0.7516 604.7 0.8220 320.8
	. 13	. 14	. 1 4 1 1 4 1 4 1 4 1 4 1 4 1 4 1 4 1 4	. 12
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P	182 941 10 10	9201. 2142. 358. 5362. 125. 8933.	9.95     13076.     11632.       94.0     2463.     1332.       2188     303.     314.       3.97     7328.     2581.       5.38     55.     32.       -6.5     3217.     1326.       95.0     2484.     1351.       2184     292.     303.       4.02     7065.     26639.       5.30     242.     208.	6.0 1213629 .95 11426. 9129 7.0 2855. 1640 175 -145117 -14600. 19149
V/FP VKTS  "AT HTUM  MEG*8 OPSF  TIPM ALFS,U  HP4 ALFS,C  PPW ALFS,C  PSI  147.2	12 0.2096 •4 62.7 C 26 2.5 •7 2.9 •5 0.0	140.9 244 0.2079 1.9 62.4 0 165 5.0 3.5 5.3	0.3941 140.9 20 0.7229 0.2071 0.2031 603.8 61.9 0.0 720.3 61.9 0.0 720.3 5.0 0.3960 141.2 20 0.3960 0.2073 0.2073 0.5235 5.0	0.0 142.4 0.2088 62.8 7.5

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TORG J THRUST CP/S	101. 1645. 172. 0.000884	392. 6422. 119. 0.033551 0.006973	405. 6606. 119. 0.003623	180. 3706. 232. 0.001613 7.006611	71. 1177. 229. 0.000632 0.004443
CLR/S, R COR/S, R CYR/S, P CMY/S, P CMY/S, P CMX/S, R	0.090341 0.016148 -0.001174 0.180147 -0.000309	0.084656 0.007622 0.003669 0.102459 0.001950	9.084655 0.007512 0.093965 0.101892 0.002206	0.107211 0.016695 0.002361 0.199839 0.002429	0.066537 0.012629 -0.000664 0.134519 -0.000612 0.002789
LIFT, R DRAG, R SIDE, R PITCH, R YAW, R POLL, R	9341. 1670. -121. 19720. 867.	8576. 766. 369. 22764. -536.	9575. 761. 402. 22914. -405.	11099. 1728. 244. 20018. 130.	6879. 1306. -69. 18660. -236.
LIFT ORAG SINE PITCH YAW ROLL	11645. 2887. -150. -4173. 1372.	9185. 2118. 382. 11501. -697.	9254. 2112. 415. 11578. -537.	12595. 2474. 234. 3408. 205. 1542.	8337. 2055. -78. 5711. -226.
BAR TEMP RHG100 L/DE L/n,R ANXL/R	29.95 97.0 0.2175 3.74 4.92 -10.1	27.95 104.0 0.2137 3.15 5.45	29.95 104.0 0.2137 3.15 5.42	29.97 77.0 0.2277 4.15 4.86	24.97 18.0 3.2272 3.67 4.52
VKTS MTUN QPSF ALFS;U ALFS;C	142.5 C.2090 63.0 7.5 7.9	160.6 0.2342 78.5 2.5 2.8 0.0	160.6 0.2342 78.5 2.5 2.8	105.3 0.1570 36.0 7.5 8.3	106.2 0.1581 36.5 7.5 8.0 0.0
VZDP TMEGATT TID#R RPRR RPRR	6.3963 0.7363 607.1 0.5273 222.1	C.4489 O.7559 603.8 C.5217 320.3 93.2	0.4471 0.7580 676.2 0.5238 221.6	0.2594 0.6812 592.8 0.5242 315.0	C.3017 5.6720 5.6720 0.5230 315.1
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VZCR MAT CVFC*P TIP4 RP47 0.2996	X F Q Q Q 4 R V V V V V V V V V V V V V V V V V V	B L C J X S S S S S S S S S S S S S S S S S S		ν φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ φ	CDR/S, CVR/S, CVR/S, CMY/S, CMZ/S, CMZ/S,	TONA 44
0.6(5) 590.0 0.5190 313.0 91.1	• m	- ~ ~ 4 1	5508 5508 2348 -132	1277	00104 19701 00221 00507	238. 0.002266 0.007119
0.2988 0.6763 591.0 0.5211	104.8 0.1557 35.4 7.5 8.4	74.97 30.0 0.2265 4.17 4.17	13356. 2557. 117. 2020. 760.	11869. 1821. 128. 19420. 2606.	0.116904 0.017798 0.001247 0.213838 0.002661	208. 2473. 239. 0.001886 0.007203
0.2946 0.6813 507.7 0.5262 317.1	104.3 0.1550 35.1 7.5	79.97 40.0 0.72.65 4.37 4.95	380 751 26 766 750 330	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13769 02220 00035 25651 30209 00278	187. 3105. 239. 0.001653 0.008193
0.2496 0.6561 596.8 0.5251	98.3 0.1311 25.2 2.5 3.3 0.0	29.92 30.0 0.2268 3.96 4.70	8936. 1708. -156. 10653. 2525.	8500. 527. -160. 17694. 2372.	0.081592 0.005057 -0.001531 0.084634 0.00327	338. 5614. 221. 0.002994 0.004256
0.2514 0.6534 595.1 0.522 215.7 91.9	98.6 0.1313 25.2 2.5 3.6	29.92 83.0 0.2256 3.99 4.59	11689. 1136. -141. 10922. 3609.	11219. 652. -144. 19383. 3458. 1103.	0.108912 0.006326 -0.701396 0.108714 0.001010	488. 8123. 219. 0.004381 0.005972

HP TPPO J THPUST CP/S CP/S	520. 8790. 248. 9.0046.81	493. 8146. 251. 0.004330	599. 9966. 252. 0.005362 0.011714 525. 8790. 280. 280. 0.004719	509. 8464. 280. 0.004512 0.007058
CLR/S,R CDR/S,R CYP/S,R CMY/S,R CMZ/S,P	0.115752 0.011635 0.003138 0.160857 0.000795	0.123751 0.017798 -0.003630 0.219600 0.000019	0.161634 0.025334 0.090034 0.298585 0.03747 -0.003485 0.127927 0.013401 -0.093644 0.180103 0.000728	0.103501 0.010180 -0.004537 0.142945 -0.000545
LIFT, R DRAG, P SIDE, R PITCH, R YAW, P ROLL, R	12074. 1214. -327. 18505. 6244.	12966. 1865. -380. 16154. 6878.	16692. 2616. 3. 23599. 6903. -628. 13237. 1387. -317. 19615. 5960.	10786. 1061. -473. 16759. 5842. 1449.
LIFT PRAG SIDE PITCH YAW PGLL	12889. 1722. -333. 7142. 6640.	14129. 2403. -394. 1695. 7413.	17909. 3163. -111. 8250. 7033. -504. 14071. 1899. 7930. 6350.	11588. 1571. -478. 5855. 6362.
PAP TEMP RH9130 L/DE L/DF AMXL/F	29.94 80.0 0.22.70 3.50 3.80	29.94 30.0 0.2270 3.34 3.51 -8.2	29.94 82.0 3.2261 3.33 3.46 -8.9 76.0 0.22.0 3.66 3.97	24.09 0.2282 3.36 3.67
VKTS MTUN CPSF ALFS,U ALFS,C PSI	88.1 0.1308 25.1 5.0 6.2 0.0	87.9 0.1305 25.0 7.5 8.8	98.4 0.1310 25.2 7.5 0.7 0.7 0.1311 5.0 6.3	88.2 C.1312 25.3 5.0 6.1
VZOR NAT CTG*P TIPN PPN	0.2440 C.6560 557.0 0.5252 316.7	0.2483 0.6569 558.3 0.5264 317.4	0.6536 0.6536 0.6526 0.5226 315.7 0.6538 0.6538 0.5227 214.0	0.2501 0.6557 0.6551 0.5245 315.7
	c L		PT 11	1

H	1080	J THPUST	CP/S	0 0/000	1 40 A 1 A 1		486.	7710	•0110	312.	J. C04529	0 007255	66316		4,04.	10027.	- 155.7	•016	0.005485	7,008118	44-00	
CLR/S,R	COR/S,R	CYR/S.P	AV/S.P		C4//00K	CMX/5,R	0.110322		01,2000	-0.903282	0.113987	436000	20000.•C	0.013152	0.112681	0.004538	86,000.0	-0.174628	0.113217	014001 0	01100010	0.01011
LIFT,	DRAG, R	SIDE	PITCH. 9		*AX**	POLL . R	11050.		672.	-329.	23340.		• 1 // (	-2698•	11456.	11	• COD	-471.	21208.	1603	1431	-2817.
1411	08.40	STOF	10110		3 X X	1 10 d	11685	• / [. ] • 7 1	- 7 P.G	-316.	11762	)	5537.	-3013.	12095	) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) ( ) (	• \$2 / 7	-453.	3604		• 905 G	-4701.
BAF	TF 4D	00.100.0		L/0£	4.0/1	ANXL /R	00	00.00	A3.0	0.2234	(C 7	J > • •	6.18	છે. લ	30.00	00.0	ت ن ن	0.222	2 H 2	) (C	5.59	-3.3
VK 1.5	W. T.		1047	ALF S, !!	At FS. C	ISd		T • 7 6 T	C-2107	4.4.1	+ u	. • >	5.9	C• C	1 6 7 1	1 • 2 • 1	0.2104	63.9	. u	• 1	σ•N	ر• ن
90 <b>/</b> //		- V -	# 9 i	MdIL	MOS	\$** C. C.	•	C-4042	70.7794	7 004	0 • 6 • 6 • 6	しむていつ	4,016	91.)		, Z.34 · C	0.7330	3 50 3		0776.0	376.0	0.30

## SECTION B

Tabulated Control and Loads Data

LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	0.170 0.222 0.232 0.390 0.392	0.444 0.244 0.244 0.444 0.444 0.444	1.621 0.373 0.419 0.482	1.428 0.666 0.487 0.569 0.569	0.445 0.445 0.445 0.457
URSB MN URSB OS GP VTAC GH LTAC SP LTAC	2123• 1477• 0•261 0•235 0•235	2770 2365 0.443 0.282 0.546	2124. 2829. 0.450 0.314 0.554	3613. 4671. 0.662 0.464 1.099	4320. 4917. 0.176 0.454
URRPL CS URBPL OS LERPL OS LAYPL OS LAYPL OS	266324 66934 6690	335 284 2044 204 215	2222 2222 2223 223 234 234 234	540. 637. 513. 258. 275.	657. 657. 489. 442.
1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1197.	1004 1004 1005 1005 1006 1006	2070. 1302. 1201. 191.		01440 01441 01441 01441 0144
URCB C. URM1 C. URM1 C. URM2 C. URM2 C. URM3 C. URM6 C. C. M1 C. C. C. M1 C.	376 1650 2032 2366	37!1. 1014. 2017. 215.	3.22 3.23 1.23 1.03 2.44 2.44 2.444	2006 2006 2006 2006 2006	50 CCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC
NA TREAT NAME TO A TREAT NAME TO A C		20 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		007.1. 047.1. 044.1. 044.1.	0.00000 0.00000 0.00000 1.10000
	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0			# # # # # # # # # # # # # # # # # # #	
44.0 A 12.0 A 12	reserved remaining	10 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	#2000 #2000 #1111		
222 24,7 44,7 47,0%	21 2.65.7) 0.2 2.24:0 0.3		2 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5		

LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	1.862 0.508 0.325 0.275 0.275	1.860 0.515 0.515 0.333 0.233 0.275	1.686 0.511 0.279 0.379 0.226	3.799 0.572 0.356 0.406 0.219	1.752 0.798 0.420 0.404 0.258
UASB MN URSB OS 3R VTAC SR LTAC GB LNAC	3251. 2475. 0.373. 0.252. 0.552.	3276. 2513. 0.255 0.209	3568- 2717- 0.421 0.263 0.621	4114. 25592. 0.605 0.272	26850 26810 00074110 100744
URRPL OS 1987PL OS 1987L OS 1987L OS 1887L OS 1887L OS	25.0. 421. 200. 203. 218.	354. 584. 413. 202. 201.	22.4 27.2 21.4 21.4 21.4 31.7 31.7	537. 586. 271. 276.	594. 632. 317. 249.
7		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	6450 4450 4450 4450 400 400		3724. 5777. 5032. 1995. 1995.
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LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	1.27¢ 0.500 0.500 0.420	1.730 0.768 0.550 0.517	1.647 0.440 0.271 0.282 0.256	1.662 0.406 0.433 0.360 0.315	0.00 0.00 0.00 0.00 0.00 0.00 0.00
URSB MN URSB OS GR VTAC GB LTAC	3506. 3227. 0.435 0.345	3913. 6972. 0.737 0.236	3575. 2269. 0.373 0.257	3563. 1508. 0.371 0.405	1927. 2213. 0.278 0.320 0.197
URRPL OS URYPL OS URBPL OS LRRPL OS LRYPL OS IRGPL OS	424. 491. 508. 244. 258.	509. 627. 574. 254. 261.	369. 430. 425. 195. 209.	453. 441. 421. 226. 240.	256. 259. 258. 191. 196.
LKKWI CS LKWI CS LKWI CS LKWI CS LKWI CS	1579. 2079. 1339. 822. 397.	2255. +040. 2090. 1021. 375.	13415 13415 1484 1484 1484 1484	23.00 23.00 20.00 20.00 20.00	2000 1000 1000 1000 1000
URC3 05 UPN2 05 URN2 05 URN3 05 URN3 05	5359. 1845. 3. 1176. 3737.	1936. 2690. 26. 1566. 3913.	17907. 1438. 2. 526. 2546.	4 8 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2 4 2	0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
URREL MN URBEL MN URBEL MN LRRFL MN LRSPL MN	20.2 20.2 1.20.2 1.90.4	8 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	**************************************	
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THETAP A19 A19	0.56 0.56 0.56 0.57 0.57				
ALPH VKTS	21 16 0.6715 10.0 0.2424 00.2	11 12 12 12 12 12 12 12 12 12 12 12 12 1	1		5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5. 5

LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	2.910 0.383 0.430 0.608 0.414	1.855 0.593 0.413 0.722 0.534	3.407 0.842 0.916 0.997 0.571	3.940 1.048 0.934 1.089	2.502 0.800 0.556 0.612 0.447
URSB MN L URSB CS CH VTAC GB LTAC GB LNAC	4091.3856. 0.493 0.517 0.518	4815. 2571. 0.772. 0.632. 0.788	5279. 4724. 0.855 0.851	5775- 3609- 1-020 1-194	5000. 4310. 0.795 0.620 1.052
LERPL US COYPL US COBOL US LARPL US LAYPL US	338. 411. 382. 218. 200.	473 558 525 310 297	667 - 752 - 654 - 535 - 463 - 467 - 657 -	899. 851. 781. 554. 653.	488. 529. 305. 305. 284.
LENGE CON CONTRACT CON CONTRACT CON CONTRACT CON CONTRACT	2734. 2520. 1340. 701. 262.	5.45.45.45.45.45.45.45.45.45.45.45.45.45	7 7 9 3 3 3 3	7040. 7250. 4436. 5110.	2004 2006 1809 1839 1848
URGE COUPAIN C	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		23.800. 66.22. 67.45. 25.15. 35.71.	C ≠ ≠ : 0 · 0 · •	28344. 2360. 1218. 806. 3973.
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LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	3.290 0.963 0.949 0.936 0.792	2.378 1.035 0.518 0.626 0.536	2.114 6.415 6.410 0.613 0.474	3.512 0.778 0.584 0.684 0.764	3.928 0.667 0.613 0.574 0.75
URSB MN URSB OS 4GB VTAC 6B LTAC 6B LTAC	6002. 5571. 1.010 1.265 0.804	5973. 3345. 0.953 0.670	5547. 0.522. 0.583. 0.599	5620. 3941. 0.630 0.984 0.643	612 6809 6809 6843 6843
URRPL OS URYPL OS URBPL OS LRRPL OS LRYPL OS LRGPL OS	575. 669. 614. 825. 796.	580. 669. 495. 480. 511.	4444426. 4266. 2324.	2847 406 2346 250	4 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8
LKNI LKNI LKNI LKNI LKNI LCS LCS LCS LCS LCS	10523. 7004. 4065. 3277. d78.	7255. 4428. 5097. 2259. 1045.	4440 4400 4400 4400 4400 4400	2034. 2054. 2058. 1057. 23.	4795. cd+5. 4470. 2750. 726.
URCB 05 URN2 05 URN3 05 URN3 05 URN5 05 #19 05	29289. 5957. 4060. 2804. 5684.	33986 33988 1491 1461	4	4 2 4 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	74410. 7338. 4700. 7356.
LRRPL MN URYPL MN URAPL MN LRRPL MN LRYPL MN LRYPL MN	1111 445 805 805 805 805 805 805 805 805 805 80	1,450 1,474 1,00 1,00 1,00 1,00 1,00 1,00 1,00 1,0	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 6 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6. 6
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LVF VTAC HST VTAC #1J VTAC #2J VTAC LAS LTAC	3.664 0.710 0.629 0.574 0.727	3.863 0.932 0.765 0.616	6.115 0.503 0.573 0.631	4.533 0.633 0.536 0.621 0.673	6.50 0.630 0.830 0.830 0.683
URSB MN URSB CS GB VTAC GB LTAC	6031. 4767. 0.728 0.956	1482. 6763. 0.756 1.229 0.998	2184. 5850. 0.641 0.951	2405. 4901. 0.758 0.912	2022- 5789- 0-867 1-078 0-860
URYPL OS URYPL OS UFBPL OS LERPL OS IRYPL OS IRSPL OS	389. 516. 455. 264. 271.	448. 462. 451. 404. 364.	411. 500. 507. 346. 350.	454. 548. 525. 369. 421.	603. 715. 635. 333. 350.
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1908 C. John C	2052 6720 2615 7185 740	64.51. 64.51. 64.55. 64.55. 66.64.	14162. 6916. 4293. 2477. 4440.	16135. 9048. 5766. 3421. 4493.	19799. 6653. 4076. 2497. 33300.
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LVF VTAC FST VTAC #1J VTAC #2J VTAC LAS LTAC	4.544 0.510 0.576 0.869 0.729	5.772 0.887 0.618 0.685 0.695	5.866 0.914 0.646 0.649	3.091 0.599 0.483 0.517 0.410	1. 0.000 0.000 0.000 0.000 0.000 0.000
URSB MN URSB CS GB VTAC GB LTAC GB LNAC	2031. 5525. 6.809 1.116	2424. 5412. 0.670 0.991	2412. 4671. 0.801 1.025 0.727	1523. 2914. 0.643. 0.521.	1074. 6190. 0.474 0.567 0.936
URYPL OS URYPL OS URBPL OS LRYPL OS LRYPL OS LRGPL OS	601. 714. 636. 268. 328.	535 635 630 782 391	569. 663. 667. 393. 407.	518. 539. 742. 287. 292.	40400000000000000000000000000000000000
LKCB CS LKA2 CS LKA2 CS LKA3 CS LKA3 CS	1335. 1532. 2445. 3987. 1224. 15.	5062. 8063. 3277. 3275. 1017.	7544. 75946. 79946. 7055.	4201. 3754. 2505. 1367. 010.	20037 20047 15505 15505 11
URCB GS URN3 GS URN3 GS URN6 GS	15292 64156 2996 3270 8336	27581. 1481. 3747. 22. 3897.	28771. 2936. 23860. 2234. 2666.	2 4 4 6 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2061. 4571. 3240. 2217. 4208.
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LVF VTAC FST VTAC #1J VTAC #2J VTAC LAS LTAC	2.322 0.606 0.631 0.523 0.482	2.220 0.483 0.463 0.454 0.363	2.161 0.471 0.460 0.520
UPSB 4N URSB CS 68 VIAC 68 LTAC 69 LNAC	1739. 4405. 1.064 0.486 1.038	1866. 2647. 0.660 0.619	2232. 2223. 0.518 0.649 6.796
URRPL OS URYPL OS URBPL OS LRYPL OS LRYPL OS	652. 518. 293. 306.	536. 612. 595. 295. 281.	653- 615- 334- 333-
LKNY CC LKNY CC LKNY CC LKNY CC CC CC	5704. 5517. 1740. 708.	446.	4430. 11571. 1685. 4774. 525.
Canada Senta	4551. 3069. 1242. 1309. 5294.	4347. 4947. 3102. 1901. 4256.	10811 7384 4754 189
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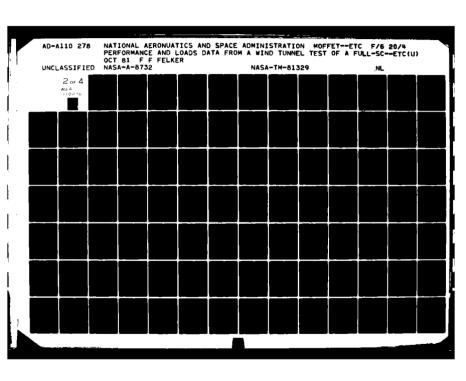
#1J VTAC #2J VTAC	0.358	0.376	0.810	0.492	0.336 0.358	0.470	0.440	0.318	0.325	0.559
V TAC V TAC	2.362 0.342	2.110 3.348	3.930 0.824	J.781 V.564	1.435	1.599	i.751 0.513	1.811	i • 726 J • 601	3.267
LVF	70	Ν̈́O	mis ,	33	40	40	નં છે	40	નં ગે	w 3
GB LNAC	0.608	0.785	1.470	0.511	0.613 0.390	0.362	0.799	1.018	1.022	1.265
GB VTAC GB LTAC	0.36c 0.635	0.448 0.686	1.128	0.645 0.646	0.677	0.630 0.498	0.415	486.0 4868	0.645	J.00.C J.744
L KCB 05 L KN1 05 #20 05	2212. 7534. 38.	3076. 9156. 34.	4927. 10641. 66.	2012. 4949. 84.	1946. 5322. 52.	1988. 5202. 30.	2906. 9934. 24.	5512. 5877. 22.	3541. 9837. 75.	5514. 11678. 55.
URCB 0S URNI CS #19 CS	2731. 5731. 29.	3487. E136. 35.	4793. 11101. 50.	5280. 6329. 71.	6450. 6058. 51.	7089. 6945. 28.	4579- 13493- 22-	9042. 9121. 29.	5052. 10324. 73.	5033. 12473. 53.
RCB MN KKNI MN #20 MN	4165. -6798. 164.	4256. -2677. 235.	4808. 3462. 453.	4168. -7602. 249.	4477. -6063. 240.	4766. -5131. 226.	4509. 58. 206.	4368. -349C. 233.	4707. -2358. 214.	5012. 5213. 250.
CECB MA UNI MA # I G MA	4795. 2773. 126.	4716. 4451. 132.	3837. 7517. 432.	4659. 6090. 219.	4662. 0128. 209.	4751. 7503. 205.	4098. 7575. 211.	4909. 0821. 217.	5045. 7511. 251.	5c14. 7992. 255.
4AT V/UK V <ts< th=""><td>0.6561 0.2496 80.3</td><td>0.6534 0.2514 33.6</td><td>0.6558 0.2505 83.05</td><td>0.5560 0.2497 33.6</td><td>0.6557 0.2496 34.4</td><td>C. 6575 C. 2+67 33 • 1</td><td>0.5046 0.2504 0.33.4</td><td>0.50 0.24 0.44 0.44</td><td>0.0000 0.0000 0.7000</td><td>0.00 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0</td></ts<>	0.6561 0.2496 80.3	0.6534 0.2514 33.6	0.6558 0.2505 83.05	0.5560 0.2497 33.6	0.6557 0.2496 34.4	C. 6575 C. 2+67 33 • 1	0.5046 0.2504 0.33.4	0.50 0.24 0.44 0.44	0.0000 0.0000 0.7000	0.00 30 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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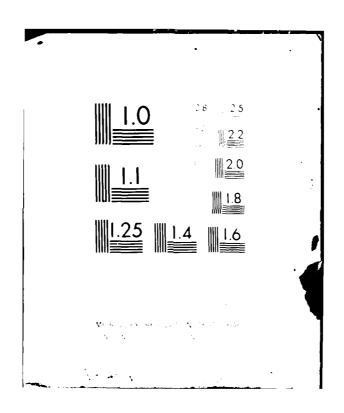
VIAC #13 VIAC VIAC #23 VIAC	1.775 0.500 0.560 0.581	1.375 3.367 0.662 0.c66	0.199 0.610 0.867 0.658	7.230 0.689 1.154 0.692
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		6 <u></u>		

SECTION C

Detailed Loads Data

= 0.0210 = 0.0006	8. S.	•	7	-1632-9	189.5	245.8	32.4	54.0	15.1	-23.2	-93.8	22.1																
CAY/ 5, R CAX/ 5, R	. 533		-617.3			•	•	24.5	-40.4	30.5	71.8	26.6																
( =0.02560 ( =0.00131	BENDING MCMENT . 3K . SIN	:	^ u	-247.5	27.6		-37.6							RUTUR	STRESS	v I v			-183.9	-112.4	9.44-	97.3	40.7	18.6	72.4	-57.3	37.0	56.67
CLR/5, R CUR/5, R	AL BENDING • 3K	) )	-2955-2	158.7	50.5	123.7	17.0	1.0-	-25.5	7.7	-2.8	7.6-		UPPER	SHAFT	503		~	-1146.0	-355.	ე•8−	1.961-	-197.2	71.6	45.0	51.0	19.7	-15.9
5.0 0.002247	BLADE NURMAL		ć	000	0	0.0	0.0	o. 0	0.0	0.0	0.0	0.0		KUTOR	K LCAD	SIN			189.1	25.5	10.4	- 30.4	-22.1	17.7	15.2	18.2	-0-1	3.1
AL FS.C CP/S =	UPPER ROTOR •28 60.5		O 0		0.0	o.°0	0.0	0.0	0.0	0.0	0.0	0.0		UPPER KI	PITCH LINK	crs		-136.9	-50.8	-23.6	-53.2	3.3	-25.8	-5.1	5.0	-5.4	-3.5	8.1
	Z			-674-3	34.6	-171.7	-18.6	-80.1	-87.9	48.2	138.4	-53.1		EDGEW1SE	ING MCMENT . IR	SIN			0.0	0.0	0.0	0.0	0•0	0.0	0.0	0.0	0.0	0.0
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0.0210	260.3 260.3 1.0.5
CMX/S,R #	CUS
( =0.00131 ( =0.00131	BENDING MOMENT  - 3R  - 3R  - 3R  - 79 - 4  - 119 - 5
CLR/5, R CDR/5, R	
0.002247	SIN 524.4 518.6 -70.7 -160.3 43.0 199.8 69.7 -4.5 29.6 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 12.9 13.0 11.1 1
ALFS,C CP/S =	-28 SI -7645.3 -280.4 524.8 5229.8 5229.8 5229.8 518 97.2 -100.4 -166.5 10.4 -166.5 10.4 -166.5 10.4 -166.5 10.4 -166.5 10.4 -166.5 10.4 -166.5 10.4 -166.5 117 -24.9 117 -24.9 117 -24.9 117 -24.9 117 -24.9 117 -24.9 117 -24.9 117 -24.9 110.5 -20.1
*K = 605.6 00 = 0.2200	SIN 527.4 813.7 -61.4 -61.4 -61.4 -61.4 -61.4 -61.4 -61.4 142.9 142.9 142.9 16.3 19.4 19.4 -710.2 -710.2 -710.0 -75.
PUINT 6 89.3 UMEG*R 0.249 RHUIOO	-11268-2 -489-2 213-9 159-4 290-4 -271-3 -140-3 193-2 193-2 193-2 193-2 -53-1 55-0 CGS -4512-5 -17-8 -22-0 4-3 -22-0 4-3 -13-3
PUN 21 VKTS = ' V/OP =	HARMENIC 34 4 7 6 5 7 8 9 5 1 0 9 6 1 7 8 4 7 6 5 7 8 9 5 1 0 0 1 1 0 0 0 1 0 0 0 1 0 0 0 1 0

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FUN 21 VKTS = V/OR =	PLINT 89.3 0.249	6 UMEG#K : RHJLOO :	= 605.6 = 0.2200	6 ALF	S.c = 0.3 S = 0.002247	0.3 CLR/S,R 247 CDK/S,R	=U.02560 CM =U.00131 CM	CAY/S, K = 0.0210 CAX/S, R = 0.0606
	UPPER	ROTOR BLADE	E NORMAL	BENDING 1	MUMENT 68	OR EDGEWISE BENDING . IK	UR PITCH	UPPER KUTOK SHAFT STRESS
S			<u>د</u> ا		•			
0.00	<b>4</b> -	95	o.	-2166.	247.	•	8	3,15.
1.2	-5	5485.	• •	-2515.	59.	• •	-707-	492.
2.5	ì	32	• • •	-2884.	81.	• •	4	686.
3.7	-	7229.	٠°	-3184.	.91	•0	-69-	1063.
5.0	ī		•0	-3410.	-120.	•°	37.	1436.
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7.5	1	~	• •	-3748.	-2160.	•0	148.	1352.
8.7	-	7397.	•0	-3716.	-2631.	•o	78.	1128.
0.0	7	5	•0	-3676.	-3189.	•0	23.	2190.
1.2	-6	6493.	•0	-3702.	-3128.	•o	31.	2579.
2.5	7	5945.	• •	-3687.	-2562.	•0	15.	3028.
23.7	7	-6807.	•0	-3614.	-2289.	• •	-37.	3208.
5.0	ĭ	5286.	°°	-3543•	$\sim$	•0	-34.	2935.
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168.7	1	5857.	•	-3259.	-2208.	• <b>0</b>	-43.	3015.
80.0	ĭ	-6386•	• •	-3184.	-1815.	•0	-31.	2958•
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02.5	ĭ	5781.	<b>.</b>	-3269.	-1101-	•0	-158.	2973.
13.7	ĭ	-6885.	•0	-3268-	-771.	• •	-544.	3131.
25.0	ĭ	-69869-	•	-3128.	-286-	•0	-568-	3133.
36.2	-		• 0	-2970.	-51.	<b>.</b>	-300•	2993.
47.5	7	5861.	• 0	-2791.	-	•0	-721.	2930
58.7	ï	•	•	-2525.	37	•0	-526.	2843.
70.0	ï	5589.	•	-2269.	0	•0	-760	2458.
81.2	1	5296.	• •	-2127.	55	• •	-	2031.
92.5	1	5134.	· 0	-2102-	16	•0	-363.	1992.
03.7	1	5418.	•0	-2172.	2355.	•o	-365.	2152.
15.0	1	5531.	• ວ	-2204•	33	• •	Ø	2040.
326.25	7-		• •	-2052-	9	0.	-572-	1513.
37.5	7-	4311.	•0	-1870.	30	0	-	
48.7	9-	4412.	• •	-1911.	$\circ$	• ວ	-334.	<b>3</b>

ŧ

VKTS = V/OR =	85.5 0.249	OME RHU	OMEG#R = RHUIJO =	605.6 0.2200		AL FS,C = CP/S = 0.0	0.032247	CLR/S,R CUR/S,R	=0.02560 =0.00131	CAY/S,R =	0.0210
	LUWER R	UT UR	BLAUE N	NCRMAL	BENDING	G MUMENT	7 87 2 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	LK EDGEWISE BENDING JR	LR PITCH	# C	
S	•	4	,	•	-	•	)			2	
000	-134	83	-9130	•	-6092	-1167.		-4402.	-2	.81.	
88.7	-136	91	-939	•	17	118		-4270.		332.	
77.5	-176	01	-895	•	_	-1250.		-3484	<u> </u>	-354.	
•	-109	.86	-3018	•	-5337.	-1327.		-3429.	7-	-288.	
55.0	-105	79	-7346	•	-5073.	-1323.		-4366.		201.	
43.7	-108	33	-7374	•	-5066.	-1198.		-4973.	7	-195.	
32.5	-113	3	-7654	•	-5121.	-1049.		-4436.	~-	-237.	
21.2	-109	in	-161		-5074.	-993.		-3714.	7-	.252.	
10.0	-103	O	-7314	•	-4915.	-1029.		-4013.	7-	228.	
98.7	C01-	30	- 708	•	-4770.	-1036.		-4925.	7	-172.	
87.5	-132	32	-7030	•	-4727.	-1108.		-5097.	1	-86-	
76.2	-105	1 5	-709	•	-4737.	-1073.		-4353.	1	.54.	
65.0	-109	90	- 7262	•	-4782.	-666-		-3967.	1	.43.	
53.7	-112	8	-7530	•	-4913.	-929.		-4624.	j	-34.	
42.5	-114	75	-1166	•	-5028.	-875.		-5294.	J	.41.	
31.2	-116	36	<b>-780</b> C	•	-4965.	-814.		-4897.	1	.67.	
20.02	-114	36	-766	•	-4809.	-161.		-4774.	1	-72.	
08.7	-110	2	-7497	•	-4720.	-159.		-4355.	1	-67.	
97.5	901-	:0	-1294	:	-4624.	- 784 -		-5376.	1	-81.	
~	901-	7	-7082	•	-4446.	-763.		-5687.	•	- 64.	
0	-136	-0	-6983	•	-4334.	-702.		-4976*	1	-96-	
7.	-106		-7005	•	-4385	-659-		-4431.	-	108.	
3	-101	4	-7106	•	-4486.	-636.		-5018.	1-	-101-	
.2	-109	35	-7269	•	-4541.	-617.		-5671.	1	.81.	
0	-109	-4	- 7309	•	-4547	-647.		-5237.	1	-82.	
-	-105	30	-7126	•	-4556.	-730.		-4292.	•	-97.	
.5	101-	99	-7136	•	-4671.	-792.		-4116.	1-	-129.	
56.2	-116	ဘ	-7637	•	-4969.	-816.		-4850.	7-	-204.	
45.0	771-	30	-8156	•	-5263.	-876.		-4983.	7-	-288.	
33.7	-171	۵	-8236	•	-5371.	- 966 -		-4037	E-	312.	
22.5	-175	18	-8215	•	-5439.	-1134.		-1301-	7-	. 84 .	
	-171	18	-8562		-5716.	-1154.		-3648.	7-	:64.	

196 CMY/5,R = 0.1112 903 CMX/S,R =-0.0053	COS 51N COS 51N 117.9 -1092.7 -12.6 -312.9 -256.2 142.5 -348.8 330.2 204.3 -214.1 35.9 192.5 -29.2 -17.2 27.7 18.3 -88.0 6f.6	
K =0.07196 R =0.00903	933.4 SIN 933.4 SIN 583.6 214.7 172.7 -194.2 -10.4 -79.2 -53.9 64.9 9.6 17.2 -4.7 8.2 -4.7 8.2	RUTUR STRESS 1313.7 1313.7 143.3 -63.6 -245.9 -118.3
CL K/3, K CDR/3, R		UPPER SHAFT COS -2620.8 -579.3 -279.3 -279.3 -279.3 -279.3
= 5.8 0.001602	SIN 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	RUTOR NK LCAD SIN 186.3 17.6 -31.4 -33.1 -42.0 26.6 57.8
ALFS+C CP/S =	UPPER KGTCK .2F .2F .0.0 .0.0 .0.0 .0.0 .0.0 .0.0 .	UPPER RU CC5 -195.3 -94.6 -30.1 -43.9 4.7 -65.3 -14.3
UMEG*R = 602.8 RHGIOÙ = 0.2193	118 SIN SIN 1060.7 -492.3 115.5 -278.0 239.2 -279.0 158.2 -54.1 -15.4	ROICH EUGEWISE NG MOMENT . LR S SIN .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0
PCINT 7 89.4 UMC 0.250 RHL	605 -3989.4 722.0 445.1 65.4 328.7 -312.4 61.7 -43.8	UPPER ROTO BENDING N COS 0.0 0.0 0.0 0.0
PIN 21 VKTS = V/OP =	HARMONIC 0 1 2 3 4 4 5 6 7 10	100 HARMONIC 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0

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= 0.1112 =-0.0053	~	NIS		285.0	-18.2	-10.6	-19.0	6*7-	-45.6	-p.1	-3.5	-17.9	0.1																
CMY/S,R = CMX/S,R =	89•	SOO	7-112-	10.1	-70.3	19.5	-58.5	13.7	4.6-	-27.3	6.0-	-6.4	0.9-																
=0.07196 =0.00903	MUMENT	SIN		334.3	46.8	-43.9	18.0	16.4	78.4	-37.0	12.6	5.2	1.1																
CLK/5, R CDR/5, R	BENDING MUMENT	cus	-1152.1	-778.1	-11.1	12.0	86.9	-30.5	43.6	28.8	8.1	4.0	9.1																
5.8	BLADE NORMAL	SIN	'	192.8	m		7.3	23.9	195.7	-99.5	4.0	36.3	-13.8		TOP.	LGAD	SIN			107.6	1.9	-20.3	4.2	-7.6	1.0	-11.4	7.3	15.8	-25.4
ALFS.C CP/S =	LOWER ROTUR	crs	2004. 2	-1283.2								8.03	23.1		LCWER ROTOR	PITCH LINK LEAD	cus		-103.4	-133.1			4.4	3.3			5.6	13.5	-4.C
0*R = 602.8 100 = 0.2193		NIS	•	-174.3								4.	13.1		ROTOR FOCEWISE	8	; ! !			-603.4	-114.2	45.8	7.1	-13.4	-18.1	-443.9	18.7	14.B	8•6
PUINT 7 89.4 UMEG*R 3.250 RHULOU	8.7	003	0 0 798 -	-1469	152.9	37.0	296.5	1-87-	41.9	107.8	8.58-	47.8	64.2		LOWER ROTO		CCS		8.6664-	1274.7	-12.2	-5.0	1-16.7	59.9	-37.2	464.7	0.4-	3.5	6.4-
HUN 21 VKTS = V/GR =			HAPMONIC	· –	. ~	· ~	•	· <b>I</b>	٥	7	- 50	• •	01	10	01			HAR MON IC	0	-4	2	~	4	2	•	1	<b>6</b> 0	6	10

things to the

	TNIDG	7		,		1	a u	3 3 3 5		7	۱	
VK   VK   VK   VK   VK   VK   VK   VK	3.250	CMEC*R RHU100	n "	0.2193	8 ALTS#U	11	5.00100.0	CDR/3, R	=0.000.0= =0.00903	CMX/S, F	- ~-	u m
	UPPER	RUTUR BLADE	106	NCRMAL	BENDING MCMENT	MCMENT	C. Y.	UK EDGEWISE	UR PITCE	I		¥
				2£		. 6K	BENL	BENDING . LK	LINK LUAD	ΑU	SHAFT STRESS	S
PSI												
0	-20	655.		•	-1105.	934.		•		.23.	-433	
.2	-29	03		•	20	1138.		၁	-5,	40.	57	
5	-28	86		•0	-1393.	833.		ċ	6-	519.	91+	
. 7	- 3	033.		•	-1414.	446.		• •	£-	348.	496	•
3	-33	S		•	-1476.	450.		3	-177	77.	1796.	
2	-35	518.		•	-1638.	190.		3		-19	7147	
8	-3.	580.		•	-1874.	-435.		•	7	89.	0605	•
78.75	-34	490.		•	-1916-	-1073.		ż	7	46.	~	•
0	-3,	140.			-1804-	-1603.		• •	ľ	36.	9195	
01.2	-26	941.		•	-1755.	-1818		ဒ်	7	113.	9164	•
5	-29	930.		• •	-1897.	-1420		• •	•	37.	1995	
23.7	- 35	542.		•	-2193.	-693.		၁	1	11.	6538	
0	74-	294.		•	-2330.	-382.		•	•	36.	6054	
146.2	04-	035.		•	-2002-	-913.		o	•	13.	1155	•
.5	-2	2765.		• •	-1814-	-1771.		• •	1	-37.	4 748.	•
168.7	-2-	475.		•	-1892.	-1926.		•0	·1-	22.	1614	•
0.0	-39	362.		•	-2228.	-1270.		ċ	7	54.	8 7 9 7	
1.2	-5	257.		•	-2513.	-653.		• •	-152	52.	9150	•
ď	-588	883.		•	-2820.	-346.		•	7	-128.	7944 740	•
3.7	79-	.8079		•	-2868-	-159.		•	ĺ	-87.	3701	•
5.0	-5	-5985-		•	-2751.	-334.		•	-2-	-707-	3783	
6.2	-5	381.		•	-2636.	-919-		•	-430	30.	3595	•
7.5	-5	346.		•	-2515-	-228.		• •	-442	45.	7877	
8.7	15,	499.		•	-2342-	561.		ဒ်	767-	.76	2486	•
0.0	15-	161.			-2214.	1126.		• •	-2	8.3.	~	•
1.2	-50	030.		•	-2107-	82		• •	· - 3	368.	-	•
2.5	-51	184.		•	-1922.	19		• •	£-	σ	845	•
3.7	740	574.		•	3	9		• o	7-	30.	_	•
5.0	-38	821.		•	9	24		• •	4-	2	-389	•
5.2	<u>.</u>	384.		•		1936.		ċ	-3		67	•
7.5		980.		• •	O.	41		•		$\sim$	-43	•
8.7	-2	561.		•0	01	916		°	-3	94.	-376	

RUN 21 VKTS =	POINT 89.4	7 CMEG*R	H		н	CLR/S,R	=0.07196	MY/S,R = 0.1112
~	3.250	KH0100		3 CP/S =	= 0.031602	CUR/S.R	=0 •00 <del>0</del> 0 =	CMX/S,R =-0.0053
	LUWER RO	RUTUR BLADE	JE NURMAL	BENDING MOMENT	CMENT •6R	LR EDGEWISE BENDING • 1R	LR PITCH	
S		<u>.</u>	ı		! !			
0.0	)94-	2.	.851.	-1807.	-667.	-3140	-797.	
8.7	744-		·	-1831.	-673.	-3929•	-239.	
7.5	-416	7.		-1742.	-101-	-4727.	-243.	
5.9	-317	4.		-1401-	-763.	-+624•	-300.	
5.0	161-	94.		-1052.	-196.	-4281.	-235.	
3.7	-20	36.		-970-	- 697 -	-4701.	-119.	
	-278	35.	-1559.	-1020-	-554.	-5813.	-137.	
1.2	-23(	.10	1604.	-927.	-554 •	-6225	-128.	
0.0	101-	•0•	-942•	-656-	-663 •	-5714.	16.	
8.7	-5.	. AC	-323.	-355.	-715.	-5449.	83.	
7.5	-8-		-260.	-209•	-677.	-6210.	67.	
6.2	.F1-		-544•	-300-	-595-	-1014.	95.	
5.0	-181		-860.	-463.	-419.	-6648	87.	
153.7	165-		1054.	-501-	-355.	-5715-	13.	
2.5	-25		1125.	-455.	-260-	-5671.	28.	
131.2	56		1210.	-455.	-164.	-6467	63.	
0.0	-59,		1373.	-517.	-153.	-6703.	<b>&amp;</b>	
8.7	-31		1523.	-587.	-140.	-5884	-7-	
7.5	-3356-		1600.	-629-	-145.	-5124.	30.	
6.2	-34		1689.	-693.	-154.	-5369.	-10.	
5.0	-38.		1951.	-895.	-162.	-5905.	-65.	
3.7	644-			-1209.	-180.	-5485.	-30.	
2.5	-50	۲•		-1461-	-211.	-4364.	-37.	
1.2	-536	•		-1611.	-253.	-3924.	-126.	
0.0	-5279	9.		-1712.	-339.	-6440	-907-	
8.7	14-	•		-1729.	-460.	-4676.	-235.	
7.5	755-	472		-1718.	-617.	-1930.	-203.	
56.2	-51(	•		-1844.	-577.	-3115.	-176.	
45.0	7	· •	3357.	-2059.	-486.	-3280.	• 447-	
33.7	-54	•	3540.	-2141.	-524.	-3997.	-303.	
S.	6	9•	3268.				-254.	
11.2		•	2984.	-1878-	-675.	-3363.	-230.	

	= 0.1366 =-0.0050 -454.7 -187.4 101.5 375.9 -296.6 239.6 -42.1 14.4 56.1	CMY/S, R CMX/S, R CGS 841.7 891.7 695.1 -342.8 -342.8 -2411.6 227.1 52.7 -52.4 66.0	=0.09316 =0.01058 MUMENI 958.1 -102.9 -113.7 -21.9 -11.9 -0.2		BLADE 0.0 0.0 0.0 0.0 0.0 0.0	ALFS, C CP/S = CP/S = C	UMEG*K = 604.9 RHJ10U = 0.2185 a.1K SIN 2 2632.2 0 -275.9 8 155.2 5 -342.0 4 326.4 1 -314.7 7 98.5 0 -38.4 8 -173.5	90.0 UH 0.251 Rh -1977-1 -296-2 685-0 12-8 385-5 -333-4 69-1 5-7 -101-0 80-8
### OPPER KOTCF BLADE NORMAL BENDING MUMENT  #### OF PRINCE BLADE NORMAL BENDING MUMENT  ###################################			STRESS STRESS SIN 2282.0	UPPER SHAFT COS 124.2 521.1	0TOR K LUAD SIN 213.3	ROINK	UK EUGEWISE MUMENT •IR SIN 0.0	UPPEK ROTO BENDING COS COS 0.0
LOPPER FOTCE BLADE NORMAL BENDING MUMENT			(A) 27	UPPER SHAFT CGS 124.2	OTOR K LCAD SIN 213.3	I KO	UK EDGEWISE MOMENT .IR SIN	
**************************************			RUTUR STRESS SIN		OTOR K LUAD SIN	UPPER RO PITCH LINK COS	UK EDGEWISE MOMENT .1R SIN	<b>-</b> □
### OFFER FOTCF BLADE NURMAL BENDING MUMENT ####################################			RUTUR STRESS SIN		OTOR K LOAD SIN	UPPER RO PITCH LINK CUS	UK EDGEWISE MOMENT .IR SIN	<b>→</b> :3
LES SIN COS SI			RUTUR STRESS		OTOR K LOAD	UPPER RO PITCH LINK	UK EDGEWISE MOMENT .1R	=
OPPER KOTCF BLADE NURMAL BENDING MUMENT  SIN CCS SIN CUS  7.1  6.2  6.2  6.2  6.2  6.3  6.3  6.4  6.5  6.0  6.0  6.0  6.0  6.0  6.0  6.0								
SIN CCS SIN CUS SIN CUS SIN CUS SIN CUS SIN CCS SIN CCS SIN CUS SIN CUS SIN CUS SIN CUS SIN CCS SIN CC								
S SIN CCS SIN CUS SIN CUS SIN CUS64656566666767686868695.1695.2695.1695.2695.1695.2695.1695.2		-0-1	13.1	-25.5	0.0	0.0	-173.5	17.
S SIN CCS SIN CUS SIN CUS SIN CUS64656566666767686868695.1		-35.5	-0-2	13.7	0.0	၁ <b>•</b> ၁	-8-2	
S SIN CCS SIN CUS SIN CUS SIN CUS64  2 2632.2 0.0 0.0 44.5 958.1 695		0.99	11.9	6.0	0.0	0.0	-38.4	101
**************************************		-52.4	۱ 🛶	7-64	0.0	000	98.5	
S SIN CCS SIN CUS SIN CUS  • 1R  • 2F  • 3R  • 3R  • 10  • 1  • 2F  • 3IN  • 10  • 1		53.7	<b>~</b>	13.7	0.0	C • 0	-314.7	69
**************************************		227.1	72.4	1-66-7	0.0	0.0	326.4	333.
**************************************		-411.6	-102.9	105.3	0.0	0.0	-342.0	385.5
**************************************		-342.1	74.2	-33.2	0.0	0.0	155.2	12.8
**************************************		46.8	-76.6	280.0	o•0	0.0	-275.9	635.0
• 1R • 2F • 3H • 5H SIN COS SIN COS SIN COS SIN COS SIN COS SIN COS • 1 • 1 • 0• 3		695.1	958.1	44.5	0.0	0.0	2632.2	-2967-
• 1K • 2F SIN COS SIN COS SIN COS		841.7		-907.6		0.0		-1977-1
UPPER FOTCF BLADE NORMAL BENDING MUMENT • 1K • 3K	S	co3	NI S	SOO	NIS	SCS	ZIS	SOS
BLADE NURMAL	• <b>6</b> K					•2F	<u>1</u> K	•
			MUMENT			IPPER ROTUR	<b>ס</b>	
	# #	CMY/S, K CMX/S, R	0	CL K/S, R CDR/S, R	"		0    11	_
604.9 ALFS,C = 6.0 CLK/S,R =0.09316 CMY/S,R = .2185 CP/S = 0.002323 CDR/S,R =0.01058 CMX/S,R =-		;		•				

A STATE OF THE STA

RUN 21 VKTS = V/OR =	PUINT 90.0 0.251	8 UMEG*K RHULOO	# # 00 1	604.9 0.2185	ALFS.C CP/S =	6.0 0.002323	CLR/S, K CDR/S, R	=0.09316 =0.01058	CAY/S, R    CAX/S, R	= 0.1366 =-0.0050
		•		ro	LOWER ROTUR	BLADE NURMAL	BENDIN	MUMENT	`	,
	,	• LR			.2R		. 3R		<b>. 68</b>	
HARMONIC	_	s o s	NI S		SOS	N I N	500	Z A	\$ 5000	Z Z
C	56 -	955.9		,	-170.7		9.96		-294.6	
-	22	9	-1060.		9	-587.3	534.9	-124.1	226.1	253.4
	<b>41</b>	59.1		6	11.5	228.8	-67.4	162.1	1.001-	56.0
į.	ť	-30.2	-136.	<b>3</b> *	-36.1	-79.5	-8-3	-53.9	32.7	-25.1
4	7	246.5	185.	a	180.9	6.49	78.7	0.49	-56.6	-25.2
2	ĭ	-68.4	-7.	6	-42.6	26.9	-30.0	29.1	7.6	0.1
•	74	110.2	483.	30	191.5	223.5	62.6	125.1	-20.0	-53.5
~	5	46.4	17.	5	112.0	-85.6	1.44	-29.0	-27.5	9•0
<b>0</b> 0	2 <b>7</b> -	137.7	-16.	÷	-46.1	15.2	3.5	-25.0	8.9	4.4-
6	-101	07.9	102.	7	-3.8	0.19	1.2	-3.5	0.6	-9.2
<u>0</u>	••	•	25.0	9	31.4	-27.7	9.1	•	-8-2	-0.5
05										
-	LOWER	ROJ	EÙGE	· ISE	LUWER RUTUR	UTUR				
	BEN	ING	HENT	, 1R	VITCH LIN	K LUAD				
	_	r08	NIS		cus	NIS				
HARMONIC										
0	-5291	91.1			82.					
7	17.	1772.5	-524		-130.5	110.1				
7	76-	0.03	-417	0	30.6	16.7				
3	•	25.3	45.	s	-24.7	7.6-				
4		3.5	41.	80	2.0	7.9				
٠,	**	16.7	-27.1	~	-3.1	-11.9				
\$	Ī	18.8	-24.	4	33.8	-4.0				
7	4	47.7	-427.	•	22.6	-20.6				
œ	•	79.67	62.		2.8					
σ	ī	-13.0	-44.	4	34.5	~				
01	ĭ	45.6	<i>.</i> •	5	-15.8	-14.5				

•

RUN 21 VKTS = V/OR =	PÚINT 90.0 0.251	8 UMEG*R RHUI OO	= 604.9 = 0.2185	9 ALFS	.t = 6.0 = 0.302323	U CLR/S,R 3 CDR/S,R	= 0.09316 = 0.01058	CMY/S, K = 0.1366 CMX/S, R =-0.0050
	UPPER	RGTON BLADE	DE NURMAL .2R	BENDING MCMENT		UP ELGEWISE BENDING .1R	UR PITCH LINK LUAD	UPPER RUTÜR SHAFT STRESS
S			,	)	;			
00.00	1-	48		-526.	1089.	• •	12	-
1.2	7-	39	•	-480.	39	• ၁	784	20
2.5	1	-193.	•	-459.	22	•	-340	. 3143.
3.7	'	-616.	•	-301.	1255.	• •	-343	99
0		-855.	• 0	-121.	·6F91	• •	-160	
6.2	•	-652.	•	-188.	1300.	<b>ໍ</b>	ROT	4731.
7.5	ı	39	•	-385.	755.	ં	787	. 4988.
~	1	5	•0	-309.	288.	<b>.</b>	175	. 5685.
0		•		-65.	-359.	• •	84	• 5896•
.2		191.	•	-60.	-710.	<b>.</b>		. 5705.
5		4	•	-227.	-67.	•0	28	. 6101.
7.	•	31	•	-451.	910.	ວ	89	6339.
0	•	-743.	•	-515-	1158.	• •	-5-	5522.
~	ſ	-313.	•	-246.	501.	္	74-	. 4577.
		~	•	42.	-464.	0	69-	3432.
168.7	-	1238.	•	-96-	- 200 -	• 0	68-	. 2887.
0	•	.426.	•	-541.	104.	<b>.</b>	66-	3188.
.2	7	355.		-995.	888	• o	651	. 3441.
Š	ï	1337.	•	-1439.	984.	ċ	-144	. 2648.
. 7	7	-4062.	•	-1755.	83 <b>d</b> •	• •	-80	
0	7	.342.		-1802-	459.	•	-197.	189
.2	7	3941.	•	-1802.	-85.	<b>.</b>	755-	. 1566.
ŝ	4-1	-4157.	•	-1927.	-24.	<b>•</b>	-483	2
. 7	<b>64-</b>	9	•	-2028-	622•	ວ	364	5.5
0	S.	5126.	•	-2048.	1150.	<b>້</b>	-325	815
	4-	4979.	•	-2031.	1748.	• ၁	-345	36
Š	3	5184.	•	-1951-		• •	-415	2
. 7	7-	~	•	-1760.	2533.	<b>.</b>	-516	. 881.
0	<b>~</b>	3915.	•	-	•	ာံ	644-	30
326.25	7		•		1809.	<b>•</b>	-274	_
Š	-2	:>05.		95	~	ວ	60	~
	7-	49	• ວ	5	871.	<b>.</b>	-436	. 1916.

RUN 21	PCINT	ω						
<b>.</b>	0.06	CARG*R	11	9 AL FS, C	S <sub>1</sub> C = 6.0	CLR/S,R	) 	H
œ	0.251	KHUIO	H				=0.01058	ü
	LUNER	KOT OR BLA	BLADE NURMAL	BENDING MCMENT	MCMENT 68R	LR EDGEWISE BENDING .IR	LE PITCH	
S		•	)	)	, ,			
0.00		-	741.	513.	-461.	-2921.	-240.	
88.7	•	212		255.	-450.	-3753.	-227.	
77.5	•	99	51.	131.	-437.	-4446.	-224.	
66.2		•	198.	247.	-520.	-4573.	-482.	
55.0		7	751.	373.	-595-	-4765	-220.	
43.7			598.	211.	-504	-5484.	-69-	
32.5	1-	O	-260.	-132.	-379.	-6579.	-88	
21.2	1-	2	-611.	-276.	-458	-7236.	-146.	
10.0	•	96	-238.	-175.	-596 -	-6954.	•9	
98.7	1	3	.52	-102.	-723.	-6649-	147.	
87.5	1	82	-154.	-204	-156.	-7364.	100.	
76.2	1-	77	-630.	-454.	-687.	-8176.	<b>.</b> 08	
65.0	-2	38.	N	-729.	-559.	-7644.	118.	
	7-	- 7196.		-824-	-461.	-6400.	•09	
142.5	7 -	08.	-1427.	-663-	-379.	-6909-	14.	
31.2	-2	93.	n	-514.	-257.	-6663.	68.	
20.0	7-	46.	-1236.	-366.	-140.	-6754.	•99	
08.7	-2	10.	- 37	-187.	-19.	-5760.	14.	
7.5	7-	11.	_	23.	-	-4876.	18.	
6.2	7-	33.	LO.	222.	76.	-5227.	-2.	
5.0	7-	11.	3	360.	• 66	-2865-	-61.	
3.7	7-	30.	77	365.	104.	-5566.	-33.	
2.5	7-	56.	-	321.	138.	-4214.	25.	
1.2	1-	<b>4</b> 8.	$\sim$	397.	145.	-4208.	-43.	
0.0	•	18	-48.	559.	48.	-4614.	-177.	
8.7		63	455.	688.	-122.	-4814.	-219.	
• 5		31	861.	758.	-228.	-4107.	-159.	
56.2	1	67	740.	671.	-201.	-3241.	-135.	
45.0	•	87	286.	397.	-153.	-3227.	-228.	
33.7	ſ	70	125.	244.	-701-	Ø	-308.	
• 5		-	372.	410.	-308-	-3818.	-262.	
11.2		~	661.	603.	-405-	-3055-	-217.	

CMY/5,K = 0.1746 CMX/5,K =-0.0064	×0.	CUS SIN		1968.9		-277.2 -703.5		4	٠		4	84.2 61.1	4.6																	
55				~	~	1	1	ı																						
A = 0.12079 A = 0.01305	BENDING MUMENT . 38	NIS			1973.9	-318.6	86.2	-194-1	62.6	-157.7	-58.0	17.6	1.1	5.02		KUTOR	STRE				3344.0	75.4	-46.2	132.5	-475.4	110.0	-35.9	6.517	-47.4	239.6
CL K/3, n COR/3, k		SDO		4.00.1	508.8	168.0	-74.1	33.7	-73.9	-17.5	52.8	-21.8	6.5	-15.0		UPPER	SHAFT	COS		3612.8	-1426.4	-540.0	205.4	249.2	-130.0	63.9	-355.4	6.b	-18.3	0.86-
= 6.2 0.003962	BLADE NORMAL	SIN			0.0	C•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		TUR	LUAD	NIS			252.4	52.3	-46.4	-8.2	-143.2	5.7	134.0	31.1	8.5	5.4
ALFS,C CP/s =	UPPER RCTUR	500		0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	0.0		UPPER RUTUR	PITCH LINK LUAD	cus		-199.0	-115.3	-14.0					-27.7	-5.3	22.8	2.0
)*K = 604.5  CU = 0.2181		NIS			4712.7	-674.7	73.5	-583.6	380.6	-486.1	163.1	-117.5	-10.1	-170.6		ROTUR EDGEWISE	. 1.R			•			0.0	0.0	0•0	0.0	0.0	0.0	0.0	0.0
NI 9 • 8 GMEG*R 51 RHUI GU	a ·	SOO		601.9	742.0	517.2	•	151.5	-381.1	2.	21.4	•	107.6	-68.2		UPPER ROTO	2			0.0	0.0	0.0	0.0	•	•	•	0.0	•	•	•
POINT 89.8 162.0																د	,													
PUN 21 VKTS = V/OR =			HAPMONIC	0	1	2	~	4	ĸ	•	~	€	6	10	10	8			HARMONIC	0		2	~	4	ß	9	7	<b>6</b> 0	6	10

PUN 21 VKTS # V/CR #	PUINT 89.8 0.251	9 DMEG*K RHÜ100	# # 400	604.5 0.2181	ALFS,C CP/S =	0.003962	CLR/5,R CDR/5,R	=0.012079 =0.01305	CMY/S,R = CMX/S,R =-	= 0.1746 =-0.0064
		9	_	101	LOWER RGTCR	BLADE NORMAL	L BENDING MUMENT	MUMENT	3	
	C3		SIN			NIS	C08	NIS	500	NIS
HAPMONIC	•	•			)    -	· ·	)   	· •		
C	255	8.6		•	2384.8		1842.9		-56.1	
	-674	4.6 -	2600.		•		-246.5	-773.5	15.0	193.9
2	-459	9.5	124.		-387.6	131.4	-357.8	73.0	-226.3	29.5
3	-144	4.2	-214.4		-127.6	-97.0	-59.7	-63.2	32.5	-15.5
4	-11	1.6	536.8		55.3	353.3	-15.6	8.861	-17.0	9.98-
5	m	35.1	272.(		4.69	151.5	1.3	66.5	-5.6	-25.8
ç		12.3	693.6		211.4	352.3	55.6	187.3	-15.3	-15.9
~	20	17.3	78.		125.7	-57.5	63.0	0.41-	-24.4	6.9-
80	61-	9.6	-216.2		-121.2	-25.7	0-8	0.81-	19.7	14.0
Ċ	-5	1.1	m.	~	-47.3	-33.6	15.9	-8.5	8.5	18.3
01	7	9.6	·		-11.5	-57.1	34.6	•	10.4	17.7
10										
)9	I CWER		KOTOR EDGEN		LOWER K	OTOR				
	CNER	INC M		<b>1</b> 8	PITCH LIN	K LOAU				
	503		SIN		CUS SIN	SIS				
HARMON IC										
C	-5496	•			-10.5					
_	7864	-	919		-188.6	123.5				
2	206	. 7	-372-3		-18.8	21.5				
3	J	. 7	6.4		-10.2	-58.2				
4	-	7.7	7.44		6.47	3.0				
5	-2	1.0	16.6		42.5	14.2				
\$	C1-	•	-71.		41.6	<b>5.61</b>				
7	J.K	•	67.4		4.4	9.6-				
<b>a</b> n	1	•	55.		-3.2	7.5				
6	30,	6.0	27.6		9.9-	10.1				
10		•	-1-		10.4	e-01-				

	POINT	<b>o</b>				,		
VKTS = V/OR =	85.8 0.251	UMEG#R RHU100	= 604.5 = 0.2181	ALFS, C CP/S =	5 = 6.2 = 0.003962	CL R/S, R COR/S, R	=0.12079 C	$CMY/S_1R = 0.1746$ $CMX/S_1R = -0.0064$
	COFER #	ROTCR BLADE	DE NORMAL	BENDING MCMENT		LR EDGEWISE	LR PITCH	
S	•	•	1			•		
0.00	35	18.	36.	2904.	-261.	-4282.	-145.	
88.7	4	.69	31.	2768.	-63.	-5610.	-130	
77.5	4.5	05.	08.	2649.	-3.	-6119-	-111-	
66.2	25	8O.	16.	2779.	-32.	-5986-	-232.	
55.0	55	12.	07.	2980.	-74.	-6432.	-101-	
43.7	5.5	70.	<b>.</b> 84	2863.	-38.	-7805-	17.	
3	43	81.	.90	2565.	-15.	-8664.	39.	
21.2	54	42.	44.	2486.	-151.	-8662.	87.	
10.0	3,	68.	32.	2540.	-376.	-7801.	149.	
98.7	35	08.	30.	2432.	- 464-	-8036.	178.	
87.5	34	-06	50.	2103.	-461.	-8978-	203	
76.2	77	24.	08.	1630.	-345.	-8819.	198.	
65.0	, <b>1</b>	56.	1626.	1253.	-220.	-1361.	122.	
53.7	77	14.	1380.	1214.	-143.	-6049-	95.	
45.5	7 7	63.	1449.	1353.	-73.	-0069-	158.	
31.2	<b>□</b>	72.	1487.	1419.	43.	-1456.	172.	
20.0	<b>.</b>	34.	S	1463.	145.	-6585	139.	
08.7	:23	22.	1462.	1504.	227.	-5015.	163.	
7.5	7	19.	1345.	1489.	348.	-4564.	192.	
6.2	4	88.	1224.	1513.	404.	-5324	185.	
5.0	⊃ <b>1</b>	•	1402.	1491.	322.	-5255-	190.	
3.7	4	.86	1345.	1233.	291.	-4283.	140.	
2.5	ĭ		9	995.	341.	-2965-	-30.	
1.2	71	7.	460-	1061.	211.	-5167-	-201.	
0.0	7.7	3.	Φ	1232.	-86.	-3486	-248.	
8.7	31	۶.	1801.	1356.	-251.	-5959.	•681-	
Š	14	<b>7</b> •	1804.	1428.	-253.	-1800-	-114.	
56.2	71	۲•	1571.	1241.	-187.	-1743.	-176.	
45.0	7	•	1323.	975.	-14.	-2863.	-233.	
333.75	57			1246.	-23.	-2558.	- 306 -	
22.5	35	3.	2458.	2068.	-158.	-3284.	-187-	
11.2	56	•66	93	2731.	-311.	-3248.	-513.	

- 0.1901 0.0043	25.00 25.00 27.40 27.40 27.60 103.1	
CAY/S, R + CAX/S, R + 1	CCC	
=0.13876 =0.01286	AUMENT  2 189.4  -306.3  -118.7  -229.5  -11.9  -11.9  -11.9  -11.9  -11.9  -11.9  -11.9  -11.9  -12.0  -12.0  -281.3  -22.7  -281.3  -22.0  -22.0  -22.0  -22.0  -22.0	
CLR/S, R CDR/S, R	- BENJING MUMENT - 36	
6.4	SIN 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.	
ALFS,C CP/S =	UPPER KCTCK BLA  CCS SI  0.0  0.0  0.0  0.0  0.0  0.0  0.0  0	
PCINT 10 89.9 CMEG*K = 607.3 0.250 RHCLCG = 0.2169	UPP ER ROTUR EUGEWISE BENDING AOMENT IR SIN CO. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	
PUN 21 VKTS = V/CR =	115 HARACO L SEA COLONIO DE LA	

. . . . .

= 0.1901 = -0.0043	228.4 154.3 154.3 125.4 133.3 13.9 13.9 13.9	
CMY/S,R = 0 CMX/S,R =-0	28.4 315.1 -328.2 60.6 51.1 -15.9 -15.9 -15.9	
=U.13876 =U.01286	MUMENT -659.2 -659.2 -464.6 -31.8 262.5 98.1 196.0 -23.0 -24.1 16.7	
CLR/5, R CDR/5, R	2524.6 1194.8 -659.2 1194.8 -659.2 1194.8 -659.2 -111.0 -51.9 -97.6 262.5 -51.9 98.1 52.8 196.0 52.8 196.0 55.1 -33.0 28.2 -24.1 18.3 16.7	
ALFS,C = 6.4 CP/S = 0.007045	B 4010-101-101 DX 1	-28.3 -52.3 4.4 -51.0 -0.1 -36.5 -41.1 30.7
607.3 A	LOWER ROTOR  28  28  3437.5  1632.4  -966.2  -239.7  -127.1  -127.1  -56.8  172.8  43.1  -94.7  107.2  -31.2  -214.4  -61.7  -7.1  33.6  13.9	7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7
UMEG*R = 6 RHULOO = 0.	118 SIN -2271-7 -2271-7 722-8 -120-6 715-4 217-1 683-4 -174-9 -311-8 -224-7 -189-8 MOMENT - 51N	•
PUINT 10 84.9 GM 0.250 RH	1936.8 2238.4 -1398.4 -1398.4 -1398.4 -176.1 -176.1 -176.1 -11.2 -10.0 558.7 -54.0.5 3819.2 3319.2 -331.5	-150.5 378.2 -60.3 -92.5 35.2
RUN 21 VKTS =	HARMONIC 113 HARMONIC 129 83 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 7 8 8 8 7 8 8 8 7 8 8 8 7 8	9 ~ 8 6 0 10 9 8 4 6

Commence of the second

	PCINT	) O I	•	4.73	, u	13			=0.1347x	<b>&gt; &gt; &gt; &gt; &gt; &gt; &gt; &gt; &gt; &gt;</b>	0.100
V/08 H	0.250	KHU100	• н	0.2169	CP/S	0.007045		COR/S, K	=0.01286	C4X/	- X
	UPPER	ROTUR BLADE			BENDING	MUMENT	UF ED		UR PITCH		UPPER KCTOR
		• 1K	''	<b>x</b>	• 3K	.6R	BENDING .	NG . LK	LINK LUA	၁	SHAFT SIRESS
S											
00.0	7	CD.	Э		Ò	3			65-	3.	3785.
1.2	٠,	_	Ö	•	1278.	2913.		• •	-21	7.	4535
2.5	<b>~1)</b>	3897.	J		_	2631.		• •	-18	.61	4915.
3.1	is 1	~	O	•	0	.9867		•	1-	.4.	5768.
5.0	v	5600.	2		3565.	3377.			651	.6	.0689
6.2	w	$\sim$	Ö	•	5	3228.		•	97	·I.	7171.
7.5	u)	10	o o	•	4	3813.		• •	11	.0	1703.
8.7	æ	~	0		*024*	4767.		• ၁	-11	19.	.9716
0.0	, LJ		Ö	•	33	4530.		• •	67-	5.	9051.
01.2	01		Ö	•	œ	4139.		•	6	.61	3
12.5	·,	$\sim$	Ö	•	m	4870.		•	48	5.	9653
3.7	æ	_	Ö	•	S	5363.		•0	39	5.	-4
35.0	w	i	Ŏ		$\sim$	4573.		<b>•</b>	11	5.	Ω
46.2	3	. •	o	•	သာ	3173.		•	16	5.	5397.
57.5	ໝ	_	Ö		•	1873.		•		,3.	4325.
168.7	-	10	0	•	•	1508.		၁		.2.	4017.
•	4	4109.	ò	•	2385.	2364.		• •	5	.1.	4221.
61.5	7	_	o O	•	9	2936.		•	•	• •	4022
05.5		•	Ó	•	Q	2347.			-15	<b>5</b> 8•	2829.
13.7			Ö	•	m	1683.			-28	80.	
25.0		m	Ö	•	$\sim$	1512.		• •	44-	•64	1929.
36.2			ò	•	-	1671.		•	-68	81.	1326.
41.5		_	Ö	•	-	2568.		• •	-61	7.	588.
58.7	7	90	j	•	~	3954.		•	-34	9	850
70.0	7-	54	Ö	•	0	4914.		•	-38	82.	1159.
81.2	1-	.+	Ó	•	0	5408.			79-	•	882.
92.5	1-	40	Ó	•	-	5433.		·	-65	57.	401·
03.7	-1	40	J.	•	S	4615.		• •	65-	.90	149.
15.0	•	$\sim$	Ö	•	430.	3366.		•	-33	31.	4
26.2		6	ó	•	S	13		•	-28	. 9	X
37.5		7	0	•		5		•		.61	
48.7	7	9.2	Ó		Ň	1223.		•	55-		7 7

RUN 21 VKTS = V/OR =	PGINI 89.9 0.250	10 CME RHÜ	OMEG*R = RHUIOO =	607.3	ALFS.C	0.007	6.4 CLR/S, K '045 CDR/S, R	=0.13876 CMY/5,R =0.01286 CMX/5,R	S,R = 0.1901
	LUNER	RUTOR	BLADE	NURMAL	BENDING MUMENT	MUMENT	LR EDGEWISE	LR PITCH	
U		• 1 R	•	~	3R	•6R	BENDING . IR	LINK LOAD	
00.00	σŏ	S	65	Ś	4222.	-179.	-4023.		
88.7	7	5	58	28	i	46.		-243.	
7.5	11	13	54	66		127.	-6475.	-252.	
66.2	ō	7 4	53	.040	3673.	181.	-1720.	-111.	
55.0	99	53	25	.21.	3702.	173.	-8530.	-106.	
43.7	9	8	SC	.161	3333.	79.	-9111.		
32.5	Ť	3	45	88.	2737.	<b>.</b>	-11038.	156.	
21.2	34	0	35	.80	2327.	-140.	-111141-	138.	
10.0	4	_	35	.30	2051.	-487.	-10550	92.	
7.86	38	•	36	.020	65	-751.	-10426	241.	
87.5	3	6	51	.69.	1080	-698.	-10399.	269.	
76.2	ĭ	7	4	•60•	425.	-541.	-9238.	131.	
65.0	7-	0	-2	~	-32.	-616-	-7314.	119.	
53.7	Ĭ	03		Ö	11.	-406-	-5958	140.	
45.5	1	35	_	-	_	-280-	-5696-	112.	
31.2		_	30	-	-	-173.	-5465.	203	
20.0	7	S	97	193.	1469.	-16.	-4607	259.	
08.7	4	S	21	Ò	1884.	294.	-3736.	169.	
7.5	-	S	22	.69	2356.	<b>58</b> 6.	-3546.	.852	
•	34	465.	30	.00	2830.	.099	-4322.	+77.	
5.0	٠	7 3	38	.661	3078.	.919	-5040•	376.	
3.7	35	40	38	171.	12	196.	-4606.	71.	
2.5	Ų	4	3,5	.39.	3263.	147.	-3246	-73.	
1.2	Š	20	45	.37.	47	388.	-2115.	-72.	
0.0	Ó	0	51	.08.	42	115.	-7837.	-80-	
8.7	4	88	47	.64•	36	124.	-5069.	-160.	
Š	74	3	9	165.	3144.	125.	·106-	-264.	
56.2	74	77	38	151.	99	87.	-066-	$\sim$	
45.0	Ř	*	<u>ر</u>	187.	2	189.	Δ	Ø	
	38	13	35	.02.	57	172.	14	-383-	
22.5	7	2	46	.37.	4	Š		0	
11.2	о́	33	64	.10.	4090	-358.	-7967-	-720.	

SICO 000000000000000000000000000000000000	NIS	(၁၁)		• 1R • CGS
000 000 000 000 000 000 000 000	0	000		-326.5
0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0		0.0		-339.1
0.0 135.6 0.0 4.8 0.0 4.8 0.0 4.8 0.0 8.0 0.0 9.0 0.0		0.0		136.0
100 100 100 100 100 100 100 100		0 0		-141-9
10.0 0.0 0.0 0.0 0.0 0.0 0.0 13.9 130.2 130.2 15.7 130.2 15.7 130.2 15.7 130.2 15.7 15.7 16.2 16.2 16.2 17.8 18.0 19.0 1				-214.3
0.0 0.0 0.0 0.0 0.0 -3.9 IOR LUAD SIN 2261.3 207.7 -1794.8 -0.4 -0.4 -1794.8 -0.4 -1794.8 -0.4 -1794.8 -0.4 -1794.8 -0.4 -15.7 -1794.8 -15.7 -116.2 21.1 -16.2 -11		0.0		7
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10K UPPER H 10AD SHAFT S SIN COS 3261.3 207.7 -1794.8 -0.4 -542.6 -15.7 -1794.8 -0.4 -542.6 -15.7 -542.6 -15.7 -542.6 -15.7 -542.6 -15.7 -22.7 34.4 -155.1 -16.2 21.8 20.7 31.5	<b>D</b> •0	0.0		• 1
LUAD SHAFT S SIN CGS 207.7 -1794.8 -0.4 -542.6 -15.7 -130.2 -31.9 -99.5 -62.7 -67.9 21.1 -22.7 34.4 -155.1 -16.2 21.8 20.7 31.5	UPPER ROTOR	PPER		OR EDGEWISE
2261.3 -1794.8 -1794.8 -130.2 -67.9 -67.9 -155.1 -155.1 -57.2	PITCH LINK LUAD	E F		œ
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-67.9 -125.1 -155.1 -51.8 -57.2		2.1	•	0
21.1 -22.7 34.4 -155.1 16.2 21.8 20.7 31.5		• 5	22	0•
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0.1446	KUTOR STOLES	SINES	7	871	1303	1880	2437.	2665	2922	3548	4063	4384	4992	5584	5550	5664	7674	3951	4411	4907	4469	3880	4016	4144	3786	3566	3549	3219	2566	1890	1527	6091	1585	1082
11 11	UPPEK	-																																
CMY/S,R CMX/S,R	5 3																																	
5 S	I S	Š	.99	. 33	-4	2	03.	55.	-6-	68.	<b>.</b> 89	05.	.90	88.	15.	36.	64.	59.	77.	-345.	38.	58.	77.	24.	- 86	08.	62.	47.	55.	.999	23.	466.	သ	83.
683	UR PITCH	2 2 4	<u> </u>	₹.	-5	4-	-3	1-		•	-2	1	7-	1-	7-	-2	7-	-2	7-	<u>.</u>	-3	۳-	15	-1	15	15	-5	-5	-5	9	9-	<b>7</b> –	4-	-5
=0.07363 =0.01289	. S	1																																
	ت المد	<b>v</b>		•									•			•		•								•			•				•	
CLR/S, K CUR/S, R	EDGEWISE		၁	Š	3	Ö	j	ò	Ó	Š	၁	Ó	Ö	၁	Ċ	0	ò	ŏ	ó	၁	ŏ	ó	ŏ	ŏ	ó	ŏ	ŏ	ŏ	ŏ	ó	j	ò	Ó	Ŏ
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8 • 3 8 94	2 6	<b>5</b>																																
8 • 3 0 • 000894	<u> </u>	¥	.2.	.4.	.6	.5	82.	.5.	.8	52.	. 7	.7.	7.	9	. 4.	. 88	8.	11.	. 4	.90	گ	12.	.2.	3.	. 4.	.5	.6	15.	.7.	.2.	.1.	832.	.61	.60
11	1UMEN	•	7.1	8.5	84	53	9	7.2	<b>5</b> -	-1152	-175	- 189	-171	-101	-36	-88	- 196	-205	-112	- 39	4	63	88	79	128	218	267	318	397	401	336	283	233	136
ALFS,C CP/S =	BENDING MUMENT					•	•											•									•	•	•	•	•	•		•
	BEND		375	-563	-815	1025	-1220-	1478	1683	1691	1594	1583	1756	2026.	2111.	1881	1506.	1396	1499.	-1632.	1703	1644	1432	1166.	-945	-771	-637	_	144-	-427	-426.	-371	-304	-297
610.2	CRMAL		•	•	•	1	ſ	1	1	1	1	1	١	ľ	1	1	1	1	1	t	1	ł	1	1	•	•	•	•	•	•	•	•	•	·
0	NCR.	¥	•	• •	• •	• •	•	• •	•	•	• •	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	·	•	0	• •	•	•	•	•
# 0 X 0	BLADE N	•																																
OMEG*R RHJ100			•			•	٠	•	•	•	.•	•	•	٠	•	•	•	•			•	٠	•	•	•	•	.•	٠	•	•	•			
<b>1</b>	<b>~</b>	Y	123		213	244	3101	381	376	~	-	3	-2808	*	N	3750	198	138	252	-3368	361	3993	367	2641	241	268	232	2172	256	247	81	178	182	
PUINT 89.8 0.248	UPPER		1	1	ı	1		ı	1	1	1	1	ŧ	1	•	ı	ŧ	1	1	1	•	•	1	1	•	ı	1	t	1	ľ	1	1	1	1
S 21 = 1		7	00	,25	.50	. 75	00•	.25	.50	.75	00•	.25	• 50	.75	00.	.25	.50	.75	00•	•25	.50	.75	00•	•25	.50	• 75	00.	•25	• 50	.75	00•	.25	• 50	.75
PUN VXT			Ó	-	~	3	45	•	~	8	0		12	23	35	Φ	57	168	80	15	02	13	25	36	47	58	70	8	92	03	15	26	37	æ

RUN 21 VKTS = V/OR =	99.8 0.248	DANEC CANEC	OMEG*R = RHU160 =	610.2		ALFS,C = CP/S = 0.00	8•3 •000894	CLR/S, R CUR/S, R	=0.07363 =0.01289	CMY/S,R = 0.1440 CMX/S,R =-0.0031
	LUWER	ROTOR	BL ADE	NORMAL	BENDING	IG MOMENT	L R BFR	LR EDGEWISE Bending . 1R	LR PITCH	11 040
S		4	•	;	<u> </u>					
0	•	610	-39	67.	-2631.	-773.		-3163.	-3	128.
8.7	19-	26	-45	92.	802	-801.		9	£-	345.
7.5	9-	37	-41	31.	-2730.	-880		-4472.	-3	-309.
•	-5	163.	-3570	20.	-2390.	-896-		-4636.	£-	-337.
5.0	4-	7	-29	47.	-2089.	-1006.		-4448.	£.	-301.
3.7	4-	68	-27	31.	-2092-	-928.		-4786.	7	-183.
2.5	-5	Š	-31,	27.	-2248.	-754.		-5626.	1-	-188.
1.2	-5	68	-34	53.	-2234.	-674.		-9609-	7-	-240.
0.0	4-	22	-30	0.40	-1983.	-768.		-5869.	7-	-142.
8.7	£-	8	-22	22.	-1664.	-879.		-5657.		-6-
7.5	-3	27	-19	76.	-1478.	-870.		-6139.		31.
6.2	£-	32	-25.	37.	-1503.	-789.		-6889-		34.
5.0	51	~	-24	47.	-1602.	-700.		-6984.		12.
3.7	74-	34	-24	.66	-1586.	-583.		-6351.	1	-21.
2.5	4-	•	-25	.99	-1478.	-446.		-6053.		-7.
1.2	4-	8	-25	68.	-1381-	-350.		-6500.		-8-
0.0	74-	75	-23	95.	-1266.	-304.		-6910-	•	-40•
8.7	4-	~	-25	03.	-1105.	-260.		-6443.	•	-13.
7.5	-40	51	-21	15.	-988-	-224.		-5759.		-4.
6.2	-3	O.	-20	62.	-971.	-221.		-5905-	•	.85.
5.0	-3	.166	-20	78.	-1038.	-213.		-6520.	7-	-102.
3.7	4-	63	-25	64.	-1139.	-185.		-6405.	•	-39.
2.5	<b>7</b> -	37	-24	87.	-1269.	-161-		-5511.	•	-61.
1.2	14-	2	-26	.90	-1401-	-790		-4981.	7	-136.
0.0	54-	348.	17-	08.	-1500.	-325.		-5271.	7	-184.
8.7	-4ª	. 60 P	-27	41.	-1517.	-407.		-5488.	7-	-245.
.5	4-	491.	-26	15.	-1560.	-516.		-4857.	-2	-259.
56.2	<b>5</b> -	4842.	-27	• 00	-1780.	-556.		-3915.	-2	.13.
45.0	7-	849.	-35	51.	-2106.	- 530 •		-3665.	-27	71.
	9-	6119.	-37	. 90	-2313.	-568.		-4010-	~	-365.
22.5	3-	9	- 36	47.	36	9		-4143.	£-	311.
11.2	3	8 95	-36	.10	-2441.	- 169.		-3551.	7-	:57.

CMY/S,R = 0.1446 CMX/S,R =-0.0031	613.2 1144.7 -1918.6 -328.8 -195.9 -270.8 231.9 -471.8 357.2 39.0 -295.6 111.8 117.6 -62.2 -9.9 -33.5 4.4	
=0.07364 =0.01288	210.6 210.6 504.5 -495.1 137.2 -135.7 14.6 -74.9 136.6 -74.9 -20.3 83.6 -38.6 -14.9 27.1 -20.1 3.9 -6.1 -4.7 -6.0	664.9 -16.6 -189.0 -211.8 -44.4 -31.1 -26.0
CLR/5, R COR/5, R	<b>-</b> →	UPPER SHAFI CUS 3276.3 -1743.0 -547.0 144.4 -80.0 -183.8 9.2 -231.1 59.8 -3.4
* 8.3 0.000871	8LADE NURMAL 0.0 0.0 0.0 0.0 0.0 0.0	218.4 218.4 56.3 33.4 25.8 33.4 14.0
ALFS,C CP/S =	UPPER KUTCR CUS . 2 R 0.0 0.0 0.0 0.0 0.0 0.0 0.0	UPPER KCTOR COS SI -390.2 -63.9 218 -23.8 6 -71.1 3 -9.0 -31 -7.2 -66 -1.3 25 13.4 33 -25.1 8
UMEG*k = 610.3 RHU100 = 0.2165	21N -278-1 -424-7 101-3 -316-5 -195-3 -68-8 -27-0 -234-1 5-3	S SIN SIN SIN SIN SIN SIN SIN SIN SIN SI
PLINT 12 90.0 0.249	12655.2 4716.0 427.5 130.5 475.9 -109.7 -68.2 -68.0 -93.7	BENDING BENDING BENDING CO.OOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOOO
RUN 21 VKTS = V/CR =	HARMUNIC 0 0 4 3 7 6 9 4 10 10 10 10 10 10 10 10 10 10 10 10 10	0 HAPPHONIC 2 2 2 10 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9

the transfer of the said

R = 0.1446 R =-0.0031	2 342.6 1 342.6 3 -29.0 1 -16.9 7 -39.9 7 -18.0 7 -18.0
CMY/S,R CMX/S,R	-574.2 -574.2 -67.1 -67.1 -17.7 -17.7 -17.7 -17.7
=0.0736+	BENDING MUMENT  - 3R  - 5R  - 6R  - 78  -
CLR/S, R CDR/S, K	<b> (</b>
= 8.3 0.00871	BLADE NORMAL SIN 638.5 274.7 -45.1 -23.1 -23.1 -26.9 -10.8 -2.9 -28.6 0.9 0.9 0.9 0.9 119.4 112.1 -12.4 -12.4 -12.4 -12.5 -14.6 12.5 -19.7
ALFS <sub>F</sub> C CP/S =	LUWER RGTCR BLA  -2858.9 -326.9 -326.9 -326.9 -455 217.6 -23 -160.3 -91 -160.3 -91 -17.9 -100.2 -23 -100 CUS SI -152.8 -152.9 -152.7 -152.8 -152.8 -152.9 -152.7 -14.1 -14.1 -14.1 -152.9 -152.
G#R = 610.3 100 = 0.2165	SIN 561.8 481.0 -68.6 -68.6 -250.4 339.5 -40.9 183.5 -19.7 -19.7 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8 -17.8
PUINT 12 90.0 ÜMEG#R 0.249 RHULO0	COS .IR
RUN 21 VKTS = V/FR =	HARMONIC 151 HAPMONIC 10987557890 1098757990 1098757990 1098757999

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PUN 21	POINT	12 CMFG		•	4	U	ε. α	C. K / S. R	=0.073	<b>X X X X X X X X X X</b>	Н
200	0.249	RHUICO	 	0	CP.	3	11 8 0 0 0	COR/S, R	11	CMX,	CMX/S,R =-0.0031
	UPPER		ADE	NORMAL	B.E.	MCMENT	N	3	UR PITCH	I.	UPPER ROTOR
		• 1K	٠	2k	• 3R	.6R	BENUING	7	LINK LU	AU	T X I
S											
0	7	3		•	-438.	703.		• 0	<u>-</u>	45.	~
1.2	7-	1867.		•	-671.	945.		•	5-	.17	1153.
2.5	7-	30		•0	92	783.		• 0	<b>4</b> 1	.995	1696.
3.7	, - , -	4		•	-1133.	632.		• 0	<u> </u>	.09	2297.
5.0	E-	1527.		•	-1388.	826.		<b>့</b>	7-	.27.	2095
5.2	1	Š		•0	-1662.	481.		ં	1	.55.	2827.
7.5	हा <b>।</b>	~		•0	-1775.	-662.		0		4.	3254
8.7	-2	2835.		•	-1714.	-1590.		• 0	7	-159.	3882.
0.0	Ž-	-		•	-1637.	-1869.		•	7-	. 94	4237
1.2	(¥	4		•	-1694.	-1863.		•	7-	241.	4678.
2.5	7-2	0		•	-1935.	-1404.		•	1+	81.	5385.
3.7	1	3660.		•0	-2145.	-485.		•	7	. 35	2691
5.0	4-	8		• ວ	-2015.	-263.			7-	206.	5377.
5.5	-5	•		•	-1641-	-1259.		<b>.</b>	7-	234.	4717.
7.5	<b>7</b> –	3		•	-1399.	-2025.		•	7-	63.	4033
168.7	1-	1654.		•	-1383.	-1537.		•	7-	63.	4055.
0.0	-2	3		•	-1480.	- 144.		•°	£ -	.90	4756.
1.2	<u>e</u>	m		•	-1635.	-306-		•	£-	43.	4836.
202.50	E +	3677.		°°	-1717.	300.		•	-3	-324.	4114.
3.7	4	Ò		•0	•	874.		•	<b>5</b> -	.36.	3888.
5.0	<b>M</b>	7		°°	4	822.		ċ	9	.88	4191.
5.2	2-	Š		•0	~	868.		·	91	.75.	4045
7.5	7-	2832.		•0	-1030-	1624.		•	2-	35.	3629.
8.7	21	Ø		•0	-833.	2276.		•	51	.22.	48
0.0	7-	0		0	-725.	2609.		• •	5-	53.	30
1.2	-2	n		•0	-644.	5373.		•	\$1	38.	87
2.5	7-	2		•0	Ø	90		• •	9-	.16.	2235.
3.7	7-	Š		•0	-575.	3756.		•	Q	•	ō
5.0	1-	1867.		٠°	4	60		0	3	3	1397.
5.2	1-			• ၁	44			•	4	4	7
7.5	1-	56		•0	-355.	95		•	S		
3 • 7	1			•	3	945.		•	-5	8	195.

PLINT 90.0 0.249	12	CMEG*R = RHCIOO =	610.3 0.2165	ALFS CP/S	*C = 8.3 = 0.000871	8 • 3 8 71	CLR/S,R =	=0.07364 =0.01288	CMY/S, R = 0.1446 CMX/S, R =-0.0031
OWER R	KOTOR	BLADE	URMAL		MOMENT	LR EDGE	EDGEWISE	LR PITCH	_ (
	• 1K	• 2K		• 3K	• • •	ŭ	NG • 1K	LINK LUA	9
- 1	82	42	•	73	- 766.		-3505.	- 36	Ö.
9	5	2		2812.	-848-		-4225.	-32	2.
-	~	$\boldsymbol{\alpha}$	•	2575.	-746-		-4649.	-31	4.
ĭ	•	31		2184.	-1018		-4553.	-33	17.
Ī	4039.	-2711		2033.	-1008-		O	-23	36.
•	3	28	•	2183.	-850.		-5280.	191-	61.
1	~	34	•	2307.	-678.		-6023.	-22	5.
ı	~	34	•	2178.	-689-		30	-212	.2.
١	336	97	1	1865.	-833.		-5748.		70.
ï	3000.	61	•	1573.	-404-		-5927.	7	.7.
ł	366	20	•	1489.	-853.		-6707.	~1	.7.
	4030.			1592.	- 160.		-7153.	M	38.
1	.4544.	25		1660.	-644.		-6723.	ł	·8•
1	-4659.	97		-1591-	-503-		-6115.	£ -	30.
•	-4679.	27		-1493.	-348.		-6261.	1	-4-
•	-4285.	25		1376.	-347.		-6866.	- 16	• •
ĩ	.4195.	$\sim$		1238.	-293.		-6810.	-5	27.
	-4596-	22		1134.	-233.		-6067.	,	-4•
•	-4095	22		1075.	-218.		-5777.	-45	5.
•	-3969.	7.7		1047.	-219.		$\sim$	-105	.2.
1	<b>+</b> 28	7.7		-1058.	-188		-6635.	-67	.7.
•	457	54		1210.	-117.		-6022.	-43	3.
•	7 2	25	1	1314.	-224.		-5223.	96-	.91
•	-4760.	52	1	1422.	-275.		-5155.	<b>5</b> 1-	.2.
•	~	77	ſ	1517.	-335.		-5507.	-201	.7.
•	$\sim$	7.7		1546.	-452.		-5310.	-77	ن.
•	25	2	•	1627.	-545.		-4403	-23	37.
•	~	58	1	1894.	-537.		-3775.	-22-	.2.
•	9	34	•	-	-539.		-4004-	-32	.6.
	150	3	•	33	-637.		-4343.	- 34	8.
•	27.1	35	•	3	7		-3961-	-25	· 80
1	636	3.7	•	S	-739.		-3369.	-28	17.

	C • K • 6	EHC1CO	II )	0.2165	CP/5 #	.r/s = 0.001022	CDK/S,R	= 01528	C4X/S,R	=-0.0028
				UPPER	RCT	BLADE NURMAL		BENDING MURENT		
	Ĺ		-		• <b>4.</b> F. C.	4 I S		• 5k	•	• OK
HAPMUNIC	ני	?	2		200	¥ 10	<b>5</b>	270	S C	210
C	-452	5.5			0.0		-342.0		1350.3	
_	67	•	824.9	~	0.0	0.0	279.8	26.5	381.6	-1506.6
7		9.	40	٠,	0.0	0.0	121.5	-67.2	-402.2	-149.2
. ه	115	6.9	161.5	,0	0.0	0.0	7.6-	0.49	-380.	9.061
4	515	٠ •	-310.0		ن د د	0.0	145.4	-82.5	-505-1	376.5
5			340.0	0	0.0	C. 0	-20.3	72.0	64.5	-280.9
ę	61-	. 1	-272.0	•	ن 0	0.0	-18.d	-93.5	98.2	192.0
7		5.2	88.1	•••	0.0	٥ <b>•</b> ٥	40.1	-10.1	-75.1	1-77-
8	64-		-102.2	~,	0.0	0.0	1.6-	7.7	40.7	51.4
6	350	٠. ٧	-21.5	~	0.0	0.0	0.8	-4.5	-219.0	79.3
0	-63	3.4	-60.5	.0	0.0	0.0	-5.5	11.3	15.3	53.6
	UPPER		LUCEN	4 I SE	UPPER RUTOR	UTOR	UPPER	RUTUR		
	BENU		NG MOMENT . 1R		PITCH LINK	ب	SHAFI	STRESS		
	C0S	35	NIS		cus		500	SIN		
HAP YON IC										
0	J	0.0		•	.303.8		3568.5			
	J	0.0	0.0	c	-81.4	242.2	-1810.0	875.4		
2	J	0.0	0.0	C	-27.3	0.5	-560.5	-1001-		
3	•	0.0	0.0		-81.6	2.8	9.08	-32.7		
4	J	0.0	0		-14.9	-38.2	-39.8	95.3		
2	<b>J</b>	0.0	J.O		-4.3	-103.4	-196.1	-237.9		
9	<b>J</b>	0.0	0.0	•	8.4	20.7	40.1	39.7		
7	3	0.0	0.0	•	17.9	61.3	-249.2	-129.3		
8	J	٠. د	J• 0		-39.9	-1.1	9-0-	99.1		
6	J	0.0	0.0	•	1.6	25.8	-27.6	-61.1		
•	•									

Į

PUN 21 VKTS = V/CR =	PUINT 90.0	13 UMEG*R KHU100	н II ж О	610.3 0.2165	ALFS,C CP/S =	8.5 0.001022	CLR/S, R CDR/S, R	=0.08979 =0.01528	CAY/S,R =	= 0.1735 =-0.0028
,				Ę	0 1 0 0			H 2 3		
		• 1R		Š	LUMER RUICK	DLADE NUKMAL	. BENUING MUMEN!	ACHEN!	.6P	
	ű	รก	NIS		cos	SIN	500	Z IS	รูกว	SIN
HAKKUNIC	600	•					, ,,,		,	
s <b>-</b>	200	<b>.</b>	7 6 7 7	I	1002.4	. 70-	7.066	7 6 1	0.6041	
<b>→</b>	2007	) v	<b>)</b> -	٠. ١	1.40- 177. A	7.46.4	6.74	• (	7.03-	****
۷ ۳	7	١	-130	ن 1	٠ 	-95.8		155	4.4	-26.2
4	327	00	58.4	٠.	202.3	-35.5	95.2	9.8	-62.1	-5.1
5	-287		-213.		-211.9	-38.7	9.96-	0.47-	39.8	22.4
···	79-	7.7	457	7	101.2	244.8	23.6	123.9	-3.1	-51.7
~	22	227.0	34.0	c	118.6	-55.1	7.94	1.3	-24.0	-1.6
or:	5-	8.3	-34.	۵	-14.6	6.4-	13.2	1-5-1	9.0	-2.0
0	6	4.6	19.	6	54.4	-22.5	-5.2	7.9	-12.1	0.0
1.0	iÑ	4.1	-13.	en	11.6	-20.8	0.6	1.1	-6.0	<b>0.</b> +
12										
5	LOWER	RUTUR		WISE	LOWER K	KUTUR				
	BENJING	ING AD		•1R	PITCH LINK					
	3	SO			cos	NIS				
HAPMUNIC										
C	-5397	٠,		•	-132.0					
-	1324	7.	-822.9		-120.2	121.8				
~	147-	. 7	-239.		31.1	12.9				
₹	7-	-26.1	23.		-27.9	-6.5				
•	61-	~	37.		1.0	2.3				
5	39	0	-20.		-19.5	-11.5				
æ	94-	7.	-37		33.3	5.4				
~	511	1.4	-188.		14.3	-13.9				
æ		7.7	5.6		10.0	5.7				
Ć	-2	9.4	24.	,	•	2.5				
1.0		9.4	-1-	2	-5.1	-25.1				

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STATE   STAT	RUN 21	PUINT	13		7	ų (V	ا ب	u X	5/ 13	0.807	7	ii ~	734
JOPER ROTOR BLADE MURMAL BENDING MCMENT OK EDGEMISE UN PLICH UPPER KUT  26. 183. 1014. 0. 0498. 175  -511. 060. 1529. 0475. 123  25.0 -593. 076. 1659. 0427. 123  25.0 -1415. 0142. 1647. 0123. 249  25.0 -1415. 0324. 1678. 0133. 249  25.0 -1415. 0324. 1678. 0133. 249  25.0 -1415. 0324. 1678. 0133. 249  25.0 -1415. 0324. 1678. 0133. 249  25.0 -1415. 0324. 1678. 0133. 249  25.0 -1415. 0263657. 0123. 249  25.0 -249. 0263657. 0267. 0123. 249  25.0 -249. 0263657. 0267. 0125. 249  25.0 -249. 0263657. 0267. 0125. 249  25.0 -249. 0263657. 0267. 0267. 449  25.0 -249. 0160. 0269. 0267. 249  25.0 -249. 0269. 0269. 0267. 449  25.0 -249. 0269. 0269. 0269. 344  25.0 -249. 0272. 1348. 0269269. 249  25.0 -249. 0241. 270. 0269269. 249  25.0 -249. 0241. 270. 0269269. 249  25.0 -269. 0269. 0269. 0269. 0269. 249  25.0 -269. 0269. 0269. 0269. 0269. 249  25.0 -269. 0269. 0269.	ο α	0.249	RHJ10		0.216	CP.	וונ וונ	01022	CDR/51R	=0.01528	Š	:	8200 1028
PST         CAS         SAK         ORN DINO         LINK LUM         DINK LUM </th <th></th> <th>JPPER</th> <th>OTCR</th> <th>ΑυΕ</th> <th></th> <th>BENDING</th> <th>MOMEN</th> <th></th> <th>EWI S</th> <th></th> <th>Į.</th> <th></th> <th>UTUR</th>		JPPER	OTCR	ΑυΕ		BENDING	MOMEN		EWI S		Į.		UTUR
PSTI         262.         C 62.         183.         1014.         0.         -498.         750.           1.250.         -311.         0.         -60.         1529.         0.         -475.         1236.           2.550.         -993.         0.         -142.         1687.         0.         -426.         1833.           2.500.         -985.         0.         -142.         1687.         0.         -226.         1833.         2493.           2.500.         -148.         0.         -148.         0.         -133.         2493.           2.500.         -148.         0.         -263.         0.         -159.         199.           2.500.         -1034.         0.         -263.         0.         -264.         199.           2.500.         -203.         0.         -263.         0.         -264.         199.           2.500.         -203.         0.         -264.         0.         -169.         0.         -169.           2.500.         -203.         0.         -712.         456.         0.         -169.         0.         -169.           2.500.         -203.         0.         -712.         456.			┥		X.	3	9	BEN		¥	ΑŊ	^	Λ
0.00         -56.         0.         -498.         Pb           1.75         -311.         0.         -76.         1659.         0.         -475.         175.         175.         1899.           2.50         -593.         0.         -142.         1659.         0.         -426.         1899.         -594.         1899.         -594.         1897.         1897.         1899.         -594.         1897.         -427.         1897.         0.         -427.         1897.         -427.         -427.         -427.         -133.         -249.         1899.         -594.         1899.         -594.         1899.         -594.         1899.         -594.         1899.         -594.         0.         -125.         -439.         -449.         0.         -126.         -439.         -449.	ഗ												
11.5         60.         1529.         0.         -475.         1529.           2.50         -593.         0.         -142.         1659.         0.         -475.         1649.           2.50         -486.         0.         -142.         1697.         0.         -223.         2403.           5.00         -1415.         0.         -124.         1678.         0.         -123.         2403.           6.55         -1104.         0.         -274.         1778.         0.         -127.         2403.           1.05         -118.         0.         -283.         -263.         0.         -133.         2403.           1.12.         -118.         0.         -283.         0.         -127.         484.           1.12.         -234.         0.         -511.         -601.         0.         -127.         484.           5.00         -135.         0.         -423.         -651.         964.         0.         -126.         114.         484.           5.00         -136.         0.         -423.         -424.         456.         0.         -126.         114.         444.           5.00         -136. <t< td=""><td>•</td><td></td><td>797</td><td></td><td>•0</td><td>83</td><td>d</td><td></td><td><b>ું</b></td><td>4</td><td>86</td><td></td><td>3</td></t<>	•		797		•0	83	d		<b>ું</b>	4	86		3
2.50         -593         0         -76         1659         0         -426         1895           2.50         -885         0         -142         1687         0         -123         2945           5.0         -196         0         -124         1687         0         -123         2946           6.25         -1004         0         -124         1678         0         -123         2946           7.50         -1004         0         -273         178         0         175         2946           0.0         -273         -263         -657         0         -156         405           0.0         -234         0         -254         0         -267         0         -267         405           0.0         -235         -263         -567         0         -267         6144         646         6144         626         6144         626         6144         6184         627         6144         627         6144         627         6144         627         6144         627         6144         627         6144         627         627         627         627         627         627         627	-	1	.311.		•0	60°	52		င်	5-	15		36
3.75         -486         0         -182         1697         0         -233         294           6.25         -1415         0         -324         1697         0         -123         294           6.25         -1415         0         -324         178         0         -123         294           750         -1004         0         -373         -263         0         -126         4405           10.0         -263         0         -264         0         -264         4405           10.0         -272         -594         0         -266         0         -267         4405           11.25         -213         0         -261         0         -267         4405           1.25         -234         0         -765         861         0         -267         4405           2.75         -147         0         -161         -894         0         -164         4406           2.75         -147         0         -162         0         -164         4406           2.75         -148         0         -164         0         -164         4418           2.76         -148	2	1	593.		•0	76	65			4-	26		Š
5.00         -985         0.         -194         1697         0.         -133         2994           6.55         -1415         0.         -274         1678         0.         -135         312           6.55         -104         0.         -273         -263         0.         -83         4405           0.0         -218         0.         -263         0.         -83         4405           0.0         -234         0.         -264         0.         -267         0.         -267         4405           1.25         -204         0.         -261         0.         -267         0.         -267         520           2.50         -204         0.         -624         0.         -267         520         520           2.50         -134         0.         -423         49         0.         -169         524         4418           3.75         -214         0.         -423         49         0.         -160         524         4418           6.25         -147         0.         -423         49         0.         -160         524         4418           1.15         -140         0	8	•	.486.		0.	14	48		• •	```-	23		63
6.25         -1415         0.         -324.         1678.         0.         125.         3112           4.50         -1104.         0.         -247.         178.         0.         -83.         4408           8.75         -1104.         0.         -263.         -657.         0.         -83.         4408           0.00         -213.         0.         -263.         -657.         0.         -263.         4408           1.25         -234.         0.         -511.         -261.         0.         -263.         4408           2.50         -139.         0.         -672.         0.         -252.         5874           2.50         -139.         0.         -425.         0.         -263.         5874           2.50         -139.         0.         -425.         0.         -125.         5844           2.50         -1176.         0.         -139.         0.         -126.         523.           1.25         -1470.         0.         -149.         0.         -160.         524.         524.           2.50         -176.         0.         -160.         0.         -160.         522.         522.	5	ı	.885.		•	-194.	1691		°°°	1-	3	7	6
7.50         -1004.         0.         -427.         778.         0.         -177.         478.           8.75         -118.         0.         -263.         0.         -263.         0.         -267.         440.           8.70         -213.         -263.         0.         -267.         0.         -267.         440.           2.50         -213.         0.         -261.         0.         -267.         0.         -267.         440.           2.50         -234.         0.         -772.         456.         0.         -267.         520.           2.50         -1390.         0.         -767.         461.         0.         -267.         528.           6.25         -1390.         0.         -767.         464.         0.         -160.         528.           6.25         -176.         443.         449.         0.         -160.         453.           6.25         -176.         -176.         144.         0.         -160.         453.           6.27         -176.         -176.         144.         0.         -127.         441.           7.50         -176.         -174.         144.         0.	•	7-	415.		•	-324.	1678.		0	7,	52	7	7
8.75         -118.         0.         -263.         -263.         -657.         0.         -637.         440           0.00         -133.         -263.         -657.         0.         -267.         440           0.00         -213.         -263.         -567.         0.         -159.         527.           2.50         -234.         0.         -511.         -261.         0.         -25.         5874.           2.50         -234.         0.         -772.         456.         0.         -25.         5874.           6.25         -134.         0.         -423.         49.         0.         -160.         528.           6.25         -1176.         0.         -160.         0.         -160.         528.         64.8           7.50         -1186.         0.         -184.         0.         -164.         45.8         67.0         160.         -160.         528.         64.18         67.0         160.         -27.         64.18         67.0         164.         64.18         67.0         160.         164.         64.18         67.0         164.         64.18         67.0         164.         64.18         67.0         164.	7	-	.400		•	-427.	778.		• •	1	11	€	~
0.30         45.         0.         -263.         -657.         0.         -267.         4842           1.25         -213.         0.         -289.         -294.         0.         -159.         520           -204.         0.         -772.         -561.         0.         -25.         6134           5.00         -234.         0.         -772.         456.         0.         -160.         529.           5.00         -134.         0.         -743.         109.         0.         -160.         529.           6.25         -175.         -1092.         0.         -160.         -25.         6144           6.25         -175.         -1092.         0.         -164.         658.           6.00         -151.         -884.         0.         -164.         658.           6.00         -176.         0.         -172.         4418         660.         67.         4518           7.5         -176.         0.         -174.         620.         0.         -278.         4518           1.25         -176.         0.         -172.         1048.         0.         -278.         4518           2.50	<b>a</b>	1	.811		•	-373.	56		၁	•	83	4	2
1.25         -213         0         -289         -594         0         -159         520           2.50         -234         0         -511         -261         0         -25         5874           2.50         -1390         0         -76         861         0         -25         5846           5.00         -1390         0         -76         861         0         -83         5846           6.25         -634         0         -72         861         0         -83         5846           6.25         -634         0         -716         -1092         0         -160         528           7.50         1175         0         -716         1092         0         -164         4618           6.00         -147         0         -649         844         0         -164         4618           6.00         -172         1048         0         -278         4418         462           5.00         -1741         0         -724         1600         0         -278         4418           5.00         -1741         0         -724         1600         0         -278         418	ċ		45.		•	-263.	65		•0	~	19	4	842.
2.50         -204.         0.         -511.         -261.         0.         -25.         5874           3.75         -635.         0.         -772.         656.         0.         -22.         6144           -0.5         -0.         -765.         861.         0.         -160.         -63.         6144           6.25         -0.         -765.         461.         0.         -160.	-	•	.513.			-289.	59		·	-	56	S	220.
3.75         -645.         0.         -772.         456.         0.         -22.         6184           5.20         -1390.         0.         -765.         861.         0.         -83.         5846           5.25         -134.         0.         -765.         861.         0.         -164.         4539           7.50         1175.         0.         -116.         -1092.         0.         -164.         4539           8.75         1186.         0.         -151.         -484.         0.         -122.         4418           0.00         -1761.         0.         -400.         260.         0.         -202.         5155           1.50         -1761.         0.         -792.         1048.         0.         -202.         5155           2.50         -1761.         0.         -724.         1500.         0.         -279.         3741           5.00         -2255.         0.         -724.         1500.         0.         -279.         4157           5.00         -1601.         0.         -724.         1500.         0.         -279.         4151.           5.00         -1742.         0.         -411.	2	•	-204-		•	-511.	26		ວ	Ĭ	52	S	874.
5.00         -1390.         0.         -634.         6446.         6.         -634.         6446.         6.         -634.         645.         646.         6.         -160.         5288.         6.         6.25         6.25         6.25         6.25         6.25         6.25         6.26         6.0         -164.         6.25         6.25         6.26         6.0         -164.         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.25         6.26         6.27         6.27         6.28         6.27         6.28         6.27         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         6.29         7.21         7.21         7.21         7.22         7.22         7.22         7.22         7.22         7.22         7.22         7.22         7.22         7.22         7.22         7.22	ě	1	635.		•	-772.	456.		ဝ	ı	22	9	184.
6.25         -634.         0.         -423.         49.         0.         -160.         5258           7.50         1175.         0.         -116.         -1092.         0.         -164.         4539           8.75         1186.         0.         -151.         -884.         0.         -122.         4539           9.00         -639.         844.         0.         -278.         5420           1.55         -1761.         0.         -792.         1048.         0.         -278.         5420           2.50         -1761.         0.         -724.         1600.         0.         -299.         3741           3.75         -2259.         0.         -724.         1600.         0.         -299.         3741           5.00         -2259.         0.         -623.         1397.         0.         -679.         4157           6.25         -1477.         0.         -623.         1382.         0.         -679.         4157           6.25         -1472.         0.         -411.         2702.         0.         -679.         4458.           6.00         -1742.         0.         -411.         2702. <td< td=""><td>Š</td><td>1-</td><td>390.</td><td></td><td>•</td><td>-765.</td><td>861.</td><td></td><td>•</td><td>1</td><td>83.</td><td>S</td><td>946.</td></td<>	Š	1-	390.		•	-765.	861.		•	1	83.	S	946.
7.50         1175         0         -116         -1092         0         -164         4589           0.0         -151         -884         0         -122         4418           1186         0         -151         -884         0         -202         5155           1186         0         -639         844         0         -202         5420           1.25         -1761         0         -639         1500         0         -278         5420           2.50         -1761         0         -724         1500         0         -299         3741           5.00         -2255         0         -724         1600         0         -299         3741           5.00         -1477         0         -623         1397         0         -699         4157           6.25         -1477         0         -623         1382         0         -749         3512           6.00         -1601         0         -411         272         0         -749         3512           7.50         -1645         0         -313         3648         0         -461         250           2.20         0 </td <td>9</td> <td>ľ</td> <td>.634.</td> <td></td> <td>•</td> <td>-423.</td> <td>6</td> <td></td> <td>•0</td> <td>-1-</td> <td>•09</td> <td>ď</td> <td>258.</td>	9	ľ	.634.		•	-423.	6		•0	-1-	•09	ď	258.
8.75       1186.       0.       -152.       4418         0.000       -512.       0.       -639.       260.       0.       -202.       5155.         1.25       -1476.       0.       -649.       844.       0.       -278.       5420.         2.50       -1476.       0.       -629.       1741.       0.       -207.       4399.         3.75       -2358.       0.       -724.       1600.       0.       -629.       4157.         5.00       -2255.       0.       -724.       1600.       0.       -679.       4157.         6.25       -1477.       0.       -724.       1600.       0.       -679.       4157.         6.25       -1601.       0.       -724.       1600.       0.       -674.       4528.         7.50       -1601.       2702.       0.       -424.       3365.         1.25       -1645.       0.       -424.       3365.         1.25       -2295.       0.       -283.       4458.       0.       -461.       2790.         2.50       -2295.       0.       -283.       4458.       0.       -430.       1433.         2.50 </td <td>۲.</td> <td>7</td> <td>.175.</td> <td></td> <td>•</td> <td>-116.</td> <td>1092</td> <td></td> <td>• •</td> <td>1</td> <td>. +9</td> <td>4</td> <td>589.</td>	۲.	7	.175.		•	-116.	1092		• •	1	. +9	4	589.
0.00     -512.     0.     -639.     844.     0.     -278.     5420.       1.25     -1470.     0.     -639.     844.     0.     -278.     5420.       2.50     -1761.     0.     -792.     1048.     0.     -299.     4134.       3.75     -2358.     0.     -1813.     1500.     0.     -299.     4157.       3.75     -2255.     0.     -724.     1600.     0.     -679.     4157.       6.25     -1601.     0.     -723.     1382.     0.     -479.     4511       7.50     -1601.     0.     -411.     2702.     0.     -424.     4511       0.00     -1742.     0.     -343.     3086.     0.     -468.     2851       0.00     -2295.     0.     -283.     4458.     0.     -468.     1872       0.00     -2295.     0.     -283.     4458.     0.     -630.     1438       1.25     -1538.     0.     -295.     4381.     0.     -491.     1438       2.00     -1538.     0.     -295.     2324.     0.     -491.     1161       1.50     -48.     0.     -295.     4381.     0.	æ	7	.186.		•	-151-	884		• •	7	22.	4	418.
1.25       -1476.       0.       -278.       5420         2.50       -1761.       0.       -207.       4399         2.50       -1761.       0.       -299.       3741         3.75       -2358.       0.       -183.       1500.       0.       -299.       3741         5.00       -2255.       0.       -724.       1600.       0.       -609.       4157         6.25       -1477.       0.       -523.       1387.       0.       -674.       472.         6.25       -1601.       0.       -523.       1382.       0.       -479.       3761.         7.50       -1601.       0.       -411.       2702.       0.       -424.       3365         30.0       -1742.       0.       -343.       3648.       0.       -468.       2491.         1.25       -1245.       0.       -283.       4458.       0.       -550.       2490.         2.257.       0.       -295.       4381.       0.       -630.       -630.       1433.         5.00       -1273.       0.       -295.       4381.       0.       -491.       1715.         6.25       -1273. <td>Ö</td> <td>•</td> <td>-512-</td> <td></td> <td>•</td> <td>-400-</td> <td></td> <td></td> <td>•</td> <td>-2-</td> <td>05.</td> <td>3</td> <td>155.</td>	Ö	•	-512-		•	-400-			•	-2-	05.	3	155.
2.50       -1761.       0.       -207.       4399         3.75       -2358.       0.       -813.       1500.       0.       -299.       3741         5.00       -2255.       0.       -724.       1600.       0.       -699.       4157         6.25       -1477.       0.       -623.       1397.       0.       -674.       4228         6.25       -1477.       0.       -523.       1882.       0.       -679.       3721         7.50       -1601.       0.       -523.       1882.       0.       -479.       3721         9.75       -2089.       0.       -4411.       2702.       0.       -424.       3541         0.00       -1742.       0.       -343.       3648.       0.       -468.       2951         1.25       -2295.       0.       -283.       4458.       0.       -550.       2491.       1843         2.50       -2295.       0.       -295.       4381.       0.       -630.       1433         5.00       -1273.       0.       -295.       354.       0.       -491.       1715         -250       -243.       0.       -295.	-	-1	470.		•	-659-			• •	7-	78.	S	<b>4</b> 50.
3.75       -2358.       0.       -813.       1500.       0.       -299.       3741         5.00       -2255.       0.       -724.       1600.       0.       -609.       4157         6.25       -1477.       0.       -623.       1397.       0.       -674.       4228         7.50       -1601.       0.       -523.       1682.       0.       -479.       3721         7.50       -2089.       0.       -411.       2702.       0.       -424.       3511         8.75       -2089.       0.       -411.       2702.       0.       -424.       3511         0.00       -1742.       0.       -343.       3648.       0.       -468.       2458.         1.25       -2295.       0.       -283.       4458.       0.       -550.       2490.         2.50       -2257.       0.       -295.       4381.       0.       -630.       1433         5.00       -1538.       0.       -295.       4381.       0.       -491.       1753         6.25       -1273.       0.       -295.       2324.       0.       -491.       1751.         7.50       -48.	2	1-	.761.		•	-792-	048		•0	7-	07.	4	399.
5.00       -2255.       0.       -724.       1600.       0.       -674.       4228         6.25       -1477.       0.       -623.       1397.       0.       -674.       4228         7.50       -1601.       0.       -523.       1682.       0.       -479.       3721         7.50       -2089.       0.       -411.       2702.       0.       -424.       3511         0.00       -313.       3086.       0.       -468.       3365         1.25       -1645.       0.       -283.       4458.       0.       -461.       2490.         2.50       -2295.       0.       -295.       4381.       0.       -630.       1872.         5.00       -1538.       0.       -303.       3586.       0.       -491.       1743.         6.25       -1273.       0.       -166.       3031.       0.       -491.       175.         7.50       -943.       0.       203.       -436.       0.       -491.       1161.         8.75       -48.       0.       -203.       1284.       0.       -513.       1161.	m.	-2	358.		•	-813.	1500.		•	7-	.66		141.
6.25       -1477.       0.       -674.       4228         7.50       -1601.       0.       -479.       3721         7.50       -1601.       0.       -479.       3721         9.75       -2089.       0.       -411.       2702.       0.       -424.       3511         0.00       -343.       3086.       0.       -468.       3365         1.25       -1742.       0.       -313.       3648.       0.       -461.       2951.         1.25       -2295.       4458.       0.       -550.       2490.       2490.         2.50       -2295.       4381.       0.       -530.       1872.         3.75       -2257.       0.       -295.       4381.       0.       -491.       1433         5.00       -1538.       0.       -166.       3031.       0.       -491.       175         6.25       -1273.       0.       -265.       2324.       0.       -436.       1161.         7.50       -48.       0.       -203.       1284.       0.       -513.       1161.	Š	7-2	:255.		•	-724.	1600.		0	9-	.60	4	157.
7.50       -1601.       0.       -479.       3721         8.75       -2089.       0.       -411.       2702.       0.       -424.       3511         9.75       -2089.       0.       -411.       2702.       0.       -424.       3511         0.00       -1742.       0.       -343.       3648.       0.       -468.       2951         1.25       -1645.       0.       -283.       4458.       0.       -550.       2491.         2.50       -2295.       4381.       0.       -630.       1872         5.00       -1538.       0.       -295.       4381.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -491.       175         7.50       -943.       0.       203.       1284.       0.       -513.       1161.         8.75       -48.       0.       203.       1284.       0.       -513.       1161.	•	7-	477.		•	-623.	39		•	9-	74.	4	228.
8.75       -2089.       0.       -411.       2702.       0.       -424.       3511         0.00       -1742.       0.       -343.       3086.       0.       -468.       3365         0.00       -1645.       0.       -313.       3648.       0.       -461.       2951         2.50       -2295.       0.       -283.       4458.       0.       -550.       2490.         3.75       -2257.       0.       -295.       4381.       0.       -630.       1432         5.00       -1538.       0.       -303.       3586.       0.       -491.       1753         6.25       -1273.       0.       -166.       3031.       0.       -436.       1850         7.50       -943.       0.       203.       1284.       0.       -513.       1161.	۲.	7-	.109		•	-523.	38		•	4-	.61	•	721.
0.00       -1742.       0.       -343.       3086.       0.       -468.       3365         1.25       -1645.       0.       -313.       3648.       0.       -461.       2951.         2.50       -2295.       0.       -283.       4458.       0.       -550.       2490.         3.75       -2257.       0.       -295.       4381.       0.       -630.       1872.         5.00       -1538.       0.       -303.       3586.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -436.       1850.         7.50       -943.       0.       203.       1284.       0.       -513.       1161.	æ	-2	.089		•	-411•	70	·	•	4-	24.	7	511.
1.25       -1645.       0.       -313.       3648.       0.       -461.       2951         2.50       -2295.       4458.       0.       -550.       2490         3.75       -2257.       0.       -295.       4381.       0.       -630.       1872         5.00       -1538.       0.       -303.       3586.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -491.       1715         7.50       -943.       0.       203.       1284.       0.       -513.       1161.	ċ	1-	742.		•	-343.	086		•	7-	99	3	365.
2.50       -2295       0.       -283.       4458.       0.       -550.       2490         3.75       -2257.       0.       -295.       4381.       0.       -630.       1872         5.00       -1538.       0.       -303.       3586.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -436.       1715         7.50       -943.       0.       203.       1284.       0.       -513.       1161.	<b>-</b>	-	649		•	-313.	648		•0	4-	19	7	951.
3.75       -2257.       0.       -295.       4381.       0.       -630.       1872         5.00       -1538.       0.       -303.       3586.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -362.       1715         7.50       -943.       0.       65.       2324.       0.       -436.       1161         8.75       -48.       0.       203.       1284.       0.       -513.       1161	2	~	567		·0	28	458		•	S	20	2	430.
5.00       -1538.       0.       -303.       3586.       0.       -491.       1433         6.25       -1273.       0.       -166.       3031.       0.       -362.       1715.         7.50       -943.       0.       65.       2324.       0.       -436.       1850.         8.75       -48.       0.       203.       1284.       0.       -513.       1161.	3	N	257		•0	59	381		•	Q	30	-	872.
6.25       -1273.       0.       -166.       3031.       0.       -362.       1715         7.50       -943.       0.       65.       2324.       0.       -436.       1850         8.75       -48.       0.       203.       1284.       0.       -513.       1161	Š	-4	53		•0	30	58		o	4	16	-	433.
7.50 -943.	•	-	27		•0	16	03		•	3	62	-	715.
8.75 -48. 0. 203. 1284. 0513. 116	7.	1	943		••	5	32		• •	4		1	850.
	æ		4		• • • • • • • • • • • • • • • • • • • •	0	28		°	S		-	•

RUN 21 VKTS = V/OR =	90.0 90.0 0.249	13 OMEG*R RHU100	# 00 # 11	610.3 0.2165		ALFS,C = CP/S = 0.00	8.5	CLR/5, R COR/5, R	=0.08979 =0.01528	CMY/S,R = 0.1735 CMX/S,R =-0.0028
	LOWER	RCTUR B	BLADE	NURMAL 28	BENDING .3R	S MOMENT	LR E	LR EDGEWISE Bending .1R	LR PITCH	TCH LUAD
V		•	•	<b>.</b>		•	! !		) 	
000	<u>6</u>	57	9	8	-1317.	-579.		-3235.	-3	.90
88.7	ň	2	Š	•	1487	-613.		-3951.	£-	_
77.5	1	2	21	•	373	-723.		-4516.	-5	.96
	-21	131.	-146	. 49	02	-858-		-4385.	£-	-319.
55.0	7	72	50-	.5.	-811.	-856.		-4383.	2-	55.
43.7	7-	78	-102	.9.	-963.	-738.		-5276.	1-	-143.
32.5	-3	50	-168	•	-1204.	-553.		-6292.	1-	172.
21.2	£-	65	-194	•	-1182.	-513.		-6376	7-	206.
10.0	1	10	-141	.2.	-937.	-651.		-5985-	,	
98.7	7-	08	-76	.90	-705.	-181-		-6250-		38.
87.5	1-	9	-71	3.	-646.	-1111.		-1140.		64.
76.2	7-	59	-11â	. 4.	-817.	-677.		-7568.		83.
65.0	-3	3293.	-176		-1082.	-562.		-1044.		
53.1		0.4	561-	•	-1199.	-465.		-6354.	1	28.
42.5	£,	5	-201	•	-1131.	-384.		-6448-	ļ	
31.2	1	9	-205	•	-1023.	-320.		-7021.		33.
20°C	£-	51	161-	8.	-931.	-230.		-6920-		-0-
08.7	-3	85	-175	. 4.	-829.	-235.		-6027.	•	17.
7.5	<u>.                                    </u>	~	-170	.9(	-738.	-175.		-5540.	•	-13.
6.2	<u>8</u> -	1	391-	34.	-686-	-138.		-60009-	•	-70.
5.0	-3	-	-158	.5.	-672.	-129.		-6366.	1	95.
3.1	Ę.	4	-16(	)1.	-693-	-108.		-5755.	•	-41.
2.5	£-	612.	-176	.1.	-129.	-104.		-4861.	•	32.
1.2	£-1	9	-11	.0	-751.	-150.		-4797.	•	-96-
0.0	-3	~	-158	34.	-727.	-216.		-5299.	-1	175.
8.7	7-	45	<b>551 - 1</b>	.;	-649-	-566-		-5217.	-2	.42.
3	-2	61	12	74.	-634.	-397.		-4370.	7-	.32.
56.2	7-	74		30.	80	-425.		-3769.	61-	.95.
345.00	-33	194.	-	38.	-1027.	-393.		-3978.	7-	71.
33.7	¥-	85	<b>1</b> 8	:1.	-1078.	-645-		31	ۥ	4
22.5		37	-101	• 91				16	7-	œ
7.11	<u>,</u>	æ	7.2	.60	-1001-	-613.		-3301.	-2	.39•

CMY/5,R = 0.2227 CMX/5,R =-0.0034	a <b>4</b>	CGS SIN	2465.5	753.7 -580.4	-240			•					41.3 87.6																
CLR/5, R = 0.11858 (CDR/5, R = 0.01911 (	BENDING MCMENT	COS SIN		2 1153.2	-134.0	91.1	-205.9	88.0	-132.7	-32.1	-12.6 3.2	-1-1	-7.3 22.7						4113.6	6.0 1105.5		ı		5.3 -304.9		•			2.5 187.0
ALFS,C = 8.8 CI CP/S = 0.002092 CI	BLADE YURMAL	NIS	4		0•0	0.0	0.0	0.0	C•0	0.0	0.0	٥•٥	0.0		UPPER KUTOR	70	N I	-		286.6 -	-0-2	34.8	-18.9	-124.9	-19.6	117.7	-36.9	17.9	1 -13.2 -
= 608.3 = 0.2161	UPPER RUICK	SIN CES		202.3		202.0		430.1		æ.			-106.9		EDGEW 1SE	ENT . IR PI				3.0 -108.1									0.0
PGINI 14 90-1 GAEG#R J-250 KHULCÜ	¥1•	SUS	1805	-122.9	230.9	108.2	406.9	-66.3	29.3	53•3	-36.1	m	-92.4		UPPEK RUIGR	BEND ING MO	503		0.0	c • o	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RUN 21 VKIS = V/CR =		HARMONIC	c.	~-	·u (	η,	<b>\$</b> (	ጥ ‹	ا ۵	<b>-</b>	ന -		10	12	28			HARMONIC	c	<b></b> • (	2	<b>~</b> ∩ ·	<b>\$</b> (	5	\$	_	or i		0

The second secon

RUN 21 VKTS = V/CR =	POINT 90-1 3-250	24 ONE RHC	OMEG#R = RHULOO =	608.3 0.2161	ALFS,C CP/S =	.C = 8.8 = 0.002092	8 • 8 20 92	CLR/5, R CDR/5, R	=0.11858 =0.01911	CMY/S,R = CMX/S,R =	= 0.2227 =-0.0034	
			ļ		LOWER RCTUR	JK BLADE	NORMAL	BENDING MOMENT	MOMENT	•	ć	
		. cos	IR SIN		\$000	SE SIN		. 3K COS	NIS SIN	<b>.6</b> . CUS	NIS SIN	
HARYCNIC												
0	5	599.9			1009.3			837.2		-221.5		
-4	5	557.9	-2902-	0	352.2	-1869.2		357.2	8.016-	183.4	145.1	
2	2	55.8	251.	5	116.0	137.4		12.1	97.1	-73.5	26.7	
. ~		11.5	-103	8	0.01-	9-69-		0•9	6-14-	32.1	-28.0	
•	7		325.	-4	152.8	159.1		56.8	9.501	-43.8	-56.4	
. د	1-		-323	0	-165.2	-114.5		-77.2	-38.1	32.4	36.3	
· •	•		589	. 00	162.5	309.7		42.1	165.4	1.6-	-63.6	
. ~	7	•	16.	Z.	151.7	-58.9		73.3	8.8	-28.5	-3.7	
a.	· •	61.7	-113	. ~	-45.3	-23.1		12.8	-0-3	2.2	8.0	
6			-196	2	-30.3	-80.2		11.0	4.6	-1.7	18.7	
61		28.5	-3.5	S.	13.2	-17.8		14.5	-10.4	-5.9	3.0	
1												
29	<u> </u>		1000 00	-	0.700.0							
•	ことによった。		1.5	M 1 SE		RUIUR TE						
	NE.N	BENDING >	MOMENT	•1R	PIICH LINK	INK LUAD						
		SOO	270		\$3 <b>2</b>	2 7 0						
HARMINIC												
c	-57	٠			-92.0							
	77	2201.8	-394.	89	-141.9	124.1						
<b>C</b> 1	ζ-I	-560.4	-118	7	33.2	18.0						
•	1		118.	-4	-28.9	9.0-						
.*	•		3.6	9	6.4	14.0						
\$		•	-47.	9	-17.5	-22.6						
· •c	ł		-24.7		50.5	-3.3						
_	7	-	0.41-	· )	18.8	-27.9						
α	•		24.6	٥	-1.8	16.4						
· c			4	C	18.1	-16.9						
		12.4	. 61		17.6	5.611						
2			•	•	,	•						

	PCINT	14						,	1			!
VKTS = V/CR =	90.1	CAEC*R RHU100	4 0 1 1	608.3	3 ALFS,C 1 CP/S =	# 0	8.8 .00200.	CL R/S, R COR/S, R	=0.11858 =0.01911	CMY/S, R CMX/S, R	S, R = 0.222 S, R = -0.003	27 34
	UPPER	CTCR	BLADE	NURMAL	BENDING	MOM	UR EDGE	72	UR PITCH	TCH	UPPER RUIOK	3%
·			•		4	6		•		2	,	)
7	•	•		(				Ć	•	•		ı
) )	•	.6767		•	1355.	1000		<b>.</b>	<b>†</b>	_	121	•
1.2	•	2324.		•	1335.	2398.		္	<u> </u>	563.	7	8
2.5	•	2523.		•	1394.	2698.		ċ	-5	83.	77	<b>.</b>
3.7	•	5003.		•0	1662.	2906.		•	1-	-140.	363	5.
5.0	•	3416.		•	1977.	3221.		o	-	139.	417	9.
6.2	• • •	3842.		•0	2077.	3079.		•	en .	371.	077	5.
.5	•	4380.		•	2093.	2524.		•	~	240.	684	.6
8.7	•	.966		•	2239.	1988.		• •	1-	. 56.	695	<b>-</b>
0.0		5307.		•0	2380.	1654.		•	-2	.47.	581	•
1.2	٠,	5046.		•0	2299.	1810.		•		-5.	579	0
12.5	•	4564.		•	1991.	2486.		•	2	.47.	779	9.
3.7	•	3940.		•0	1661.	3070.		• •	2	209.	69	8.
35.0	•	3329.		•	1642.	2800.		•	1	-30.	588	4.
146.25	•	3901.		•0	1946.	1462.		•0	1-	. 401	489	۲٠
57.5	_,	5296.		•	2051.	59.		•	7	106.	28	<b>6</b>
68.7	•	4815.		•	1631.	113.		•	2	20.	50	·.
80.0	•	2159.		•	973.	1360.		•		12.	14	3.
91.2		89.		•0	407.	2078.		•	1-	. 55.	56	2.
02.5	•	-612.		•	38.	1969.		•	•	-80•	29	5.
13.7	•	-975.		•0	-67.	1840.		•	7-	155.	99	5.
25.0	•	-141.		•	5•	1650.		•	1.5	.515.	10	
36.2	•	-216.		0.	51.	1524.		•	-7	,02.	25	5.
47.5	•	-676.		•	57.	2164.		•	<u>ر .</u>	504.	07	<b>.</b>
58.7	1	-1414.		•	55.	3174.		•	7-	-270.	90	•
70.0	ť	-1290.		• 0	16.	3877.		•	-2	.35.	383	5.
81.2	ľ	-1295.		•	39.	4618.		• •	<b>5</b> 1	470.	53	5.
92.5	1	3		•0	5	1		0	-5	. 199	08	9.
03.7	1-	Ò		•	$\sim$	792		•	140	.94.	15	•
15.0	•	-547.		•	257.	970			-3	371.	19	•
26.2		46.		•	575.	3272.		•	13	334.	2	3.
37.5		.166		•0	02	228		•	-3		96	•
48.7	•	2186.		•0	1293.	324		•	41	. 16.	88	O.

RUN 21 VKTS = V/OR =	POINT 90.1 0.250	14 OME RHO	OMEG#K = RHG100 =	608.3 0.2161	ALFS.C.	%C = 8.8 = 0.002092	.8 CLR/S,R 92 CDR/S,R	=0.11858 CMY/S,R = 0.2227 =0.01911 CMX/S,R =-0.0034	<u> </u>
	LOWER	RUTOR		NURMAL	NDING	MOMENT	LR EDGEWISE	LR PITCH	
S		4	•	į.	•	<b>.</b>	•		
0.00	Ř		28	57.	1789.	-272.	-3577.	-255.	
88.7	ż	ø	23.	2	1519.	-235.	-4505.	-255.	
77.5	ř	4	23,	86.	1669.	-318.	-4846		
6.2	403	037.	58	.69	1874.	-435.	-4517.	-295.	
55.0	Ř	4	32,	45.	1943.	-427.	-4815.	-231.	
43.7	Ž		97	95.	1633.	-292-	-6569•	-85.	
32.5	<b>~</b>		18	07.	1183.	-161-	-1519.	-101-	
21.2	<b>~</b>		14	34.	1052.	-260-	-7614.	-177.	
10.0	Ž	<b>,56</b> .	17	85.	1207.	-466.	-7186.	-56.	
7.86	Ñ	876.	21	84.	1230.	-949-	-1120.	140.	
87.5	7	582.	18	18.	932.	-658.	-8976.	182.	
76.2	Ĩ	529.	ŏ	99.	426.	-513.	-9308•	121.	
65.0	17-	573.	-3	20.	-56.	-367.	-8182	71.	
53.7	7-	789.	9-	1.	-278.	-314.	-7153.	48.	
42.5	1-	951.	-7	•	-244.	-288-	-1441-	48•	
31.2	-2,	135.	1-	•	-165.	-249.	-1951.	54•	
20.02	17-	386.	12-	3.	-130•	-221.	-7233.	70.	
08.7	-2	215.	9-	•	-118.	5	-5879.	. 61	
7.5	-2	.606	6-	5.	-133.	-13.	-5433.	14.	
•2	-76	89	-10	3.	-108.	• 99	-1685-	-82.	
5.0	-16	2	12-	03.	15.	45.	-2891	-69-	
3.7	7-	26	-3	55.	153.	44.	-4831.	• 20	
2.5	77-	595.	-3.	35.	273.	75.	-3827.	10.	
1.2	ĭ	904.	Ī	.06	*644	24.	-4105.	-50•	
0.0	~	138.	Š	15.	710.	-67.	-4814.	-142.	
8.7	•	711.	10	55.	9	-100.	-4196.	-234.	
.5	E1	313.	14	75.	1313.	-130.	-3730.	-715.	
56.2	7	792.	17	77.	31	-124.	-3438.	-146.	
45.0	7	016.	17.	.04	1170.	-58.	-4212•	-231.	
333.75	7	105.	171	16.	32	S	79	-359.	
22.5	7	830.	.77	71.	1753.	മ	97	-316-	
11.2	ጘ	641.	79.	31.	1948.	-299•	-3269.	-238•	

FUN 21 VKTS = V/OR =	90.0 90.0 0.249	LS CAE RHC	CMEG*R RHU100	0	610.2	ALFS,C CP/S =	11	9.0 0.003825	CLR/5,R COK/5,R	=0.14057 =0.02179		CMY/S,R =	= 0.2597 =-0.0059	
					J. A.	UPPER RCTOR	R BLADE	NORMAL		BENDING MLMENT				
		. 800	• LR S	NIS		.2P. CDS	SIN		. 3R CUS	a NIS		. 68 CUS	SIN	
HAR YON IC	•	)	)	<u>.</u>			i i		040		.,			
c.	2/10	201				•			0.0761	4		2,500.5		
	~		5582	5.2		ဂ • ၁	0.0	_	481.3	7583.5	<b>-</b>	10003	211.4	
~	4	108.3	-574.9	6.4		၁ <b>•</b> ၁	o• o	~	-94.3	-788.5	7	-1067.1	1.164-	
۳	Ĭ	1.1.4-	16	168.4		0.0	0.0	•	-78.2	96.1	•	-393.4	395.3	
4	•	-1.8	-663.6	3.6		0.0	0.0	•	-33.5	-208.4		8.0-	683.1	
2	-127	27.0	67	795.7		0.0	0.0	_	-8.8	34.8		55.0	6-127-	
9	ĭ	-63.8	64-	3.664		0.0	0	•	-65.4	-171.8		211.9	313.5	
7	•	41.6	77	14.4		0.0	0	•	55.5	-61.1		-85.9	-53.4	
8	7-	178.7	17-	5.1		0.0	0.0	•	-12.5	32.5		167.0	98.86	
6	2	282.2		7.7		0.0	0	~	-5.1	5.1	•	-108.9	58.5	
10	7-	124.7	-13	8.5		0.0	0.0	-	-11.7	33•3		63.7	666	
	UPPER	RC	JR ED	=	SE	UPPER RUTOR	_		UPPER	RUTUR				
	BEN	BENDING	MOMENT .	_	∝	PITCH LINK	NK LCAD	•	SHAFT	STRESS				
	_	503	S	Z		CUS	SIN		SOS	SIS				
HAPMONIC														
0		0.0				-70.0			4449.6					
-		0.0		0.0	•	-147.6	373.2	•	-974.5	1447.1				
2		0.0		0.0		44.8	-36.8	_	1-099-	219.5				
3		0.0		0.0		-89.3	1.19		43.7	-12.3				
4		0.0		0.0		-62.5	-17.9	•	94.1	35.7				
2		0.0		0.0		1.61-	-138.7	~	-339.1	-309.2				
9		0.0		0.0		34.4	15.8		24.5	113.7				
1		0.0		0.0		0.09	133.0		-423.0	-27.4				
&		0.0		0.0		-41.1	-7.6		42.1	205.1				
6		0.0		0.0		39.7	-4.6	۰.۵	4.9	109.5				
10		0.0		0.0		1-6-7	13.	_	6.65-	766.8				

= 0.2597 =-0.0059	-0.1 -0.1 -103.2 -103.2 -71.7 -71.9 47.8 0.5
CMY/S,R =	163.4 163.1 163.1 163.1 163.0 163.0 163.0
=0.14057 =0.02179	AUMENT S IN S
CL R/S, R CUR /S, R	BENDING COS 3 COS -3 -292.7 -172.6 -29.1 -29.1 -29.2 -29.5 -29.5
5.C = 9.0 S = 0.003825	TCR BLADE MORMAL  -2K  SIN  -3458.0  -3458.0  -103.7  382.6  36.9  368.0  -177.7  -40.6  -177.7  -40.6  154.8  154.8  12.8  12.8  147.7  -7.3
.2 ALFS,C 61 CP/S =	LGWER RCTCR  COS  3159.5  4.1  -53.2  149.3  114.0  -13.7  149.3  114.0  -13.7  -149.3  -179.2  -34.4  -179.2  -35.1  23.5  1.5  42.0  16.2  -6.8
UMEG*R = 610.2 RHU100 = 0.2161	S. SIN
PUINT 15 90.0 0.249 RH	282.0 -5208. 282.0 -5208. 282.0 -5208. 62.5 -18839.6 -18840.9 609. 10.3 -27131.4 -298. 203.0 -417. 203.0 -417. 203.0 -417. 203.0 -4176061.4 -298. 3072.0 3496061.4 349.
RUN 21 VKTS = V/OR =	133 H MARARA L & Q C

KUN 21 VKTS = V/OR =	PCINT 90.0 0.249	15 UME RHC	UMEG*R = RHUI 00 =	610.2	2 ALFS,C 1 CP/S =	. 0	9.0 33825	CLR/S, R CDR/S, R	=0.14057	CMY/Saf	5,K = 0.2597 5,K =-0.0059
	UPPER	ROTUR	BLAD	NCRMAL	BENDING	ž S	UR E	R EDGEWISE	UR PITCH	ς.	UPPER KUTOR
		• TY	•	J	۲,	•		•	C ALIA		,
S										!	:
0	4	1307.		•	2158.	~		•	-55	-257.	77
1.2	4	+522.		•	2369.	3886		o	7	72.	3504.
2.5	un	1803.		•	2747.	3735.		°	7	•06	87
3.7	,~	7152.		0.	3412.	3863.		•	ī	61.	36
0	-	7885.		•0	4041.	4332.		• •	2	64.	5325
6.2	w	3418.		•0	4183.	4417.		•	Ñ	03.	47
7.5	w	3927.		•	4075.	4204.		•	4	424.	5641.
~	<b></b>	9212.		•	4188.	4095.		• •	-	•09	6412.
0.0	v	1113.		•	4384.	4010		•	-2	211.	6548
1.2	w	3373.		•	4301.	4004		•	-	23.	6215
12.5	w	3776.		•0	3912.	4228.		•	4	97.	6752.
3.7	3	3053.		•	3483.	4478.		• •	Š	46.	1014.
35.0	•	,607.		•	3352.	4138.		•	2	56.	6131.
46.2	~	5525.		•0	3436.	2647.		•	2	235.	5105.
7.5	-	7684.		•	3133.	955.		• o	4	05.	4440
168.7	•	5436.		°.	2255.	964.		• •	5	93.	4555.
0.0	• •	2593.		•	1309.	2204.		• 0		55.	5599.
1.2		156.		•	596.	2391.		• •	•	44.	5689.
2.5	•	-255.		•	.99	1539.		o		72.	4197.
3.7	1	-840.		•0	-201.	1173.		•	7		3533.
5.0	7	1245.		•	-244.	1172.		•	4-	39.	4217.
6.2	7	1330.		•	-306-	1263.		• •	-5	. 76	4399.
7.5	-	.1564.		•	-379.	2186.		•	-5	19.	4107.
8.7	-2	22 90 •		•	-333•	3572.		•	-3	36.	4145
0.0	-	93		•0	-192.	4498.		•	-2	81.	3975.
1.2	-	•		•	63.	5228.		• •	4-	32.	3578.
2.5	1	42		•0	374.	5697.		•	-5	•	7657
3.7	•	53		•		5210.		• •	4-	76.	1902.
5.0				•0	-	4214.		•		~	1920.
326.25	-	1955.		•0	38	3323.		•	-5	7	3282.
7.5	LCT)	3166.		•	1938.	2439.		•		54.	3296.
8.7	4	77		•	13	2224.		•		0	97

RUN 21 VKTS = V/OR =	POINT 90.0 0.249	15 OME RHO	OMEG#R = RHD100 =	610.2 0.2161	ALFS,C CP/S =	°C = 9.0 = 0.003825	.0 CLR/S,R 25 COR/S,R	=0.14057 =0.02179	CMY/S,R = 0.2597 CMX/S,R =-0.0059
	LOWER	ROTOR	BLADE	NORMAL	NDING	MOMENT	LR EDGEWISE	LR PITCH	c
S	-	4		4	•	6	•	רואי רואי	<b>a</b>
000	.80	S	~	98.	3	-47.	-4666.	0	<b>3.</b>
88.7	72	90	2	86.	4239.	73.	-5362.		
77.5	.8	86	-	.06	4191.	48.	-5656	S	
66.2	æ	~	S	77.	4290.	-27.	-5717.	00	•
5.0	86	60	665	•	4358.	14.	-6549.	-11	•9
43.7	7.	35	-	•	4067.	.96	-1560.	-12	2.
32.5	39	18	4	87.	3631.	91.	-8625.	-36	• 9
21.2	9	89	$\overline{}$	•	3498.	-23.	-8611.	-170	•0
10.0	7	O	~	37.	3501.	-231.	-8448-	43	3.
98.7	59	14	2		3222.	-415.	-9236	272	2.
87.5	7	63	3		2639.	-386-	-10258	256	• 9
76.2	51	44	~		1907.	-211.	-10092	149	•6
65.0	~	0	4	•09	1225.	-144.	-8932.	141	1.
53.7	•1	19	0	38•	868.	-195.	-834C.	130	••
45.5	•	_	-	.,	804.	-175.	-870Z•	104	•
31.2	Ϊ'	48	_	.6	736.	-177-	-8584.	144	•
20.0	<b>7-</b>	39	_	3.	584.	-140 -	-7258	162	2.
08.7	-11	S	W1	50.	447.	-09-	-5845-	136	• •
7.5	-21	19	2	71.	373.	133.	-5310.	164	•
•	-11	23	55-	• 0•	393.	176.	-5258	184	•
5.0	"	44	<b>7</b>	01.	442.	85.	-4888	7	3.
3.7	01-	38	27	78.	451.	128.	-3968-	5	3.
2.5	-16	08	9-	•19	590.	209.	-3094	35	<i>y</i> .
7.1	. 7	9/	4	.0.	•136	67.	-3239	-5(	•0
0.0	72	85	ဆ	27.	1478.	-127.	-3978•	-18	<b>ω</b> •
3.7	2£	31	9		1991.	-112.	69	-234	•
.5	36	54	Ç	•	2395.	-10.	-5355-	-184	•
56.2	74	43	4		2445.	51.	-3265	-150	• 0
45.0	4.5	43	9	•	2408.	132.	-4566.	-75	2.
. 7	14	104.	382	25.	2890.	7	-4320.	$\sim$	• 9
22.5	7.	22	3		3736.		16	7	• 7
11.2	3	84	4	•	4260.	-72.	-3891•		5.

9 CLR/S,R = 0.06855 CMY/S,R = 0.1e65 1 CUR/S,R = 0.01593 CMX/S,R = -0.0004	BENDING MUMENT  • 3R  COS SIN	-784.5 630.0 -664.5 1530.7 -2299.3 90.8 -97.5 -460.6 -191.1 51.4 46.0 -385.4 134.1 219.0 -12.5 -794.5 177.3 -59.3 31.3 171.9 -180.5 -16.5 -56.1 52.6 98.2 39.0 -0.2 -44.8 -53.2 28.6 18.9 63.7 -34.3 7.2 -3.1 -97.8 -143.8	UPPER RGTUR SHAFT STRESS COS SIN 3506.5 -2476.7 -727.9 -596.4 -144.8 56.6 -142.8 -198.1 144.8 -198.1 144.8 -4.1 98.9
ALFS,C = 10.9 CP/S = 0.000251	RGTCR BLADE NURMAL  2R S SIN		UPPER RUTUR CGS SIN 84.3 249.3 -126.1 249.3 -7.0 -20.7 -85.6 -27.7 7.2 -42.9 33.9 -129.5 33.0 13.2 -20.8 52.1
= 627.9 = 0.2161		1050.0 -336.0 164.9 -96.1 246.8 -161.4 122.0 12.9 250.3	EDUENISE SIN O.O O.O O.O O.O O.O
PGINT 16 90.2 GMEG*K 0.242 RHU100	CUS	-1697.0 580.6 372.8 210.3 793.4 -12.7 -114.5 101.5	PPER RUTUR BENDING MD, COS O.O O.O O.O O.O
RUN 21 VKTS = V/OR =	HARMONIC	0 1 2 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8 4 8	136 H ARR ON 0 C L 0 E 4 & 0 F &

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CMY/S,R = 0.1665 CMX/S,R =-0.0004	-717.1 104.9 286.7 43.3 -4.6 11.8 -51.8 -51.1 3.0 41.7 11.6 -7.1 -36.7 -15.2 9.0 11.2 2.3 -7.1 -5.3 -7.1 -5.3
=0.06855 =0.01593	MUMENT S S IN 559.5 126.2 105.3 105.3 115.8
CLR/S, K CDR/S, R	COS .3R SIN .2821.3 S59.5 -132.4 559.5 105.3 105
= 10.9 0.000251	UR BLADE NURMAL 2R SIN 519.8 260.1 -57.3 -81.8 13.2 199.6 -85.4 12.7 -2.7 11.3 11.3 11.3 11.3 11.3 11.3 11.3 11.3 -2.7 -2.7 -2.7 -2.7 -2.7 -2.7 -2.7 -2.7 -1.8 14.2 -1.8 14.2 -1.8
ALFS,C CP/S =	COS .2R .28 .28 .373.6 .373.6 .373.7 .373.0 .125.4 .111.9
UMEG*R = 627.9 RHU100 = 0.2161	1R 449.6 514.7 -50.8 -142.6 380.6 -68.4 -45.7 53.5 -10.1 SIN SIN 23.1 -40.6 -222.1 0.7
PUINT 16 90.2 0.242	-6936.1 -710.2 -710.2 -710.2 -710.2 -710.2 -710.2 -710.2 -710.3 -
RUN 21 VKTS = V/OR =	137 HARA 10 1 2 2 4 2 5 7 2 6 9 1 10 1 2 2 4 2 5 7 2 6 9 1 10 1 2 6 9 9 1 10 1 2 6 9 9 1 10 1 2 6 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9

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RUN 21 VKTS = V/OR =	96.2 96.2 0.242	16 DMEG*R RHU100	11 11	627.9	ALFS,C CP/S =	14	13.9	CLR/5, R CDR/5, R	=0.06855 =0.01593	CMY/5, R CMX/5, R	S, K = 0.1665 S, R =-0.0004	565
	UPPER	KUTUR BLADE	Z 3	URMAL B	BENDING MCMENT	MCMENT 6R	UR E BENI	UR EDGEWISE BENDING .IR	UR PITCH		UPPER ROTUR SHAFT STRESS	TUR SS
v						,						
00.00	•	13	0		214.	947.		•	•	.69	-	.00
1.2	•	115	0	1	1			• •	-	38	1	.66
2.5	1-	Ň	0	•	546	9		· •	-11	•	17	13.
•	-23	~	·	1	853	327		•	1		001	.5.
5.0	-2	•	•	7	.1128.	1142.		•	-	187.	J	79.
6.2	-3	.406.	0	7	-1469.	790.		•	4	.68	15	97.
7.5	£-	679.	• •	-1	-1689.	97.		•	S	.89	~	.4.
	£-	015.	•	-1	-1650.	-1140.		o	8	378.	267	.4.
0.0	7-	150.	0	7	502.	-2137.		•	7	. 50 •	S	32.
1.2	-2	194.	0	7-	.464	-2215.		•	7	. 71.	36	.66
2.5	-2	.619.	•	7-	728.	-1716.		•	<b>~</b>	347.	41	. 9.
3.7	-3	.044.	0	-2	-20103-	-1068.		•	#	447.	5280	280.
5.0	£-	1665.	· ?	-2	.028.	-561.		<b>.</b>	4	.00	57	• • •
5.2	-3	$\sim$	•	-1	763.	-858-		•	2	263.	64	73.
7.5	1-	539.	•	7	-1457.	-1854.		• •	-	• 961	41	.90
3.7	•		•	7	238.	-2185-		ં	?	82.	43	8.
0.0	1-	_	၁	7-	122.	-1405.		•	ν,	340.	55	.4.
1.2	-2	4	•	-	141.	-516.		• 0	2	:53.	62	. **
2.5	-2	5	0	7	193.	130.		•	7	166.	58	78.
3.7	-2	9	•	7	109.	1054.		• •		89.	54	<b>.</b>
5.0	-2	.649.	• •	ı	88	1819.		ဂ	7	103.	25	34.
5.2	1-	.607.	•	1	9	1820.		•	?-	:72.	57	8.
7.5	1	-600-	·	•	28	1823.		ô	7-	-241.	5.10	197.
3.7	1	-486.	•		58.	2508.		ċ	1-	.22.	64	42.
0.0	1	-695-	0		262.	3281.		•		-55.	48	.7.
1.2	1	.313.	0		270.	8		•	1	.99.	~	.7.
5.5	ı	.717.	0		165.	4631.		•	1-	173.	3	23.
3.7	-1	~	0		103.	18		o	7-	.61.	-	•
5.0	1-	-	•		145.	4646.		• •	1-	176.	S	55.
7	1	37	·		Š	9		°	•	-37.		15.
7.5	1	7.1	•		223.	5		•	1	-14.	S	34.
3.7	ſ	~	•		7	82		°	•	-43.		

POINT 90.2 0.242 LCWER	16 OMEG*R = 627.9 RHUIOO = 3.2161 : RUIOR BLADE NURMAL	ALFS.C = 10.9 CP/S = 0.000251 BENDING MUMENT L	.9 CLR/S,R :51 CDR/S,R :EN EDGEWISE	
2.			<b>—</b>	LINK LOAD
6355	783713.	'	-3839	-359.
7159	•	96- •	-3872.	-379.
8158	•	51	-4516.	-439.
8.		- ·	-4592.	-413.
92.	•	<b>-</b> -	-4657	-687-
F- • • • • • • • • • • • • • • • • • • •	•	77-	-4/11.	<b>7</b> '
56.		18775.	-5593	-258.
844	•	8	-5667	-765.
133	-252	6-	-5717.	~
40 <b>.</b> – 3	-232		-1419-	•0
363	-238		-6700.	28•
1338	-253		-6636	-73.
384	-259		-6814.	- 46
08°	-256	1 I	-6692	12.
3440	-244		-6974	- 8-1
5940	-245			4
2340	-239	•	-6457.	-29•
1040	-235		-6357.	-123.
-68524104. -73314224.	-2416.	6439. 5424.	-6542. -6581.	-96. -67.
8742	-249	-43	-6197	-101.
1442	-249		-5807.	-88.
1961	-249	-50	-5905-	-91.
3840	-245	1	-6061.	-181.
353	-247	-57	-5568.	-242.
+042	-268	-58	-4774.	-264.
3345	-296	.8602.	-4400	-324.
38484	-316	99-	-16471	-365.
20501	-330	-	32	36
445	-345	.1.9 -841.	-4041.	-364.

- 0.1950		Z I A		60.7	14.0	21.5	82.5	4.07	94.8	71.6	91.5	81.0	-17.1																
			9•	6 -24		<b>~</b>	0	9	3	<b>(7)</b>	4	4	7																
CMY/S+R CMX/S+R		รูกว	702	8	-681	-621.	-944	76.	60	-80	7	76.	-48																
=0.08018	G MUMENT 3K	SIN		-1207.6	-206.8	31.8	-93.3	39.5	-93.2	9.01	-1.7	7.7	8.6		RUTÚR	STRESS	NIS	: :		-3373.3	$\sim$	-43.0	140.3	-266.9	16.1	-344.4	24	27.8	)
CL K/S, K CUK/S, R	BENUIN	cus	-892.3	721.2	9.66	8.2	268.8	-1.7	2.3	61.4	-28.7	22.1	-10.1			SHAFI			3913.1	41	-801.ĕ	139.7	-80.2	-14.5	-34.7	1-66-	-132.7	6.1	
= 11.1 0.000208	BLADE NGRMAL	N IS			0.0										ROTOR	LOAD	NIS			t	23.7	-53.2	1.66-	-76.3	61.8	1.6-		20.0	
ALFS,C CP/S =	UPPER RCTOR	SOO	0.0	0.0	ဂ•၀	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		UPPER RO	PITCH LINK	crs		81.6	-113.0	-25.2	-97.2	15.5	8.99	-4.6	-11.8	-11.0	4.01-	
0.4k = 675.0 00 = 0.2161		NIS		_	-542.7	4.87	-345.2	193.5	-279.4	151.8	-163.3	194.1	-132.9		EDGEWISE	ENT . IR	SIN			0•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
PUINT 17 91.1 UMEG#K 0.226 RHUIOO	**************************************	cus	-2054.4	319.6	5 *8 6 5	251.5	1346.3	-132.7	103.6	0.8	46.8	-179.1	-42.4		UPPEK RUTOR	I NC			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	•
NUN 21 VKTS = V/OR =		HARMONIC	0	-	~	<b>~</b>	<b>4</b>	r.	9	1	<b>&amp;</b>	6	C1	140	)			HAPMONIC	0	-	7	3	4	5	•	7	80	0	

į

= 0.1950 =-0.0052	209.3 -91.1 -91.3 -15.6 -15.6 -15.6 -7.5 3.6
CMY/S,R =	-555-1 -755-1 -755-1 -755-1 -75-2 -16-3 -17-1 -17-1 -17-1 -17-1
=0.08018 =0.01852	MUMENT - 152.6 - 152.6 - 152.6 - 1 13.6 - 1 13.6 - 1 13.6 - 1 13.6 - 1 13.5
CLR/S, R CDR/S, R	AL BENDING -1539.2 -1357.8 311.0 51.8 162.2 -72.4 44.9 42.3 23.4 4.7 -20.3
= 11.1 0.000208	BLADE NURM 51N 51N 51N 372.8 180.9 -70.2 -20.9 182.4 -97.2 81.2 18.7 -38.7 -38.7 -28.7 -29.2 17.9 -29.2 17.9 -29.2
ALFS,C CP/S =	CGS - 2R - 2576.1 - 2576.1 - 536.4 - 107.0 347.1 - 167.3 160.6 80.3 - 55.9 42.9 - 25.6 - 25.6 - 25.0
OMEG*R = 679.0 RHU100 = 0.2161	FLING TO THE TO
PGINT 17 91-1 OME 0-226 RHC	COS -4521.6 -3184.0 840.3 191.9 571.4 -259.0 71.8 220.7 -259.0 71.8 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1 -0.1
FUN 21 VFTS = V/GR =	HARYONIC 12 2 2 3 3 4 4 10 10 10 10 10 10 10 10 10 10 10 10 10

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PUN 21 VKTS =	POINT 91.1	17 OMEG*R	)) ~			ALFS,C =	11.1	CLK/5, K		CAY	CMY/S,K = 0.1950
œ	~	RHUI		0			300208	CUR/3, K	14	CAX	/5,R =-0.0u52
	UPPER	RUTCR BL	BLADE	NURMAL		BENDING MCMENT	ž	3	UR PITCH	Ξ	UPPER KUTÜK
		• 1k	٠	2K	.3R	•6R	NH S	BENDING . 1R		LGAD	SHAFT STRESS
S											
00.0		359.		•0	251.	-252	•	• •	•	- 86 •	
1.2	•	-626.		•	-280.	-134	•	ဝံ	-1	9	-3385.
2.5	-2	2007.		•	-006-	482		· •	1-	192.	-2823
3.7	£-	670.		•0	-1345.	908	•	•	•	Ś	-2012.
5.0	<b>5</b> -	4401.		•0	-1594.	856	•	• 0		153.	-2411.
6.2	-45	255.			-1807.	400,		•0	,	385.	-1773.
7.5	-43	327.		•	-1961-	-419	•	•	•	639.	-1110
8.7	-40	065.		•0	-1984.	- 1446		0	7	.690	-9-
0.0	£-	159.		0	-1950.	-2286.		• •	•,	385.	1476.
01.2	<b>6-</b>	3169.		•	-1997.	-2436	•	ဝံ	_	. 44	2399.
2.5	<b>5</b> -	.097.		•0	-2187.	-1771-	•	<b>.</b>		180.	3388
23.7	-43	394.		•0	-2468.	-016-	•	•	`',	338.	÷104•
5.0	-43	348.		•0	-2513.	-628	•	• •	7	435.	6234.
46.2	4-			• ວ	-2055.	-1090	•	•0	113	394.	<b>9679</b>
57.5	-2	48		•	-1463.	-1944	•	•0	. •	272.	6605.
68.7	ı	58		•0	-1272.	-2413.	•	•	•••	229.	7271.
80.0	1-	91		J.	-1372.	-1671.	•	•0		246.	8214.
91.2	7-	96		•0	-1381.	-193	•	•		.861	9739.
02.5	<b>.</b> 1	241.		·0	-1298.	638	•	•		144.	10560.
13.7	-2	65		•	-1212.	846	•	•0		<b>2</b> 8•	9928
25.0	-2	9		•	-995-	77	•	• •	ī	177.	6996
36.2	-1	1971.		•	-6009-	œ	•	•	ï	319.	10287.
47.5	1	7		•	-162.	822	•	•	7	-166.	10026.
58.7		39.		•0	207.	104	•	•	•	-68•	8856.
70.0				• •	462.	250	•	ဝ	7	200.	2
81.2	•	-131.		•	578.	34	•	•	7	-239.	6913.
92.5	1			•0	557.	98		•	ī	158.	5619.
3.	1	781.		•0	439.	5355	•	•	ī	188.	S
15.0	1	-896-		•	343.	98	•	•	-1-	9	1979.
26.2	1	481.		•0	390.	56	•	•	•	-52•	575.
37.5		561.		• •	511.			•			101.
48.7		_		•0	511.	4	•	•	•	-26.	6

RUN 21	7	17						:		ı
VKTS = V/OR =	91.1 0.226	OMEG*R RHJ100	# 10 # 10	679.0 0.2161	CP/S =	, c = 11.1 ; = 0.000208		CDR/S,R CDR/S,R CDR/S,R CDR/S	=0.08018 =0.01852	CMX/S,R = 0.1950 CMX/S,R =-0.0052
	LUWER	ROTOR B	BLADE N	NORMAL R	BENDING 38	MOMENT .68	LR EDGEWISE BENDING . 1K	MISE ALK	LENK LOAD	
v		•								1
000	151	960.	G	-	-2301.	-663.	64-	962.	-36	7.
_	10.	503.	•		2327.	-754.	-51	5115.	-405	5.
77.5	4-	907.	15	•	.2009.	-819-	-51	-5139.	-396	• 9
66.2	- 3	524.	251	•	-1536.	-006-	-53	343.	-428	.8
55.0	77-	.060	-	•	-1187.	-965.	-58	-5829.	-408	8.
43.7	-2	113.	01	•	.1060.	-855.	<u> 19-</u>	-6158.	-539	9.
32.5		138.	4	•	-1073.	-611.	-63	-6332.	-187	7.
21.2	-2	944.	_	•	-868-	-493.	-66	-6664.	-34	3.
10.0	ĩ	591.	-808	3.	-604-	-586-	-71	-1167.	-331	
98.7		746.	366	•	79.	-680	72-	-1690-	6-	.06
87.5	•	548.	693	<b>*</b>	289.	-628.	78-	-8209.	4	42.
76.2	ĩ'	,75.	373	•	293.	-505-	[R-	-87078-	4	46.
65.0	-1'-	-967	66-	•	72.	-386-	)6-	-8906-	2	70.
153.7	-2	120.	9	.•	-275.	-291.	16-	-9152•	6	36.
42.5	7-	-186	-	•	-466.	-226.	58-	-8992.	7-	24.
131.2	<u> </u>	525.	-1551	.•	-589-	-217.	38-	-8811.	-	18.
20.0	4-1	J76.	9	•	-903•	-270.	-84	-8664.	8	.2.
08.7	7	587.	N		-1250.	-341.	<u> </u>	-8379.	£-	35.
7.5	<u>3</u>	4 92 •	_		-1489.	-373.	51-	-1998.	-25	5.
6.2	SI	556.	3		-1817.	-378.	- 7	-1704.	1	-1.
5.0	-1	153.	6	•	-2246.	-404-	:1-	-7396.	-87	7.
3.7	-1	527.	Š	•	-2580.	-453.	59-	-6950-	-118	8.
2.5	<del>آ</del> ا	214.	1	•	-2309•	-468	<del>3</del> 9-	-6524.	£-	33.
1.2	80	534.	-		-2927.	- 466 -	79-	-6223.	-30	•0
0.0	1-	144.	5		-2849.	- 597.	-55	5960.	-136	6.
8.7	ğı	527.	3		-2652.	-101-	-56	.5679.	-217-	۷.
7.5	9-	210.	$\mathbf{r}$	· · ·	.2449.	-720.	-53	5324.	-54	3.
56.2	9-	335.	_	-	-2326.	-663.	54-	4923.	-277	7.
45.0	١	411.	w	- -	-2400•	-604.	34-	4693.	-33	30.
333.75	١	-6348-	-3950.		$\sim$	-573.	74-	-4662.	-386	
22.5	9-	329.	· U	•	240	- 261.	74-	-46+1.		7.
11.2	9-	275.	74	۶.	-2237.	-584.	14-	.601	<b>€</b> ₹-	ė.

RUN 21 VKTS = V/GR =	PulNT 9c.1 0.250	18 CMCG#R KHULGO	# 0001	668.8 0.2161	ALFS,C CP/S =	= 5.8 0.001662	5.8 662	CLR/S,R CDR/S,R	X =0.07404 X =0.00893	0.4 9.3	CMY/S, R CMX/S, R	= 0.1118 =-0.0033	70 M
				den	UPPER RCTUR	8LA JĒ	2 8 8 1		BENDING MCMENT				
		¥.		,	.2F				38.		•	• X2	
		ะบร	SIN		ccs	N I S		°03	NIO		(C)	NIS	
HARYCHIC					,			1					
0	-2468	÷8∙8			0.0		ī	-1111.8			654.3		
7		33.4	276.8	α,	0.0	0.0		278.5	-224.2		1034.9	<b>1</b> -	7
<b>C</b> I	~	65.4	-379.3	•	o•o	0.0		112.4	-126.8		-285.3	-200-4	4
3		•	145.	~1	၇• ၀	0.0		1.2	65.7		-340.9		5
<b>.</b>	M	•	-227.7	~	o•0	0.0		108.8	-56.6		-376.3		4
2	7-	•	289		J.O	0.0		-60.1	61.9		167.8	•	~
\$		•	-213.1	_	o • 3	0.0		16.9	-84.1		51.7		٣
7		41.5	75.8	*1	0.0	0.0		34.6	9.0		-63.1	7	7
80	1	•	-29.1		0.0	o•0		4.6	7.6		31.8		<b>.</b>
σ		34.1	0.3	~	0.0	0.0		8•0	-3.2		-51.5	23	9
10		-7.3	-66.	10	0.0	0.0		-14.3	7.4		-1.7	52	7
	UPPER		RUTUR EDGEW	ISE	UPPER KUTUR	OTOR		UPPER	ROIOR				
	BLN	BENDING MO	MUNENT	18	PITCH LIN	K LUAD		SHAFT	STRESS				
		ros	SIN		CCS	NIS		cos	SIN				
HAP 4CN IC													
0		0.0			175.8		,	3574.6					
-		0.0	ာ• 0		-71.7	511.9	ī	-1793.0	137.2				
2		0.0	3.0		-30.8	12.3	•	-510.6	-54.0				
3		0.0	0.0		-73.2	-2.7		48.7	-38.8				
4		0.0	0		-7.6	-35.8	Ţ	-102.0	81.9				
2		0.0	0		13.7	-61.7		-58.7	-237.8				
9		0.0	J•0		-2.0	39.2		3.3	29.3				
1		0.0	0.0		7.9	58.8	•	-117.3	6.66-				
8		o•0	0.0		-16.5	6.5		4.01	7.6				
0		0.0	0		4.6	17.0		-40.0	-42.3				
10		0.0	0	_	29.8	-3.2		-75.8	62.7				

= 0.1118 =-0.0033	ž	NIS	1	247.4	-22.8	-11.0	3.5	-49.8	9.0-	-2.1	0.0-	3.6																
CMY/S,R =	• 6K	500	7.80-	128.2	23.6	-36.4	40.0	-11.5	-21.2	1.4	-6.5	-1.4																
=0.07404 =0.00893	MUMENT	NIS	!	177.4	41.4-	2.3	3.6	6.811	9.61-	-2.4	7.5	-1.8																
CLR/3, R CDR/5, K	L BENDING MUMENT	cus	-1886.1	37.4	31.4	50.0	-103.3	55.6	35.7	13.5	-5.4	<b>6.4</b>																
5.8	BLADE NORMAL	NIS		-61.2 253 5	-77.5	-11.2	39.3	223.6	-68.0	16.3	-11.8	<b>7.6</b> -		TOR		SIN			0.811	0.6	1.1	9.0-	-2.5	0.5	-13.9	-0-3	0•1	-9.5
ALFS,C CP/S =	LOWER RCTOR	002	-2981.0	-84.2	39.6	106.9	-210.1	167.0						LOWER RUTOR	PITCH LINK	cus		-131.8	-101-2	28.5	-24.3					10.4		4.6-
UMEG*R = 608.8 RHU100 = 0.2161		NIS		-355.8	-118.5	41.0	-76.4	459.2	12.8	16.5	6.4-	-1.3		ROTUR EDGEWISE	MUMENT . 1K	z			-656.4	-228.4	-7.5	1.9	-39.3	-37.3	-424.0	16.8	-18.0	8 <b>•</b> 6
PUINT 18 90.1 CME 0.250 RHU	• 18	SOO	∞ .	-273.2	3.7.6	156.2	- 351.1	50.7	216.0	-51.3	47.1	78.9		LCWER ROTU	_	503		-4900.0	8 * 8 * 6	6.467-	0.61	-17.9	9.9	7.8.	352.0	-6.3	-31.5	0.1
PUN 21 VKTS = V/CR =		HAR WONTE	G	، ۳	<b>,</b> ~	•	5	9	1	æ	6	1.0	14.	5			HARMERIC	Ç	4	7	3	4	5	9	7	œ	6	10

į

/S,K = 0.1118 'S,K =-0.0033	UPPER KUTUR SHAFT STRESS		•666	60	1519.	2054.	63	2921.	3124.	3655.	4122.	4357.	4862.	5431.	5419.	4923.	.6144	4365.	4920.	5288.	<b>.</b> 606 <b>5</b>	4634.	4621.	4639.	2	2	2	53	05	2671.	1	9	2	4 9
).07404 CMYZ:	UR PITCH LINK LUAD		30.	89.	80.	144.	299.	<b>209</b>	615.	494	266.	280	370.	375.	359.	334.	297.	296.	261.	<b>508</b>	277.	185.	-25.	-123.	٦.	72.	43.	28.	-55.	-107.	35.	132.	-1-	-75.
CLR/S, R = 0 CDR/S, R = 0	UR EDGEMISE BENDING .IR	1	• •	•	• •	ં	• •	· •	<b>்</b>	o	• •	•0	•	ċ	•°	ċ	٠ <u>0</u>	ၨ	·°	•	•0	•	°	•0	• •	•	·°	ċ	°0	•	• 0	• •	•	•
,C = 5.8 = 0.001662	MUMENT UR		822.	848.	.101	•009	679.	510.	-35.	12	-1401-	-1663.	-1021-	-463.	-224.	-727.	-1418.	-1432.	-673.	77.	454.	713.	0	756.	1101.	84	2491.	07	3574.	3513.	2992.	46	1804.	08
AL FS CP/S	BENDING .3R	; ;		-789.	-985-	-1086.	-1142.	-1321.	-1521.	-1506.	-1346.	-1287.	-1393.	-1569.	-1609.	-1367.	-1347-	-978-	-1147.	-1365.	-	-1546.	-	-1177.	-1084.	-982.	-883-	-852.	-821.	-169.	-754.	-723.	-630-	-695-
*K = 608.8 00 = 0.2161	BLADE NURMAL		•0	•0	• o	• O	• °	•0	°	•	•	• 0	°°	•	•°	0	·°	•	°°	•0	•0	•0	<b>.</b>	•0	υ <b>.</b>	•0	•	•0	٠°	0.	• o	• •	•0	•0
PUINI 18 90.1 UMEG*R 0.250 RHOLOO	UPPER ROIGA BI		178	5	œ	$\sim$	-2852.	O	Ø	$\sim$	223	$\sim$	S	252	287	-2287.	9	•	3	•	•	-	Ñ	Ň	5	ĸ	$\sim$	ò	~	-2876.	ø	5	Ġ	Ñ
PUN 21 PUNTS = 9	วิ	S	00.0	1.2	2.5	3.7	5.0	6.2	7.5	8.7	0.0	01.2	12.5	23.7	35.0	•	157.5	68.7	80.0	91.2	32.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	95.5	03.7	15.0	26.5	37.5	48.7

KUN 21 VKTS = V/OR =	90.1 90.1 0.250	18 UMEG*R RHU100	2*R 100 =	608.8 0.2161	8 ALFS,C	s,C = 5.8 S = 0.001662	5.8 CLR/S,R 1662 CDR/S,R	.K =0.07404 .R =0.00893	CMY/S,R = 0.1118 CMX/S,R =-0.0033
	LOWER R	OT OR	BLADE	NORMAL	BENDING MOMENT	MOMENT -68	LR EDGEWISE BENDING 1R	E LR PITCH	H AD
S			,		;	<u>;</u>			1
000	- 55	97	3	.00	-2202.	-743.	-3128	-5	74.
88.7	09-	95	ന	53.	241	-729.	72	-308	08.
77.5	-50	40	36	68.	-2382.	-788.	-4411	-300	.00
.2	74-	18	30	59.	-2051.	-884.	-4347	-303	03.
55.0	-35	08	23	•	-1743.	-931.	-4095	-248	48.
43.7	- 38	58	22	•	-1770.	-852.	-4559	-141	47.
32.5	94-	9	28	•	-2005-	-101-	-5491	-158	58.
21.2	75-	53	31	33.	-2092-	-649-	-5910	-215	15.
10.0	14-	35	28	•	-1943.	-751.	-5606	7	37.
98.7	-34	12	23	11.	-1719.	-863.	-5389	•	-7.
87.5	-31	33	21		-1631.	-866.	-5961		42.
76.2	146	62	25	12.	-1786.	-785.	-6710,		•09•
65.0	-53	3	31	.93	-2052-	-683.	-6510.		52.
53.7	-55	78	33		-2154.	-593.	-5624	1	19.
42.5	-56	72	33	71.	-2045.	-525.	-5407	7	-45.
31.2	-56	29	33		-1916.	-476-	-6709-		•6
20.02	-53	82	32		-1853.	-434.	-6211		18.
08.7	-52	73	30		-1787.	-389.	-5530	ï	25.
7.5	-54	46	30	47.	-1712.	-335.	-4886		-38.
6.2	-55	0.5	31		-1673.	-293.	-5210		-54.
5.0	-53	48	30		-1662.	-277.	-5808-		-88.
3.7	~53	8	29		-1658.	-270-	-5589.		-72.
2.5	-53	4	29	•	-1661.	-268.	-4746.		-33•
1.2	-53	9	30	•	-1671.	-294.	-4384	ĭ	-64.
0.0	75-	46	~	, 3.	-1658.	-355.	-4834•	091-	•09•
8.7	15-	24	27	.69	-1611.	-431.	-5136	,	225.
7.5	95-	37	26	31.	-1622.	-485.	-4569.	,	05.
56.2	75-	66	27	.2.	-1791.	-481.	-3686.		85.
45.0	-56	23	31	.20	-2013.	-462.	-95196-	-25	57.
333.75	-53	.669	-334	•	207	-536.	-4053	£-	26.
22.5	14-	76	30	•	-1996-	ဆ	-	-5	77.
11.2	34-	45	7	17.	-5004-	-165.	-3486	-5	.62

01 nd					30	4	4	_	<b>8</b> 0	0		0	0	9																
= 0.1072 =-0.0025	89	SIN	•		-1390.8	-214.4	231.4	246.1	-756.8	131.0	-45.	-10.	57.0	13.																
CMY/S,R	•	<b>C</b> C C S	1	364.6	1506.9	-183.1	-96-1	-355.3	304.6	142.5	-8-4	121.4	108.1	73.0																
=0.06938 =0.00890	MUMENT	ZIZ	; •		412.7	-289.5	46.1	-34.9	2.19	-18.6	6.6-	-2.5	11.3	8.6		RUTOR	SIRESS	SIN			473.0	-101-1	-121.0	255.2	-267.7	35.7	-77.3	-102.3	Or .	95.4
CUR/S, R COR/S, R	L BENDING MUMENT	503	)	-1437.8	696.2	9.09	35.3	127.1	-110.8	40.4	20.0	39.5	0.2	0.5		UPPER				3568.2	-959.5	-394.1	-3.6	-189.6	0.44-	31.1	-250.9	156.6	34.7	-36.8
5.5	BLADE NURMAL	2	<u>.</u>	•		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0-0		RUTOR	LUAD				224.9	44.7	13.7	-26.6	-77.2	25.6	74.2	56.8	6.3	-20.5
ALFS,C CP/S =		47.	3	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		UPPER RU	PITCH LINK	COS		176.9									30.2	20.0
GMEG*R = 609.8 RHULGO = 0.2150		71.			1720.3	-		1		-234.5			-88	12		ROTUR EUGEWISE	Ž	SIN			0.0								0.0	
PCINI 19 108.5 0.300 P		101	2	-3364.5	829.0	230• (	127.6	4.504	1-675-	-129.9	43.6	-158.4	4.96-	-83.6		UPPER RE	-	503		0.0	30	).0	0	0.0	0	0.0	0	0	0.0	0.0
RUN 21 VKTS = V/CR =			CINCRAVI	C	·	. 2	1 (~	4	· <b>v</b>	· •		· cc	Φ.	01	14	48			HAR MON IC	0		2	· (C)	*	2	•	•	• •	6	10

= 0.1072 =-0.0025	239.5 239.5 12.3 12.3 -24.7 -20.2 -43.5 -6.0
CMY/S,R CMX/S,R	139.6 139.6 139.6 130.0 14.0 150.0 12.0 12.0 13.0 13.0 13.0 13.0 13.0 13.0 13.0 13
=0.06938 =0.00890	NUMENT S S IN 265.6 -6.0 -22.8 119.4 -27.6 -1.7 -2.4 23.8
CLR/S, R CDR/S, K	AL BENDING MUMENT  -2134.6  -2134.6  -37.1  265.6  37.6  -37.1  265.1  -17.8  119.4  -17.8  119.4  1.9  2.1  1.9  2.8
5.5 0.001245	SIN 51N 51N 51N -773.2 470.0 -31.9 -25.4 25.6 -25.6 -470.0 -25.6 -25.6 -20.6 -20.6 -20.6 -10.7 110.4 110.4 110.4 110.4 110.4 110.5
ALFS,C CP/S =	COS .2E SI -3302.9 -773 -28.6 470 45.9 -31 181.6 -25 -31 18.4 -62 -25 -25 -25 -25 -25 -25 -25 -25 -25 -2
OMEG*R = 609.8 RHJ100 = 0.2150	5 IN 411.3 743.1 743.1 139.1 100.4 81.4 81.4 100.6 170.6
PUINT 19 108.5 GME 0.300 RHL	CUS .IR
RUN 21 VKTS = V/OR =	HARMCNIC 10 10 10 10 10 10

A 45.00

RUN 21 VKTS = V/CR =	108.5 0.360	19 UMEG*R = RHJ100 =	609.8 0.2150	8 ALFS+C 0 CP/S =	,C = 5.5 = 0.001245	5.5 CLR/5, K 245 CDR/5, R	=0.06938 =0.00890	CMY/5,R = 0, CMX/5,R =-0,	0.1072
	UPPER	RUTOR BLADE	NGR MAL	BENDING MUMENT	MUMENT -6R	UR EDGEWISE BENDING .1K	UR PITCH	UPPER SHAFT	KOTUK STRESS
v		•			; }				) )
00.0	-2	359.		-619-	1978.	•	181	•	1912.
-	1	-1693.	•	26	32	•0	187	•	94
2.5	<b>1</b> -	~		-778.	692.	•	19	•	2403.
3.1	-2	088		-174.	910.	•0	153	•	3196.
5.0	-2	557.		-871.	930.	•	434	•	1561.
6.2	-2	357.	•	-1167.	288.	•	990		3297.
7.5	-2	292.	•	-1335.	-248	•	624	•	3518.
8.7	-2	063.	•	-1132.	-176.	•	376,	•	4267.
0.0	-	~		-843.	-1682.	•	747	•	4329.
01.2	ľ	239.	•	-845.	-2116.	•	314		4143.
12.5	•	.846.		-1120.	-1436.	0	360		1901.
23.7	-2	326.	•	-1425.	-490	•	351	•	5702.
35.0	-2	.1961.		-1587.	-384•	•	361		5240.
46.2	-2	.220.		-1588.	-1163.	•	324		4110.
57.5	-1	.517.	•	-1537.	-1956.	•	246	•	3463.
68.7	-2	048.	•	-1601-	-2063.	•0	717		3677.
80.0	-3	308.	•	-1891.	-1652.	•	661	•	4359.
91.2	4-1	592.	•	-2323.	-1084.	•	200		4563.
02.5	-5	.166.	•	-2637.	-414.	•	214		4153.
13.7	9-	.255.	•	-2684.	51.	•	139		<b>+058</b> •
25.0	-5	.815.	•	-2583.	89.	•0	8	•	4184.
36.2	-5	348.	•	-2447.	202	•	04-		3681.
47.5	-5	197.	•	-2224.	.899	•	-48	•	3115.
58.7	<b>5</b> -	.847.	•	-1941.	1199.	•0	61-	•	3285.
70.0	4-	556.	•	-1741.	œ	•0	115	•	3541.
81.2	-46	3	•	-1630.	2717.	•	101	•	3394.
92.5	4-1	59	•	-1514.	3115.	•	941-	•	
03.7	-3	4	•	-1316.	3001.	•0	-185	•	2983.
15.0	£-	-	•	-1060-	_	o	98	•	2673.
•2	-2	2357.		-820.	2129.	•0	112	•	2591.
37.5	7-	9		-674.	S	•	-115	•	3
48.7	-2	$\tilde{}$		-609-	1709.	•0	-65	•	2194.

RUN 21 VKTS = V/OR =	PUINT 108.5 0.300	19 UNE RHJ	UNEG*R = RHJ100 =	609.8 0.2150	ALFS,C CP/S =		5.5 1245	CL K/S, R CDR/S, R	=0.06938 =0.00890	CMY/5,R = 0.1072 CMX/5,R =-0.0025
	LOWER	ROTOR	BLADE N	NURMAL B	BENDING MOMENT	MOMENT	LR L	LR EDGEWISE	LR PITCH	c
ഗ		<b>.</b>	•		<u> </u>	<u>.</u>				
000	5-	-5305-	7	•	164.	-763.		-3339.	2	*
88.7	1	5215.	~	52	194.	-789.		-3456.	67-	Ď.
77.5	4-	.164	0	١	.003	-856.		-4119-	S	7.
66.2	1.3	1114.	N	•	-1611.	-956-		-4586.	-32	24.
•	7-	2458.	-1626		-1445.	-973.		-4455.	-189	•6
43.7	E-	1517.	C.		-1665.	-839.		-4556.	-176	• •
32.5	4-	1729.	_		942.	-104.		-5183•	-23	3.
21.2	4-		v		-2028.	-732.		-5694•	-186	• 9
10.0	1	3315.	v		-1929.	-877.		-5667.	- 85	5.
58.7	E.		-	i	1803.	-971.		-5483	11	7.
87.5	4-1		ų١	•	1921.	-945		-5700.	89	•6
76.2	2.	524.	2	•	306.	-865.		-6281.	<b>.7</b>	• 60
65.0	91		Ø	•	.909:	-777.		-6889-	Ę,	34.
53.7	9-		-	•	663.	-668		-5929•		8.
45.5	-		-4343		2653.	-571.		-5413.	20	•0
131.2	-	.900	-4363		643.	-519.		-5731.	-44	••
20.0	9			•	581.	-470.		-6226.	-32	2.
08.7	9-			•	480.	-414-		-5981.	6-	•6
5	9	.649			324.	-396.		-5425.	-87	7.
.2	9	6433.			.2176.	-381.		-5406.	-121	1.
C	9-			•	183.	-326.		-5775-	76-	2.
-	9		. •	•	243.	-306-		-2870-	-108	• 80
	-6			١	.167.	-345.		-5323.	16-	1.
7	10 I	5972.			.047.	-370.		-4776.	99-	• •
0	1		-3412	•	-1978.	-410.		-4774.	-174	•
	R. I			•	89	-512.		-5113-	-252	2.
5	<b>5</b>			•	893.	-562.		-4957.	-18	2.
56.2	i S	68 13 •	-3249	2	9	-511.		-4114-	-215	5.
45.0	9-		-3581	•	$\sim$	- 508 -		-3651.	-34	• 9
	1 1		-3472	•	2	-611.		-3876.	-331	1.
22.5	1 1	003.	-3184	•	1151.	- 406-		-4185	-56	4.
11.2	2			•	132.	-743.		-3877.	-296	• 9

t

CMY/S,R = 0.0246 CMX/S,R =-0.0006	899	COS SIN	-1123.7	1188.4 -1981.8		3.4 376.2							11.3 -16.4																
K =0.02499 K =0.00209	BENDING MUMENT	SIN		-628.4	-280.3	38.8	7.6	58.8	-38.8	7.3	-14.0	-2.2	11.3				ZI'S			-135.5	-217.7	-330.4	264.4	-29.3	16.3	6.1	-7.5	-01.3	84.4
CLK/5, K CDR/5, R		รกว	-2861.7	ידינ ו	-5.4	39.9	106.2	-31.5	-28.6	-2.2	-1 - 1	1-4-	-4.3		UPPER	SHAFT	<b>COS</b>		1927.5	-1944.7	-780.4	171.3	-244.4	0.68-	5.3	36.9	-64.6	10.7	0.3
ALFS,C = 0.2 CP/S = 0.002093	UPPER RUTCR BLADE NORMAL	CLS SIN		336.0 -679.4	5-	82.6 23.0			'				7-		UPPER RUTOR	PITCH LINK LOAD	SOS SIN		157.7		8.7 41.0					e	-5.9 10.1	1	-16
592•1 0•2281	UPPER	J	-2441	33	7	8	20	1-	-5	7		1-				IR PIT			-15	-3	7-	-2	•	-1			1		7
UMEG#R = 0	<b>2</b>	NIS		-521.7	-826.2	-34.8	-84.2	147.0	-31.8	-2.3	34.4	89.4	5.		EDGE	FNT	~			0.0	ဂ• ၀	0.0	o•0	0.0	0.0	0.0	O•0	0.0	o•0
PCINT 7 105.0 UME 0.299 RHU	3.	500	4.121.2	3	-29.8	164.9	316.9	-117.5	-102.9	62.6	38.2	16.0	4.3		UPPER RCTUR	LNG	000		0.0	0.0	0.0	ဂ•၀	o•0	0.0	0.0	0.0	0.0	0.0	0.0
PUN 23 VKTS = V/CR =			HARMONIC	- <b>-</b>	5	2	•	~	9	7	80	6	0.1	15	2			HARMONIC	c		7	e	4	2	9	7	<b>6</b> 0	6	10

Į

= 0.0246	. 6R	SIN		9.167	26.1	-29.5	3.3	-111-1	-35.9	1.9-	0-4-	-7.0	1.0																
CMY/S,R :		cos	-953.9	88.5	33.0	43.2	-42.5	18.0	13.2	T-6-	0.3	-10.0	6.9																
=0.02499 =0.00209	MCMENT	NIS		410.0	430.3	19.2	-58.7	2.5	115.2	15.2	-3.0	7.4	8.5																
CLR/S, R CDK/S, R	AL BENDING MOMENT .3R	cos	-4844.8	-105.5	101.7	107.7	101.0	-43.3	-26.5	25.5	1.0	13.9	9.4-																
0.002093	BLADE NORMAL	SIN		311.4	<b>5.969</b>	5.5	.117.1	38.6	229.7	3.9	-1.3	6.0	10.1		KUTOR	LOAD				115.3	6.1	25.9	-2.1	7.7	20.1	-8.4	_	•	<b>5.4</b>
ALFS,C CP/S =	LOWER ROTOR .2R	500	-7252.4	-309.5					-18.0	87.2	5.1	70.7	-28.1		LOWER KE		503		-239.9	-65.5	32.3	-1.1	3.3	-17.2	12.3	11.1	-2.2	8.9	8 • 8
3*R = 592.1 100 = 0.2281		SIN		165.4	1102.1	54.2	-86.6	17.9	308.3	76.8	10.1	86.2	-33.9		ROTOR EDGEWISE	CMENT . 1R	SIN			-614.9	-292.9	-36.0	24.7	-28.6	-42.0	60.0	7.8	<b>6.4</b>	-5-3
POINT 7 105.0 OMEG*R 0.299 RHU100	• 1R	500	-10792.9	-603.0	112.5	189.4	257.4	-180-1	-225.6	140.2	6.4	1.17.2	-45.2		LOWER ROTOS	-	500		4.6004-	-70.5	24.3		-52.5		-19.4	-96.5	-19.2	6.3	-10.2
RUN 23 VKTS = V/OR =		CINCHOVO	) C		2	6	<b>4</b>	ur.	9	~	80	0	01	1	<b>L5</b> :	3		HARMONIC	O		7	3	4	5	9	~	œ	6	10

金属を かられて

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CMY/S,R = 0.0246 CMX/S,R =-3.0006	UPPER ROTUR SHAFT STRESS		-485	-420.	-524.	2.	201.	359.	œ	1413.	7007	2902	3745.	3715.	3301.	3249.	3103.	7870	3149.	3775.	3944.	3876.	3714.	3205.	2663.	2290.	1805.	1480.	1590.	xõ.	7	811.	338.	2
=0.02699 CMY/ =0.00209 CMX/	UR PITCH LINK LUAD		-730	-217.	-148.	-33.	33.	87.	107.	• 0•	• 80	43.	12.	-46.	-43.	-19-	-101-	-63.	-115	-162.	-168.	-217.	-311.	-586-	-233.	-291.	-325.	-291.	-349.	0	7	Q.	-335.	-297.
CLR/S, R CDK/S, K	UR EDGEWISE BENDING .IR		•0	ဲ	•	•	•0	• •	°	•0	•	•	•	•0	• •	•0	•0	•	•	•	•0	ċ	°	•0	•0	•0	•	•	•0	•0	•	•	•0	•
S,C = 0.2 S = 0.002.93	MCMENT • 6R		~	46	249	-2995-	-3230.	-3900-	-4094-	-5415.	-5884.	-5683.	-5204.	-4847.	-4653•	-4703.	- 4464-	-4990 -	-4656 •	-4180.	-3730.	-3210.	-2613.	-2118.	-1778.	-1414.	-955.	-565-	-357.	-411•	-866.	-1501-	-1825.	
592.1 ALFS.C	IAL BENUING	1	-2433.	-2645.	-2876-	-3134.	-3399.	-3609.	-3645.	-3510.	-3366.	-3302.	-3311.	-3386	-3427.	-3318.	-3155.	5	-3157.	-3239.	G	-3157.	-5888-	-2841.	-2598.	~	-2070-	-1995	-1961-	-1993.	-2051.	-2056.	-2075.	-2219.
UMEG*R = 59 RHU100 = 0.2	BLADE NORMAL .2R		90	14	58	051	35	55	59	2	81	61	~	93	93	7	57	43	59	87	96	3	8	Ð	20	æ	58	44	43	-1500	46	~	147	7.1
PUINI 7 105.0 UM 0.299 RHG	UPPER ROTCR	)	5583	6011	0	725	0	-7660.	4	O	8	-5704.	-6094	52	19	-6005	5777	-5748.	-6207.	-6710.	-6860.	-6937.	-6941.	-6501.	-5883.	55	-5390.	ø	_	-5293.	6	84	01	
PUN 23 VKTS = V/OR =		S	00.0	1.2	2.5	3.7	5.0	6.2	7.5	8.7	0.0	01.2	12.5	23.7	35.0	46.2	57.5	168.7	90.0	91.2	02.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	92.5	03.	15.0	26.7	37.5	8.7

M/S,R =0.00209 CMX/S,R =-0.0006 WISE LR PITCH
0.2093 CDR/S,R LR EDGEWISE
ALFS: L = CP/S = 0.00; BENDING MUMENT
= 0.2281 DE NORMAL
105-0 UMEG#K 0-299 RHU100 LOWER ROTOR BLAE
VK 15

PUN 23 VKTS = V/CR =	PUINT 105.4 0.301	GAEG*K RHU100	6 * K 100 #	593.2 0.2263	ALFS, C CP/S =	0.00 0.003972	6 CLK/S,R 2 CDR/S,R	=0.08253 =0.00167	CAY/S+R =	= 0.053c =-0.0035
				đ.	UPPEK RUTCR	BLADE NORMAL		BENDING MOMENT		
		. IR			.2R			38		.6R
		cos	SIN		SOS	N I S	500	NIS	500	NI S
HAPMONIC					6		70.7			
	n cc 1-	٠ ر د د د د			7-160		0.026-	1	0.1011-	
	1	1.46-	• 47/1		1.40	806.3	193.5	350.5	4.756	6.8741-
2	9-	•	-758.5		-428.9	-514.6	-347.4	-310.0	-982.2	-357.1
~	7-	-203.6	187.5		-1.6.5	110.2	-87.6	9.001	120.0	•
4	1	-32.3	-236.5		35.0	-117.3	14.3	-56.3	-28.7	168.9
2	-39	8	234.0		-198.3	81.8	-59.6	41.3	239.7	-208.1
•	917-	6.91	-416.3		-53.8	-280.4	-54.6	-127.3	200.4	209.5
7	7	248.0	14.2		114.0	28.4	13.9	-34.2	-132.8	5.7
œ		9.10	168.2	2	-1.8	9.65	2.6	-26.5	-50.3	-106.3
6		6.7.5	109.3	3	14.3	39.6	12.7	-20.3	-15.0	-100.8
01		-1.2	-37.	8.	-7.5	9.8-	-11.6	5.3	6-94	0.0-
15										
6	UPPER	RU	RUTOR EUGEW	_	UPPER R	ROTOR	UPPER	ROTOR		
	BEN	OING M	CMENT	•1R	PITCH LIN	K LUAD	SHAFT	STRESS		
		cus	NIS		cos		503	NIS		
HARMONIC										
C		0.0			-142.4		4090.8			
~		0.0	0.0	0	23.7	203.3	-2245.6	1769.3		
2		0.0	· °	0	-23.8	54.8	-355.5	-478.2		
3		٠. د.	်	0	-11.7	50.2	451.9	61.2		
4		J. J	o	0	-32.8	7.5	-58.3	311.1		
ĸ		0.0	0.0	0	22.5	8.84-	25.6	-423.1		
ç		0.0	•	0	33.6	9.61	-72.5	5.8		
7		0.0	•	0	39.2	1.4-	-113.1	-247.9		
œ		0.0	•	0	20.3	8.7	61.3	-116.4		
6		0.0	o	0	-38.3	•	•			
10		o••	•	0.	-6.0	32.4	-7.3	1.6-		

= 0.0536	350.0 40.6 58.8 -1.8 31.0 -47.5 -9.8 -9.8	
CMX/S,R = CMX/S,R =-	. COS -371.2 139.8 -240.8 -27.3 -27.3 -25.3 -25.3	
=0.08253	NUMENT 8 SIN 174-1 155-1 -119-6 -13-2 -43-6 12-3 12-3 29-3 -4-6 5-5	
CLR/S,R CDR/S,R	BENJING .3R COS -668.4 93.8 -512.9 7.6 55.2 -136.0 55.1 44.7 -20.7 -20.7	
0.003972	8LAUE NORMAL 51N -168.0 297.6 -230.4 -39.0 -57.9 252.1 -5.8 4.5 89.0 39.9	ACTOR NK LOAD SIN SIN 61.2 25.0 -17.0 6.2 1.4 4.2 1.7 18.1 2.3 6.9
ALFS,C CP/S =	LDWER RUTOR	LOWER RU PITCH LINK CCS -146.6 -159.0 32.6 -3.0 -1.9 -1.9 -3.2 33.5 8.9 2.9 -0.8
UMEG*R = 593.2 RHUIGO = 0.2263	SIN -614.7 338.6 -411.2 1.8 -325.5 -444.1 127.0 -86.1 73.4	ROTUR EUGEWISE ING MUMENT - IR US SIN 4.5 -99.5 7.5 -99.5 9.9 -658.1 1.06.4 5.3 -11.4 9.6 -73.5 9.6 -73.5 8.3 800.8 8.3 800.8
ຜ ີ	.1R -2439.2 -190.9 -793.6 -63.7 110.6 -471.1 -100.8 253.7 -27.7	CGWEK ROT BENDING LUS -3924.5 1427.5 399.9 113.9 113.9 -45.3 70.8 628.3 -15.8 -15.1
3 POINT 105.8		
RUN 23 VKTS = V/OR =	HARMONIC 0 1 2 2 3 4 4 7 7 10	TS7

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The second second

t

CMY/S,R = 0.053 CMX/S,R =-0.003	UPPEK RUTOK SHAFT STRESS	^	•	2253	3250	3468	336	395	• 508	• 605	2. 6732.	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	. 2654	206	144	. 97	•	175
=0.08253 =0.00167	UR PITCH Link Luad	-116	34-	39-	81	161	261	136	-1:	[1 -	-32	<b>1</b>	12	36	24	-159	-294	-186	-134	-259	-267	-234	-346	-347	-193	-241	-395	-310	-227	-349	0	-314
6 CLR/S,R 2 CDR/S,R	UR EDGEWISE BENDING . 1K	0	0		•	• •	• •	•	ż	•0	•0	•	•	•	•	•0	•	•0	• 0	•	•0	• •	• •	•	•	•	•0	•	o	•	•	•
S.C = 0.66 S = 0.003972	MUMENT .6R	-7111-	212	4	-1817.	7	-1836.	2	136	228	233	91	-1329.	-1773.	-2712-	-3607.	-3718.	$\sim$	-2590.	5	5		Ð	~	0	1389.	1699.	1815.	47	.099	-117.	-364.
.2 ALFS,C 63 CP/S =	BENDING .3R	5	-962	96	-300•	-156.	-247.	-241.	-15.	209.	4	94.	-159.	-321.	-266.	-243.	-536-	-966-	-1341-	-1500.	-1465.	-1275.	-1093.	-934.	~	-401-	-272.	-240-	-274.	-401-	Ø	-475.
UMEG*R = 593.2 RHU100 = 0.2263	BLADE NURMAL	3		_	S.	2	š	22	3	7	2581.	7	2	22	46	74	41	513.	O	٥	S	45	0	3	3	4	0	Ò	-	0	876.	9
8 8 10	ER ROTOR	~	2536	-2163.	111		-114.	4	-414-	4	so ·	~	-133.	3	<b>.</b> 02	471.	56	8	-3275.	N	-3683.	_	•	~	5	9	-2210.	-2450.	~	-1696.	Š	-2213.
23 PULL S = 105. R = 0.30		70	~	S	۲.	0	~	ŝ		0	.25	Š	٠.	0	~	Š	7	0	~	Š	~	0	$\sim$	Š	۲.	Ö	?	Ň	-	ó	2	Ň

RUN 23 VKTS = V/OR =	PUINT 105.8 0.301	8 CME RHU	CMEG*R = RHU100 =	593.2 0.2263	2 ALFS,C 3 CP/S =	# 0	0.6	CLR/S, R CDR/S, R	=0.08253 =0.00167	CMY/S,R = 0.0536 CMX/S,R =-0.0035
	LOWER F	ROTOR 18	BLADE N	NORMAL	BENDING MGMENT	MCMENT .6R	LR E	LR EDGEWISE BENDING - 1R	LR PITCH	TCH LOAD
U	•	•	;	•		:				
0000	-20	0	-101	2.	-793.	-547.		-3007.	-2	84.
88.7	-28	~	-141	2.	-842.	-374.		-4432.	-2	87.
77.5	-22		-136	•	-594.	-382.		-3949.	£.	.307.
7	1	-172	140		-235.	-560		-3169.	-2	.278.
55.0	,7	-	30	.2.	-104-	-604		-4252.	1-	-194.
43.7	-13	Δ	-22	•	-311.	-486.		-6140•	1	-109.
32.5	-25	527.	-117	•	-724.	-458.		-6302.	•	55.
21.2	-20	•	-144	•	-1023.	-009-		-4845.	ĺ	41.
10.0	- 14	+82.	-115	4.	-967.	-800		-4288.	ľ	25.
98.7	-14	S	-93	• 9	-807.	-943.		-5582.		41.
87.5	-24	~	-111	5.	-951.	-952.		-6594.		.96
76.2	-23	.676	191-		-1272.	-822.		-5467.		61.
65.0	-35	1	-214	•	-1399.	-619-		-3618.		1.
53.7	74-	*	-238	•	-1316.	-406-		-3543.	•	13.
42.5	-3	<b>3</b>	-224	3.	-1123.	-237.		-4905-	•	-23.
31.2	75-	0	-179	.9	-785.	-127.		-5221.	•	-40•
20.02	-25	582.	-128	.61	-372.	-25.		-3925.	1	-32.
18.7	-21	$\sim$	-86	.6	-59.	.99		-3230.	1	37.
7.5	-18	2	-60	.2	93.	114.		-4369.	•	-94•
5.2	-21	-4	19-	3.	122.	166.		-5631.	1	-150.
5.0	-2	5	- 75	3.	87.	198		-5063.	1-	-156.
3.7	-20	•	-71	•0	-3•	125.		-3408	1-	-130.
2.5	77-	.667	-78	5.	-237.	33.		-3035.	1-	138.
1.2	-35	30	-132	7.	-564.	3.		-3950.	7-	18.
0.0	- 34	m	-175	•	-758.	-93.		-4004-	-2	289.
3.7	75-	:17.	-108	5.	-829.	-262.		-2546.	-2	56.
7.5	-36	33	-117	3.	-997.	-337.		-1201-	-2	08.
56.7	04-	33	-214		-1193.	-381.		-1417.	7-2	.09
45.0		77	-233	2	-1162.	~		-2631.	£-	332.
33.7		~	-144	•	-920-	-675.		-2748.	Ę-	.31.
22.		395.	-1340	•	-694.	-698-		-1649.	-3	.80
1.2	-11	70	16-	••	-658-	-665.		-1404.	-3	00.

= 0.1579 =-0.0040	<b>୦</b> ୯	NIS		ī	'			'			-45.6																		
CMY/S, R CMX/S, R	•	cos	-64.5	1114.1	-1863.2	-171.0	-111.5	190.4	200.3	-173.0	72.1	-47.2	75.9																
=0.11436 =0.01082	MOMENT	NIS		418.0	-513.2	61.3	-120.3	22.3	-192.6	-62.2	-11.4	-12.5	6.6	; ;	אטרטא	STRESS	NI S			1467.4	-612.3	96.1	641.2	-418.0	6.9	-346.0	-89.0	-35.1	39.9
CLK/S, R CUR/S, R	IL BENDING MCMENT	SOO	978.5	359.0	-668.5	-62.0	51.0	-36.0	-35.0	26.5	12.6	<b>6.4</b>	23.4			SHAFT			4814.6	-2011.0	-480.7	172.2	36.9	-57.0	16.4	-133.7	82.1	14.6	-48.1
5.8	S BLADE NURMAL	NIS		0.8101	-830.3	87.5	-254.6	93.7	-413.8	17.9	9•0-	-41.5	19.5	; ()		K LOAD				282.9	14.6	3	0.1	-60.4	7.5	-5.9	2	-25.7	2
ALFS,C CP/S =	UPPER KUTUR .2R	cos	2997.9	241.6	-861.0	-99.5	147.2	-146.5	32.6	154.0	-71.8	85.9	-39.7		UPPER ROTOR	PITCH LINK	COS		_	-79.5	99.5	-120.5	57.4	-95.3	3.0	13.3	$\sim$	-10.2	4
*R = 597.3 UO = 0.2251		SIN		2018.8		185.7	å	269.3	-652.8	91.1	64.1	9	58.7	•	EDGE	7	NIS			0.0	0.0	0.0	o•0	0.0	0.0	0.0	0.0	0.0	0.0
PUINT 9 105.6 UMCG*R 0.299 RHUIUO	•1.	500	1618.4		1		9.	•	-113.3	0	-166.1	•	•		UPPER ROTOR	BENDING AC	503		•		•	•	•				•	0.0	•
KUN 23 P VKTS = 1 V/CR = 0			HARMONIC O	·	7	~	4	5	9	7	rr.	σ	CI	16				HARMONIC	ဂ		7	3	4	~	9	1	œ	6	10

= 0.1579	740	NIS			1.716			•				13.8																		
CMY/5, R CMX/5, R		C05		-135.4	1989	-351.6	48.9	-25.8	8 *62	6.4-	N	13.1	22.4	5.3																
=0.11436 =0.01082	MOMENT	NIS		Ġ	٠ • • •	287.8	-17.9	175.1	43.0	6.917	5.9	26.4	-13.9	•																
CLR/5, R CUR/5, R	BENDING MOMENT	SOS		1152.6	230.5	6.486-	-29.5	47.7	-66.2	34.4	81.7	1.1	-7.2	-1.3																
5.8 0.004235	BLADE NORMAL	SIN		6	V.0V4-	1.064	-164.7	359.4	•	399.7	-24.8	-23.2	28.1	\$		TOR	X 1140				134.0	41.9	-46.0	-14.2	-3.7	29.0	6.5	29.4	18.0	-20.1
ALFS,C CP/S =	LOWER ROTOR	500		1432.3		-1209.6		129.2	-124.9	183.1	228.9	-92.9	-61.1	16.6		AUTUR WINTOR	PITCH INK	COS		-85.0	-192.8	-38.4	-20.7	-2.6	30.7	4.71	9.1	- 10.8	-22.5	12.4
) OMEG*R = 597.3 RHUIOO = 0.2251		NIS		(	-1138.5	453.5	-339.5	•	•	•		-217.5	•	116.3		REITH FORESTA	MOMENT ATR	_				3	72.		8.	-140.4	•	-45.9	-32.1	4
PCINT 9 105.6 OME 0.299 RHU	91	\$000		1359.6	26.6	•	-118.8	-51.8	-234.4			-118.5	•	•		TISE STATE	-	COS		-4836.6	2771.2	1131.0	204.5	-13.8	35.5	-136.7	1361.6	7-69-5	1.3	-27.3
PUN 23 VKTS =			HAP YONIC	<b>6</b>	~	2	~	*	<b>'</b>	~	~	<b>3</b>	6	01	1	61			HARMONIC	0	_	2	<b>6</b> 0	•	\$	\$	•	œ,	6	61

JA 4

HILLION = 0.2251 CP/S = 0.004235 CDK/S,K = 0.01082 CMX/S,R in the color of the colo	RUN 23	PUINT 105.6	σ.	ال ال	μ	597.3		H	5.8	CLR/5, R	п	CAY,	•••	61510
OPPER NOTOR BLADE NURHAL BENDING HOMENT         UNR EDGEMISE         UR PITCH         UPPER NOTOR           11         -2R         -3R         -6R         BENDING -1R         LINK LUAD         SHAFT           25         -187         -6R         -778         0         -209         -218           25         -187         -187         0         -218         -218         -218           25         -187         -187         0         -218         -218         -218           25         -187         -187         0         -218         -221         -218         0         -218         -218         -218         -218         -221         -218         0         -218         -		3.299		0010	0	•22		0	04235	CDR/S, R		CMX	**	0.0040
11. 2440. 656778. 0. 25 -189. 1859. 255807. 25 156. 1915. 255807. 26 1551. 2714. 9581198. 0. 27 2155. 356. 13301467. 0. 28 346. 13301467. 0. 28 346. 13301467. 0. 29 346. 13301467. 0. 25 348. 5216. 1355. 3. 25 548. 5216. 1267281. 0. 27 3461. 332. 1267411. 0. 28 420. 1321. 1500. 179. 0. 29 440. 4221. 1500. 179. 0. 29 440. 4221. 1500. 179. 0. 29 440. 4221. 1500. 179. 0. 20 1184. 1839. 249. 67. 0. 2418. 286. 1294. 67. 0. 25 -188. 2156. 590. 1294. 0. 26 1184. 2982. 1293. 3248. 0. 27 1184. 2982. 1293. 3248. 0. 28 1184. 3378. 1477. 3921. 0. 29 1129. 293. 1193. 0.		144	KOTOR . 1R	8	2	JRMAL	BENDING .3R	MUMENT .6R	Z	3	P.	CH UAD		ROTOR STRESS
171.         2440.         656.         -778.         0.           25.         189.         1859.         255.         -807.         0.           25.         189.         1859.         255.         -807.         0.           25.         1856.         1830.         -1467.         0.           27.         275.         3566.         1830.         0.           27.         275.         3913.         1822.         -788.         0.           27.         3467.         4260.         1823.         161.         0.         0.           25.         3465.         4260.         1823.         161.         0.         0.         0.           25.         3413.         1505.         179.         0.														
25         -189         1859         255         -807         0           50         1915         387         -1198         0           151         2715         1356         1198         0           27         1551         275         3566         1330         -1571         0           25         3456         1330         -1571         0         0         0           25         3456         1330         -1572         0         0         0         0           50         3456         1330         -1502         -798         0	C		11	7	4	_	.059	-778.		•	7	209.		2406.
50         356.         1915.         387.         -1198.         0.           75         11551.         2714.         958.         -1551.         0.           2755.         3367.         1330.         -1467.         0.           25         3456.         3467.         1382.         -798.         0.           55         346.         3460.         1823.         161.         0.           56         4260.         1823.         -161.         0.           57         4260.         1823.         -161.         0.           57         5436.         2258.         -546.         0.           57         3594.         4221.         1500.         179.         0.           57         3461.         3461.         0.         0.           50         2317.         3544.         1241.         -2247.         0.           50         4412.         1241.         -2247.         0.           51         2457.         3464.         -2247.         0.           52         4412.         1241.         -2247.         0.           50         1813.         720.         -436.         -22	~	•	68	-	8	_	255.	-807.		ċ	ï	218.		2323.
1551.         2714.         958.         -1551.         0.           2755.         3566.         1330.         -1467.         0.           255.         3467.         1382.         -1467.         0.           366.         3437.         1505.         -3.         0.           75         3467.         1623.         161.         0.           76         4400.         2151.         -281.         0.           77         5448.         5278.         -281.         0.           57         5448.         5278.         -281.         0.           57         5468.         1973.         -281.         0.           57         486.         1271.         0.         0.           57         446.         1500.         179.         0.           57         446.         166.         -3491.         0.           50         1970.         68.         -2647.         0.           50         1970.         68.         -2647.         0.           50         1970.         68.         -2647.         0.           50         1184.         247.         429.         -1066.     <	5		56	-	9	_	387.	-1198.		•	•	-25.		3085.
2755         3566         1330         -1467         0           25         3467         1330         -1467         0           25         3456         1365         -798         0           25         3456         1505         -798         0           25         4260         1823         161         0           25         4260         1823         161         0           25         5435         2258         -546         0           25         5448         5276         1973         -741         0           25         5448         5276         173         0         0           25         448         4221         150         0         0           25         4362         166         -2247         0         0           26         4362         172         165         -3491         0         0           26         4362         1970         68         -2247         0         0           27         436         -429         -1064         0         0           28         -118         198         -4247         0         0 <td>-</td> <td></td> <td>2</td> <td>~</td> <td>-</td> <td></td> <td>958.</td> <td>-1551.</td> <td></td> <td>•</td> <td>_</td> <td>167.</td> <td></td> <td>4081.</td>	-		2	~	-		958.	-1551.		•	_	167.		4081.
25         3476.         3367.         1382.         -798.         0.           350.         3913.         1505.         3.         0.           350.         4260.         1853.         161.         0.           357.         4940.         2151.         -281.         0.           25         548.         5276.         1973.         -231.         0.           360.         2276.         1973.         -231.         0.           50         248.         5276.         1973.         -231.         0.           50         248.         1241.         -2247.         0.         0.           50         241.         1657.         -411.         0.         0.           50         247.         1657.         -411.         0.         0.         0.           50         183.         172.         -1841.         0. <td>က</td> <td>•</td> <td>55</td> <td>m</td> <td>56</td> <td>_</td> <td>3</td> <td>-1467.</td> <td></td> <td>•</td> <td></td> <td>167.</td> <td></td> <td>4314.</td>	က	•	55	m	56	_	3	-1467.		•		167.		4314.
56         3362.         3913.         1505.         3.         0.           75         3845.         4260.         1823.         161.         0.           70         4677.         4901.         2151.         -281.         0.           25         5435.         2258.         -546.         0.           50         345.         4221.         1500.         179.         0.           75         2317.         3332.         1267.         -411.         0.           50         3461.         3654.         1241.         -2247.         0.           50         4362.         4172.         616.         -3451.         0.           50         4364.         1241.         -2247.         0.           50         1970.         68.         -2604.         0.           50         1970.         -436.         -2247.         0.           50         198.         -436.         -2604.         0.           50         1184.         1839.         -436.         -1797.         0.           50         -1813.         179.         -588.         0.           50         -184.         294. <td>~</td> <td>•</td> <td>16</td> <td><b>(4)</b></td> <td>36</td> <td>_</td> <td>3</td> <td>- 198</td> <td></td> <td>0</td> <td></td> <td>174.</td> <td></td> <td>3922.</td>	~	•	16	<b>(4)</b>	36	_	3	- 198		0		174.		3922.
75         3845.         4260.         1823.         161.         0.           70         4577.         4901.         2151.         -281.         0.           25         5745.         2258.         -281.         0.           75         3559.         4221.         1500.         179.         0.           75         3559.         4221.         1500.         179.         0.           75         2317.         332.         1267.         -411.         0.           75         2452.         1241.         -2247.         0.           75         2657.         3412.         68.         -2604.         0.           75         2657.         3412.         68.         -2604.         0.           75         2657.         3412.         68.         -2604.         0.           75         -1813.         720.         -436.         -2247.         0.           75         -1847.         689.         -2647.         0.           75         -1847.         439.         -769.         -788.         0.           75         -1847.         249.         -788.         0.           75 <td>•</td> <td>ŕ</td> <td>79</td> <td>•</td> <td>16</td> <td>_</td> <td>1505.</td> <td></td> <td></td> <td>•</td> <td>•</td> <td>9</td> <td></td> <td>4208.</td>	•	ŕ	79	•	16	_	1505.			•	•	9		4208.
00         4677.         4901.         2151.         -281.         0.           25         5435.         2258.         -546.         0.           50         5448.         5276.         1973.         -231.         0.           50         3459.         4221.         1500.         179.         0.           50         2317.         3332.         1267.         -411.         0.           50         4362.         1241.         -2247.         0.           50         4172.         1052.         -3691.         0.           50         4172.         1052.         -3691.         0.           50         1970.         68.         -2604.         0.           50         1970.         68.         -2604.         0.           50         1970.         -632.         -1797.         0.           50         1183.         720.         -632.         -1797.         0.           50         1184.         249.         67.         0.           50         1184.         249.         67.         0.           50         1184.         249.         67.         4439.         0.	~	·	45	4	97	_	1823.	161.		•		<b>5</b> •		5516.
25       5795.       5435.       2258.       -546.       0.         57       3548.       5276.       1973.       -231.       0.         75       3559.       4221.       1500.       1179.       0.         200       2317.       3322.       1267.       -411.       0.         55       4362.       4172.       1052.       -3451.       0.         75       2657.       3412.       616.       -3451.       0.         75       4362.       4172.       616.       -3451.       0.         75       -1216.       1084.       -2247.       0.       0.         75       -1813.       720.       -436.       -2247.       0.         50       -1813.       720.       -429.       -1066.       0.         75       -1847.       689.       -729.       -1066.       0.         75       -184.       2156.       590.       1294.       0.         75       1144.       2247.       941.       2449.       0.         75       1184.       3307.       1596.       4439.       0.         75       1124.       2348.       1647. </td <td>C</td> <td>•</td> <td>11</td> <td>4</td> <td>3</td> <td>_</td> <td>2151.</td> <td>-281.</td> <td></td> <td></td> <td>•</td> <td>-21.</td> <td></td> <td>6710.</td>	C	•	11	4	3	_	2151.	-281.			•	-21.		6710.
50       5448.       5276.       1973.       -231.       0.         75       359.       4221.       1500.       179.       0.         55       4362.       4124.       -2247.       0.         50       4172.       1241.       -2247.       0.         50       4362.       4172.       616.       -3451.       0.         50       1970.       68.       -2604.       0.         25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         50       -1813.       720.       -632.       -1797.       0.         50       -1813.       720.       -632.       -1797.       0.         50       -1817.       429.       -67.       0.         50       -189.       249.       -74.       0.         50       414.       2477.       941.       2419.       0.         50       414.       2477.       941.       2419.       0.         50       1184.       248.       1654.       4439.       0.         50       1281.	~		95	ur)	4	_	2258.	-546.		ċ		146.		7407.
75       3559.       4221.       1500.       179.       0.         2317.       332.       1267.       -411.       0.         25       4361.       3654.       1241.       -2247.       0.         50       4172.       1052.       -3691.       0.         75       2657.       3412.       616.       -3451.       0.         80.       1970.       68.       -2604.       0.         25       -1216.       1084.       -424.       -2247.       0.         25       -1813.       720.       -429.       -1747.       0.         50       -1847.       689.       -429.       -1747.       0.         25       -1847.       1839.       249.       67.       0.         26       -118.       1839.       249.       67.       0.         50       -18.       292.       1294.       0.         50       1144.       2547.       941.       2419.       0.         50       1281.       3348.       1654.       4439.       0.         50       1271.       3248.       16439.       0.         50       1229.	3	- •	3	ħ.	~	_	1973.	-231.				16		8275.
00       2317.       332.       1267.       -411.       0.         55       3461.       3654.       1241.       -2247.       0.         50       2657.       3412.       616.       -3451.       0.         75       2657.       3412.       616.       -3451.       0.         75       1216.       1970.       68.       -2604.       0.         25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1487.       689.       -7429.       -1797.       0.         75       -118.       1839.       249.       67.       0.         75       -118.       1839.       249.       67.       0.         75       -118.       2156.       590.       1294.       0.         75       -144.       2477.       941.       2419.       0.         80       1144.       2547.       941.       2419.       0.         81       1281.       1294.       4439.       0.         80       1276.       2982.       12439.       0.     <	-	•	5.5	7	$\sim$	_	1500.	179.		•	•	39		9016.
3401.       3654.       1241.       -2247.       0.         5C       4362.       4172.       1052.       -3691.       0.         75       2657.       3412.       616.       -3451.       0.         75       2657.       3412.       616.       -3451.       0.         80.       1970.       68.       -2604.       0.         25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1847.       1839.       -429.       -1066.       0.         25       -118.       -1839.       249.       67.       0.         25       -118.       2156.       590.       1294.       0.         26       414.       2942.       1294.       0.         27       1184.       2942.       0.         29       1293.       3248.       0.         29       127.       3921.       0.         29       127.       3921.       0.         29       1229.       2942.       0.         29       2933.       1447.	0	,	17	m	~	_	1267.	-411.						8648.
5C       4362.       4172.       1052.       -3451.       0.         75       2657.       3412.       616.       -3451.       0.         80.       1970.       68.       -2604.       0.         25       -1813.       720.       -632.       -1797.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1817.       689.       -429.       -1066.       0.         70       -950.       1198.       -749.       -588.       0.         25       -118.       1839.       249.       67.       0.         25       -118.       2156.       590.       1294.       0.         75       414.       2477.       941.       2449.       0.         80       1144.       2982.       1294.       4488.       0.         25       1281.       3348.       1654.       4439.       0.         25       1281.       323.       1447.       3921.       0.         25       1221.       3021.       1243.       2942.       0.         25       1229.       2933.       1193.       1609.	$\sim$	•	70	.,	Ð	_	1241.	~		•				7298.
75       2657.       3412.       616.       -3451.       0.         80.       1970.       68.       -2604.       0.         25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1867.       689.       -429.       -1066.       0.         75       -186.       -429.       -1066.       0.         25       -118.       1839.       249.       67.       0.         50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         75       414.       2982.       1293.       3248.       0.         80       1184.       3348.       1654.       4439.       0.         80       1275.       3233.       1447.       3921.       0.         80       1229.       2933.       1193.       1609.       0.         80       1295.       1064.       -764.       0.	S		79	4	~	_	1052.	-3691.		•		Φ		6035.
00       80.       1970.       68.       -2604.       0.         25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1687.       689.       -429.       -1066.       0.         90       -950.       1198.       -79.       -588.       0.         25       -118.       2156.       590.       1294.       0.         50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         75       414.       2477.       941.       2419.       0.         80       1144.       2982.       1293.       3248.       0.         80       1184.       3348.       1654.       4439.       0.         80       1275.       3233.       1447.       3921.       0.         80       1229.       2933.       1193.       1609.       0.         80       1395.       1064.       -764.       0.	~	•	57	(T)	4	_	616.	-3451.		• •		227.		5756.
25       -1216.       1084.       -436.       -2247.       0.         50       -1813.       720.       -632.       -1797.       0.         75       -1687.       689.       -429.       -1066.       0.         00       -184.       1839.       249.       67.       0.         25       -118.       2156.       590.       1294.       0.         50       414.       2477.       941.       2419.       0.         75       414.       2982.       1293.       3248.       0.         25       1184.       2982.       1293.       3248.       0.         25       1281.       3307.       1654.       4439.       0.         75       1275.       3233.       1447.       3921.       0.         26       1221.       3021.       1243.       2942.       0.         27       1275.       2933.       1193.       1609.       0.         25       1295.       2942.       0.       0.         25       1229.       2933.       1198.       88.       0.         25       1295.       1904.       -764.       0.	0		80	7	D.		ø	2604			•	375.		6436.
50       -1813.       720.       -632.       -1797.       0.         -1687.       689.       -429.       -1066.       0.         -1687.       689.       -79.       -588.       0.         25       -118.       1839.       249.       0.         25       -18.       2156.       590.       1294.       0.         50       414.       2477.       941.       2419.       0.         75       414.       2982.       1293.       3248.       0.         25       1281.       3307.       1596.       4088.       0.         75       1275.       3233.       1447.       3921.       0.         75       1275.       3233.       1447.       3921.       0.         26       1229.       2933.       1193.       1609.       0.         27       1019.       2982.       1064.       -764.       0.	2	ľ	91		0	_	•	-2247.		o		250.		6866.
75       -1687.       689.       -429.       -1066.       0.         90       -950.       1198.       -79.       -588.       0.         25       -118.       1839.       249.       67.       0.         50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         80       1144.       2982.       1293.       3248.       0.         80       1184.       3348.       1654.       4439.       0.         80       1275.       3233.       1447.       3921.       0.         80       1221.       3021.       1243.       2942.       0.         80       1229.       2933.       1193.       1609.       0.         80       1395.       2982.       1064.       -764.       0.	5	1	2		72	_	-632.	17			•	-35.		6115.
00       -950.       1198.       -79.       -588.       0.         25       -118.       1839.       249.       67.       0.         50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         75       1144.       2982.       1293.       3248.       0.         25       1281.       3307.       1596.       4439.       0.         50       1184.       3348.       1654.       4439.       0.         75       1275.       3233.       1447.       3921.       0.         26       1221.       3021.       1243.       2942.       0.         27       1229.       2933.       1193.       1609.       0.         29       1395.       3056.       1198.       88.       0.         75       1019.       2962.       1064.       -764.       0.	-	ľ	87		æ	_	-429.	1066		•	1	318.		4926.
25       -118.       1839.       249.       67.       0.         50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         00       1144.       2982.       1293.       3248.       0.         25       1281.       3307.       1596.       4439.       0.         50       1184.       3348.       1654.       4439.       0.         75       1275.       3233.       1447.       3921.       0.         26       1221.       3021.       1243.       2942.       0.         27       1229.       2933.       1193.       1609.       0.         28       1395.       3056.       1198.       88.       0.         75       1019.       2982.       1064.       -764.       0.	0	-	20		_	_	-44.	-588			ï	535.		4247.
50       -18.       2156.       590.       1294.       0.         75       414.       2477.       941.       2419.       0.         00       1144.       2942.       1293.       3248.       0.         25       1281.       3307.       1596.       4088.       0.         50       1184.       3348.       1654.       4439.       0.         75       1275.       3233.       1447.       3921.       0.         20       1221.       3021.       1243.       2942.       0.         25       1229.       2933.       1193.       1609.       0.         50       1395.       3056.       1198.       88.       0.         75       1019.       -764.       0.       0.	2	·	2	7	20	_	249.			•	7	543.		3889.
414.       2477.       941.       2419.       0.         00       1144.       2982.       1293.       3248.       0.         25       1281.       3307.       1596.       4088.       0.         50       1184.       3348.       1654.       4439.       0.         75       1275.       3233.       1447.       3921.       0.         00       1221.       3021.       1243.       2942.       0.         25       1229.       2933.       1193.       1609.       0.         50       1395.       3056.       1198.       88.       0.         75       1019.       2982.       1064.       -764.       0.	S		18	7	_		.065	594			š	<b>.</b> 004		3697.
00     1144.     2982.     1293.     3248.     0.       25     1281.     3307.     1596.     4088.     0.       50     1184.     3348.     1654.     4439.     0.       75     1275.     3233.     1447.     3921.     0.       00     1221.     3021.     1243.     2942.     0.       25     1229.     2933.     1193.     1609.     0.       50     1395.     3056.     1198.     88.     0.       75     1019.     2982.     1064.     -764.     0.	7		7	7	4	_	941.	•		•0	ť	341.		3893.
25       1281.       3307.       1596.       4088.       0.       -400         50       1184.       3348.       1654.       4439.       0.       -480         75       1275.       3233.       1447.       3921.       0.       -456         00       1221.       3021.       1243.       2942.       0.       -307         25       1229.       2933.       1193.       1609.       0.       -256         50       1395.       3056.       1198.       88.       0.       -271         75       1019.       2982.       1064.       -764.       0.       -211	0		43	~	Q,	_	293	$\sim$		·0	1	359.		4182.
50     1184.     3348.     1654.     4439.     0.     -480       75     1275.     3233.     1447.     3921.     0.     -456       00     1221.     3021.     1243.     2942.     0.     -307       25     1229.     2933.     1193.     1609.     0.     -256       50     1395.     3056.     1198.     88.     0.     -271       75     1019.     2982.     1064.     -764.     0.     -211	2		3	L.J	~	_	596	4088			ì	400.		4224.
75     1275.     3233.     1447.     3921.     0.     -456       00     1221.     3021.     1243.     2942.     0.     -307       25     1229.     2933.     1193.     1609.     0.     -256       50     1395.     3056.     1198.     88.     0.     -271       75     1019.     2982.     1064.     -764.     0.     -211	S		4	m	3	_	654	43			ì	480.		4020.
00     1221.     3021.     1243.     2942.     0.     -307       25     1229.     2933.     1193.     1609.     0.     -256       50     1395.     3056.     1198.     88.     0.     -271       75     1019.     2982.     1064.     -764.     0.     -211	~		52	(1)	~	_	144	S			ì	26		3300.
25 1229. 2933. 1193. 1609. 0256 50 1395. 3056. 1198. 88. 0271 75 1019. 2982. 1064764. 0211	0		7	(L)	0		1243.	945			ľ	307.		23
0 1395. 3056. 1198. 88. 02 5 1019. 2982. 1064764. 02	2		2	7	Q,	_	193	609			7	256		1874.
5 1019. 2982. 1064764. 02	Ç.	·	0	m	0		1198.	8		•	ľ	7		45
	75	·	~	7	•		•	76		•	ſ	211.		2740.

	PUINT	6					•	
VK 1S = V / OR =	105.6	RHO	DMEG*R = 597.3 RHU100 = 0.2251	3 ALFS	Sec = 5.8 S = 0.004235	•8 CLK/5,K 35 CDR/5,R	=0.11436 =0.01082	CMX/S,K = 0.15/9 CMX/S,R =-0.0040
	LOWER	ROTUR BLAD		BENDING	MOMENT	LR EDGEWISE	LR PITCH	c
U			v <b>7</b> •	•	•			<b>.</b>
00.00	ş*1	3918	2966	1738.	-425.	-3439	-25	2.
	. , •	78	2531.	687	91	610	7	32.
77.5	. 4	2726.	2239.	1846.	-33.	-6478.	-31	11.
66.2	4	-	9	151	-141-	-5694.	-315	5.
55.0	4	4	3621.	2210.	-183.	-6713.	-13	31.
43.7	. •	Ď	2859.	1843.	-66-	-9119.		5.
32.5		1691.	1736.	1279.	-106.	-9955.	1-	5.
21.2	. •	Ò	1425.	902.	-444-	-8250.	Ĩ	-4-
10.0		-	1681.	837.	-149.	-6762.	5	57.
98.7	•	Φ	1722.	789.	-938.	-7533.	7	.6
87.5		713.	1083.	417.	-925.	-8195.	122	2.
76.2	7	1030.	-9-	-144.	-716.	-1541.	171	7.
65.0	7	1721.	- 702 -	-401-	-414-	-4512.	7	12.
153.7	ī	ന	-644.	-170-	-274.	-3461.	-22	2.
42.5	•	-d70.	-220.	315.	-100	-5220.	6	95.
131.2		6	436.	811.	48.	-6379.	170	••
20.0	~	1525.	1330.	1329.	163.	-4664-	9	65.
08.7	7	N	2004.	1841.	321.	-3500.	0	97.
7.5	7	0	2220.	2107.	* 767	-4471.	6	93.
6.2	• •	S	.1627	2261.	612.	-0440-	2	24.
5.0	•	30	2352.	2216.	648.	-6541.	109	.6
3.7	-	_	2173.	2013.	611.	-4490	21	16.
2.5		0	1676.	1624.	·616	-3018.	•	35.
1.2		Φ	1123.	1259.	344.	-3471.	-265	5.
0.0		622.	1005.	1124.	42.	-3764.	-350	• 0
8.7	•	4	Š	1069.	-252.	-2037.	-262	2.
3		-	1087.	190.	-327.	171.	-217	7.
56.2	ī	1045.	262.	5	-259.	179.	87-	84.
45.0	1	9	-797-	-13.	-257.	-I468•	-38	82.
. 7		-17.	95.	247.	-321.	2 c	-401	•
22.5	•		1105.	~	-401-	7 +	-35	53.
11.2	•	5	2343.	1587.	-491.	-1774•	0.8-	7.

CMY/S,K = 0.1814 CMX/S,K =-0.0068	<b>9</b>	COS SIN		750.8	ţ	7						9.5 -157.2																			
K =0.13524 R =0.01160	BENDING MUMENT	NIS			6.0171	1.161-	3.6	-143.9	-76.8	-207.5	43.3	-37.3	-16.1	-10.4			SIRE				1288.7	-525.8	-31.1	718.3	-152.0	84.8	-401.1	-12.5	-69-1	4.99	
CLR/S, K CDR/s, R		cos		2042.6	<b>7.16</b> -	-739.3	-92.3	17.5	-213.7	-21.0	41.4	31.6	1.4	8.09		UPPER	SHAFT	cos		5279.1	-3516.3	-389.8	297.2	-211.7	224.7	26.7	-32.5	223.0	6.44	26.7	
,C = 6.0 = 0.006703	CR BLADE NURMAL 2P	SIN			2902.2	-1205.0	-57.4	-284.7	-195.1	-433.4	63.1	45.1	103.8	0		RUTOR	INK LUAD	NIS			382.5	-19.5	36.8	39.3	-72.9	-13.9	177.5	-55.6	35.7	-54.1	
ALFS,C CP/S =	UPPER RUTCR	CCS		4528.7	-431.5	1.646-	-151.3	87.6	-476.2	108.6	68.2	-65.3	185.0	-34.5		UPPER RUT	PITCH L	cos		-45.7	-1111.0	107.2	-15.5	-8.3	10.6	15.4	-116.4	20.4	2.2	11.6	
OMEG*K = 597.3 RHU100 = 0.2247	2	SIN			4753.4	-1586.9	å	-	30	-720.1	•	218.0	24.2	66.5		EUGE	MOMENT . 1R	~			•	•	•	•	•		0.0	•	•	•	
PCINT 10 106-1 CME 0-300 RHL	•	003		3756.9	•	8	-287.5		-914.1	-8.2	•	•	470.1	-135.4		UPPER ROTOR	ING	c u s		0.0	0.0	•	•	•		•	0.0		•	•	
RUN 23 P VKTS = 1 V/OR = 0			HARMONIC	0	<b>4</b>	2	3	4	77	J)	~	œ	6	<b>51</b>	10	64			HARMONIC	C	7	2	3	4	5	ዏ	7	œ	c	10	

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- 15

= 0.1814	175.0 175.0 129.6 143.7 143.7 199.5 199.5 109.5
CMY/ S+R =	26.3 142.4 142.4 142.5 143.5 1
=0.13524 =0.01160	AUMENT  R SIN  -1257-2  -14-1  273-3  140-3  220-8  -58-4  15-1  15-1  13-9
CLR/S.R CDR/S.R	BENDING COS
0.006703	SIN SIN 2295.0 875.8 -23.0 593.7 269.7 378.3 -200.5 -81.7 21.8 51.9 51.9 51.9 51.9 51.9 51.9 51.9 51.9 -11.9 -23.6 35.6 -23.6 -11.9 -11.9 -11.9 -23.6 -11.9
ALFS,C CP/S =	CDS SIN CDS SIN CDS SIN 3313.1 -2295.0 -1499.9 875.8 -23.0 -217.8 -23.0 -217.8 -223.0 -217.9 -217.9 -21.8 -11.9 -21.8 -21.9 -21.6 -23.9 -23.1 -224.2 -23.1 -224.2 -23.1 -224.2 -23.1 -224.2 -23.1 -22.3 -30.6 -23.1 -22.3 -30.6 -23.1 -22.2 -23.1 -22.
OMEG*R = 597.3 RHU100 = 0.2247	2 - 8 - 8 - 4 - 4 - 4 - 4 - 6 - 6 - 6 - 6 - 6 - 6
PGINT 10 106.1 QMEG*R 0.300 RHU100	.18 SIN 3991.9 -465.0 -37972186.5 891.9 -2186.5 891.9 -2186.5 891.9 -154.9 -154.9 -159.2 1529.2 131.6 -29.2 1529.2 11029.2 1229.2 12.
RUN 23 VKTS = V/DR =	HARMCHIC 100 100 100 100 100 100 100 100 100 10

ţ

CMY/S,R = 0.1814 CMX/S,R =-0.0068	UPPER KUTUK SHAFI SIKESS	,	1972.	1758.	2067.	3144.	3554.	3202.	3829.	5641.	7126.	7932.	8818.	9861.	10330.	9509.	7813.	7074.	7936.	8648.	8138.	7369.	6785.	5826.	2	4224.	4127.	4161.	4075.	3423.	180	1097.	954.	1597.
=0.13524 CM =0.01160 CM	UR PITCH LINK LOAD		-129.	55.	0	112.	15.	219.	-	180	-37.	41.	375.	650.	446.	-3.	111.	530.	331.	-154•	-116.	•99	-169.	-525.	-671.	-569-	-667-	-260	-571.	-660	-361.	-185.	M	
CLR/S,R CDR/S,R	UR EDGEWISE BENDING • 1R		••	• •	• •	•	•	ò	•	•	•	•	•	•	•	•	•	o	ċ	•	•	•	•	•	•	ċ	·	o	·	•	•	•	•	•0
ALFS,C = 6.00 CP/S = 0.006703	MCMENT • 6R			48.		77	-1261-	355.	08	48	18	66	2010.	47	57	6	-1447.	-2296.	-2145.	-2314.	-1941-	æ	4	-330•	959.	S	3183.	~	7	4351.	_	296.	-307.	- 362 -
	BENDING .3R		3	5	1140.	2235.	2924.	3143.	3416.	3849.	4439.	4974.	4893.	4275.	3748.	3371.	2941.	2470.	1747.	99	34		2•	3	58	32	143	32	38	'n	55	1670.	62	44
UMEG*R = 597.3 RHU100 = 0.2247	BLAUE NORMAL • 2R		87	46	765	351	12	6658.	9	61	23	13	50	63	98	35	69	13	4	07	05	18	12	84	52	250	62	690	904	703	266	66	958	39
PUINT 10 106.1 UME 0.300 RHU	UPPER RUTUR • 1K	•	8	771.	4	2	~	1277.	4	4	g	093	S	61	90	0	-	œ	3534.	•	0		0	3		3	7	3	-	~	88	3173.	9	33
RUN 23 VKTS = V/CR =		S	0	1.2	2.5	3.7	5.0	56.25	7.5	8.7	0.0	01.2	2.5	23.7	35.0	146.2	51.5	168.7	0.0	91.2	02.5	13.7	25.0	36.2	41.5	58.7	70.0	81.2	95.5	03.7	15.0	26.2	37.5	48.7

RUN 23	POINT	10		607		•		13636	1
Λ α	0.300	RHL	CHEC+K =	0.2247	ALF3,C CP/S =	= 0.006703	0.0 CLK/5,R 703 CDR/5,R	=0.01160	CMX/S,R = 0.1814 CMX/S,R =-0.0068
	LUNER	ROTOR	BLADE	ORMAL	ING	MOMENT	LR EDGEWISE	LR PITCH	
		. 1R	.2R		•3R	.6R	BENDING . IR	LINK LOAD	0
S									
0.00	<b>.</b>	3733.	7	•	4175.	-299.	-3921.	4-	5.
88.7	w	•	52	5.	4255.	107.	-5921.	-321	1.
77.5	,	3	92	•	4356.	421.	-8072.	-266	• •
66.2	v	~	47	•	4689.	404	-9118.	01-	5.
55.0	7.7	9	41	•	4937.	325.	-9340	-14	N
43.7	5		22	•	4809.	336.		<b>ι</b> ς	3.
32.5	,	$\sim$	01	•	4243.	238.	-11076.	242	2.
21.2	v	Б	20	•	3494.	-55.	-11003.	•	3.
10.0		0	89	•	3001.	-418.	-9564.	3	•
98.7	•	Ð	19	3.	2702.	-695.	-8396.	227	7.
87.5	***	5	63		2095.	-753.	-8223.	61	•
76.2		1480.	3	• 9	1185.	-603.	-7722.	101	7.
65.0		-	_		529.	-419.	-5994.	130	••
53.7	,	0	35.	•	434.	-270-	-4109.	8	. 8
142.		253.	606	•	785.	-122.	-3517.	173	3.
31.2		•	~		1279.	• 9	-1961-	32.	2.
120.0	~	3	1849	•	1644.	155.	-3959.	181	7.
08.7	· <b>V</b>	2	15	5.	1934.	383.	-3148.	151	1.
7.5	, <b>v</b>	•	3	•	2300.	581.	-4726.	389	.6
6.5	. 7	N	9	•	2521.	674.	-3514.	322	2.
5.0	. 4	•	Ģ	•	2405.	741.	-4402.	153	3.
3.7	7	5	28	•	2200-	739.	-3950	306	••
2.5	7	<b>O</b>	=	•	2070.	544.	-2437.	184	•
1.2	.7	3	7		1934.	223.	-1169.	-178	• 33
0.0	. 7	~	38		1846.	-67.	-670-	1	7.
8.7	. 7	9		•	1755.	-241.	-345-	130	•0
ŝ		5	8	•	1379.	-244.	455	-322	2.
56.2		3	_	8.	830.	-128.	1307.	-432	2.
45.0		5			663.		1011.	-162	2.
	7	1557.	1253	•	71		-439.	-43	1.
22.5	~1	~	σ	•		_	-7007-	-659	9.
11.2	~	$\sim$	3	3.	54	-387.	-2880-	-22	2.

CMY/S,R = 0.1888 CMX/S,R =-0.0126	8 <b>9</b>	COS SIN	1063.5	699.3 -59.1	-14		63.5 278.5		43	30	١	8-	4-																
CLR/S,K =0.14505 CDR/S,R =0.01129	AL BENDING MOMENT	COS	2486.8		-939.3 -1029.3											SHAFT STRESS			5775.2	•	-242.9 -645.5	•	945	99-	101	-515	-228	-108	-12
1 ALFS,C = 6.0 1 CP/S = 0.009078	UPPER RUTOR BLADE NCRMAL		5113.5	-251.6 3351.5	-1212.9 -1546.1						80	226			UPPER ROTOR	PITCH LINK LOAD			-149.2								11.3 -114.6		
PGINT 11 106.4 LMEG*R = 598.1 0.300 RHC100 = 0.2231	18	CGS SIN	4585.5	-422.5 5433.8	'		6.	7.8	8.	2.2	.7 390.	æ			UPPER RUTUR EDGEWISE	1. F	COS SIN		0.0								0.0		
RUN 23 VKTS = V/OR =			HARMUNIC O	-	2	٣	<b>4</b>	~	9	7	œ	6	01	168	В			HARMONIC	0	-	7	~	4	~	9	7	ထ	6	10

RUN 23 VKTS = V/CR =	PUINT 106.4 0.300	11 OME RHL	OMEG*R = RHU100 =	598.1 0.2231		ALFS,C : CP/S =	6.0 0.009078		CLR/S,R CDR/S,R	=0.14505 =0.01129	30.55	CMY/SsR #	= 0.1888 =-0.0126	
				ل.	LOWER R	ROTOR	BLADE N	NORMAL BE	SNIGN	BENDING MOMENT				
		•	. 1R	,					. 3R			.6R	~	
		c 0 s	SIN	z	COS		SIN	03	S	NIS		COS	NIS	
HAKKONIC	555	9,45			4588	^		323	6.			139.5		
) <b>~</b>	121	25.8	-5708		-313.1	ı	642.2	-74.2	4.2	2196.0		111.5	21.9	
· ~	-22	-2231.4	1379.0		-1473.		1221.3	-120	9.2	805.6		-465.3	155.6	
m		38.9	-20°		-305-		79.6	-14	1.1	35.1		131.7	-8.2	
•	<u>1</u>	94.3	1092.5		-85		704.2	-70.8	9.8	321.5		6.99	-175.7	
S.	7-	83.1	-78		-173		36.7	-8	2.9	31.3		45.4	8.0	
છ	M	12.0	686		375.		278.7	150	9.6	189.5		-28.6	-67.6	
~	ĸ	22.7	-308		72.	1	302.9	7	1.4	-86.3		-41.4	35.9	
œ	1-	6.51	-157		-37		-45.1	12	2.8	5.0		-1.9	17.8	
6	4-	•	281		53.	_	10601	7	S.8	1.0		7.3	-21.9	
10	ĺ	88.7	152		7.	_	1.96	-3.	2.4	11.5		12.4	-22.9	
10														
69	LOWER	R ROTOR	OR EDGEW		LCM	LCWER ROTOR	TOR							
	BEN	OINC		.18	PITCH LINK	LINK	LUAD							
	_	0.00	SI	z	CUS		NIS							
HAPMONIC						•								
0	-413	38.8			81.									
_	45.	4532.9	3795	15.1	-230		225.7							
2	77	82.6	-1718	8.2	-54.		107.7							
٣	4	6.91	4-	•3	51.		29.7							
4	•	Φ	-10.3	•3	-25.		53.4							
5	4-	44.5	29	•2	25.		28.8							
\$	7-	0	-143	0.	38.		6.4							
_	- 76	S	-1047	89	-6-		-73.5							
œ	-13	38.3	$\sim$	2.0	4.0	•	-7.6							
6	6-	9	-13	٠,	-55	ı	_							
01	1	71.1	91-	•2	-121-		-87.0							

1 .

3 XUN 23 XVX 23 XVX 23 XVX 23 XVX 23 XVX 23 XVX 24	106.4 0.300	I OMEG*R RHUIOO	= 598.1 = 0.2231	ALFS,C CP/S =	0°9 = 7°	CLR/S,R CDR/S,R	=0.14505 =0.01129	CMY/S,R = 0.1888 CMX/S,R =-0.0126	
	JPPER ROT	ROTOR BLADE	DE NORMAL 28	BENDING P	MUMENT • 6R	UR EDGEWISE BENDING .IR	UR PITCH LINK LUAD	UPPER RUTOR SHAFT STRESS	
		•	1		; ;				
0.00	135	2.	1191.	1362.	149.	•0	-206.	3402	
1.2	191	•	.986.		-54.	•0	•	2053.	
2.5	214	· •	3203.	S	-245.	•	175.	2200.	
۲.	5316	•	.958.	2747.	-1468.	•	*64	3272.	
5.0	847	•	7050.	3381.	-1745.	ာ	-116.	3060.	
6.2	837		1484.	3625.	577.	• •	22.	2277.	
7.5	808	•	7317.	4078.	3015.	0.	232.	2928.	
8.7	100	3.	,299.	4689.	3456.	0	184.	4490	
0.0	194	•	101.	5427.	3248.	•	-84.	5411.	
01.2	304	•	1619.	6083.	3258.	•	-159.	5816.	
12.5	8	•	1344.	6007.	3078.	•	352.	.1699	
23.7	189	•	1.20.	5218.	3403.	•	852.	8162.	
35.0	795	8	1946.	4436.	3681.	•	386.	9097.	
46.2	124	•	818.	3833.	1691.	•0	-305-	8411.	
57.5	864	7.	1151.	3299.	-1462.	•0	•89	.4689	
68.7	703	•	.597.	2789.	-2677.	•	618.	6513.	
80.0	377	•	.709.	1929.	-2618.	•0	131.	7571.	
91.2	3861	•	.891	773.	-2971.	•0	-427.	8616.	
02.5	1	5.	105.	102.	-2371.	•	-151-	8882.	
13.7	218	•	.001.	-13.	-657.	•	52.	8678.	
25.0	-155	8	808.	-91.	-148.	•	-311.	9228.	
36.2	28	•	.750.	. 49	-247.	•	-708.	7565.	
47.5	Ę.		349.	668.	1343.	•	•906-	6789.	
58.7	-60	•	314.	1201.	3262.	•	-803	6068.	
70.07	100	•	:822.	1436.	3536.	•	-374.	5801.	
81.2	217	7.	1645.	1644.	3831.	•	-294.	6308.	
92.5	106	3.	1594.	1864.	5096.	•	-174.	7093.	
03.7	87		327	2072.	4742.	•	-937.	6931.	
15.0	_	•	166.	2249.	2019.	•	-529.	5230.	
26.2	9	•	129.	N	108.	•0	-248	33	
37.5	Ó	•	199	0	436.	•0	-272.	3121.	
	115	2. 3	109	89	762.	•	-292.	91	

RUN 23 VKTS = V/OR =	106.4 106.4 0.300	L1 UMEG*R RHU100	" "	598.1	ALFS, C CP/S =	,C = 6.0 = 0.009078		CLR/S,R CDR/S,R	=0.14505 =0.01129	CMY/S,R = 0.1886 CMX/S,R =-0.0126	<b>6</b> 00
	LOWER RC	OT OR BLADE			NDING	MOMENT	LR EDGEN		LR PITCH	<b>-</b> 9	
U	•	¥.	٧7.	•	¥,	•	TONIA	¥1.	LINK LUAD	€	
2000	1305	6	8927	5.7	7117	-143.		-4024-	-	~	
•	1230			. 6	011	26.		77	-389		
77.5	1130	. 6	8750.	9	6171.	644		825	16-		
66.2	1275		•	40	6488.	693.	1	S	` -	12.	
55.0	140		6666	99	6699	647.	•	-10951.	-190		
43.7	126	•	æ	9	6540.	674.	1	(T)	172	25	
32.5	1,401	• 80	v	55	.610	577.	•	-10735.	45	52.	
21.2	116	• 20	-4	5	5061.	243.	1	-11987.	13	33.	
10.0	166		7028.	44	.46.	-210-	1	-11819.	_		
98.7	768	•	6754.	40	4034.	-565-		-9780.	35	96.	
87.5	29(	•	5487.	35	33.	-628.		-7857.	27	79.	
76.2	747	2.	3263.	51	.01	-463.		-7234.	901	.90	
65.0	77	•	$\sim$	ري	880.	-292-		-6780.	159	.69	
53.7	74-	•6	467.	4	.08	-188.		-5031.	243	• 50	
142.5	1,5	• a	634.	<b></b>	.29.	-127.		-2578.	390	.0.	
31.2	132		1418.	21	.10.	-73.		-1574.	194	.7.	
20.0	16.	•	1939.	2	.849	109.		-2397.	317	.7.	
08.7	116		٠	16	,75.	405.		•	34	47.	
7.5	14:	•	•	5 7	146.	596.		-1261-	482	32.	
6.2	175	•6	2413.	22	228.	702.		-196.	593	.60	
5.0	348	•	$\sim$	23	159.	.662		-1107.	165	5.	
3.7	218	•	ന	24	485.	688.		-2412-	345	.2.	
2.5	384	•	3232.	25	580.	2		-1759.	156	96.	
1.2	39.	•	3664.	25	,22.	107.		714.	-15	5.	
0.0	305	2•	CD.	24	53.	3.		2329.	59	98.	
8.7	314	2•	un	23	.09	-110.		1385.	87	80.	
7.5	304		3031.	<b>2</b> C	36.	-116.		159.	-33	33.	
56.2	707	•	· Th	16	.88.	24.		1437.	-16	.1.	
45.0	204	l.	$\sim$	11	0			3106.	1-	•1.	
33.1	394	œ.	S	22	B	35.		1407.	-63	11.	
Ň	705	5.	4575.	33	132.	-99-		-2288.	~	.7.	
11.2	100	•	6871.		3	-202-		-4037.	01-	•00	

= 0.1607 =-0.0055	×	NI S		-2404-1	218.4	367.6	-364.8	540.9	-88-4	O. &	399.0	31.8																
CMY/S, K II	**************************************	C03		1200.0	-103.0	-314.4	404.0	102.2	-21.7	195.6	22.0	101.2																
=0.09322 =0.01567	MUMENT R	NIS	9	-262.0	59.4	-106.0	88.2	-117.0	-63.9	37.5	-9.5	-10.3		RUTUK	<b>SIRESS</b>	SIN			735.8	-650.1	6.4-	502.1	-430.2	46.3	-447.7	296.1	-89.5	19.2
CLR/S, R COK/S, R	AL BENDING MUMENT • 3R	SOO	-708.6	-196.5	25.1	119.9	-129.4	5.1	55.5	-1.0	7.0	34.7						5000.4	-3385.2	-730.9	309.7	-8-1	234.1	-57.6	-126.0	6.69	0.0-	-41.6
C = 8.2 = 0.001055	P BLADE NORMAL R	SIS	0	-438.7	97.9	-185.7	199.1	-230.6	57.7	1.64-	-221.1	1.1		RUTUR					239.0	20.0	29.4	-30.7	-85.1	52.2	93.1	74.3		<b>1.</b> 0-
ALFS,C CP/S =	UPPER ROILR	COS	639.2	-180.7	42.9	287.8	-364.7	50.6	45.6	-124.7	165.8	-63.9		UPPER RUTUR	PITCH LINK	COS		-481.2	-31.2	-6.3	-57.3	-58.5	43.5	27.4	-68.4	-36.2	22.6	9•3
UMEG*R = 600.5 RHUIGO = 0.2214	ט	NIS	60		143.3	-388.4	524.7	-404.3	290.1	6.08-	-571.1	113.9		EUGEW I	MOMENT . 1R	S I S			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0•0
PLINT 12 106.8 CM 0.300 RH	•	503	-1851.2	-260.6		•	-567.5	-1.6	70.5	-350.6	αO°2	-170.2		UPPER RUTUR	S	503		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RUN 23 VKTS = V/CP =		HARMONIC	0 -	7 2	· M	4	S.	ç	_	æ	6	10	172				HARMCHIC	0		7	3	4	5	9	7	89	ņ	10

CMY/S,R = 0.1807 CMX/S,R =-0.0055	-249.3 -249.3 -249.3 -249.3 -249.3 -360.8 -360.8 -360.8 -360.8 -360.8 -360.8 -360.8 -286.4 -2
=0.09322 =0.01567	SIN SIN 246-1 152-9 157-4 157-4 6-8
CLR/S, R CDR/S, R	BENDING MUMENT  -3R  -3R  -3R  -3R  -65.8  -826.8  -826.8  -7.9  -23.3  -23.3  -23.4  -17.5  -16.0  -23.4  -5.0  -5.0  -6.8
8,2 0,001055	R BLADE NORMAL R SIN 957-7 458-5 -89-7 234-0 400-0 301-7 -72-2 -33-6 18-3 23-4 18-3 23-4 18-3 23-4 18-3 -9-6 4-2 151-0 -9-6 4-2 15-4 4-1 15-4 4-1 15-4 15-6 15-6 15-6 15-7 15
ALFS,C CP/S =	LOWER ROTUR 2R COS 2R COS 2R COS 2R 436.5 -552.7 -978.4 44.9 318.6 -77.6 101.9 172.1 18.3 30.8 LOWER RU COS COS 22.3 -22
12 DMEG*R = 600.5 RHU100 = 0.2214	** SIN SIN ***
PCINT 1 106.8 0.300	COS256.9 -1161.6 -1356.4 -1358.0 -148.8 -358.0 -148.8 -284.0
RUN 23 VKTS = V/OR =	HAPYON IC 1123 TARETHIC 123 TAR

The second secon

RUN: 23 VKTS = V/CR =	POINT 106.8	12 UMEG#R RHU100	#R = 606.5 00 = 0.2214	.5 ALFS,C	, c = 8.2 = 0.001055	CLR/5, K CDR/5, R	=0.09322 CM =0.01567 CM	CMY/S,R = 0.1807 CMX/S,R =-0.0055	
	UPPER	OTUR	BLADE NORMAL	BENDING	MUMENT	UR EDGEMISE	UR PITCH	UPPER KUTÜR SHAFI STRFSS	
v		4	• •	)	•	•			
00-0	ì	9	934	-348-	-867.	0	-636.	~	
200	-2	100		-742.	-1283.	•0	10	1078-	
2.5	1 -	6	-	-907	-2643.	•	-403	310	
3.7	61-	~~	- 10	-840.	-2746.	• •	-489.	1061	
5.0	<u>.</u>	~	•	-606-	-2028.	•0	-354.	2608.	
6.2	7-		•	-1135.	-2422.	•0	-19.	3083.	
	7-	1980.		-1282.	-3278.	•	• 96	3628.	
8.7	1-	Ð	•	-1203.	-3382.	• •	-224.	4912.	
0.0	1-	2	•	-876.	-3617.	·°°	-577.	6567.	
01.2	1	632	-	-665.	-4385.	<b>ံ</b>	-532.	7619.	
2.5			1243.	-987.	-4133.	• •	-566.	8148.	
23.7	-2	269.		-1463.	-2601.	•	-155.	8939.	
35.0	<b>5</b> -	4366.	~	-1458.	-2005-	•°0	-166	9697.	
46.2	7-	045.	-64.	-1155.	-3603.	0.	-281.	9104.	
57.5		234.		-1015.	-6464-	•0	-395.	7151.	
68.7	•	619.	027	-1028.	-4645.	•	-485.	•9909	
80.0	-2	124.	3	-1145.	œ	•	-455.	7194.	
91.2	-2	832.	-61.	-1403.	~	•	-417.	8479.	
02.5	<b>7</b> -	•	-609-	-1576.	-1999.	•	-906-	7789.	
13.7	<b>5</b> -	-	-970-	-1454.	14	•	-624•	6437.	
25.0	-2	0	-119.	-1060-	-1421.	•	-630	6194.	
36.2	1-	~	940.	-518.	19	•0	-633	6101°	
47.5	1-	$\sim$	103	-109.	94.	•0	-161.	5232.	
58.7	-15	4	21	-20.	882.	•0	-818-	4757.	
70.0	'	~	565	10.	38	•	-636•	5229.	
81.2	1-	~	36	164.	2564.	•	-521.	0	
95.5	-1	S	960	215.	S	•	-128.	4483.	
03.7	•	86	46	m	87	•	-979-	98	
15.0	•	4	665		07	•	-654.	8	
26.2	1-	33	385	84.	601.	•0	-443	1501.	
7.5	•	88	1437.	-1-	62	•0		Ē	
48.7		90	533	-95.	-1326.	•	-111.	1639.	

P!IN 23 VKTS = V/CR =	PUINT 106.8 0.300	12 OMEG*R RHUICO	A 00	600.5	ALFS,C CP/S =	•C = 8.2 = 0.001055		CL R/S, R CDR /S, R	= 0.09322 = 0.01567	CMY/S,R = 0.1807 CMX/S,R =-0.0055
	LOWER	ROTOR B	BLADE I	NGRMAL	BENDING	MGMENT	LR EDG	EDGEWISE	LR PITCH	I
		81	7	~	.3R	•6R	Z	7.	LINK LUAD	AD
S		1	l							
000	ı	987.	~	7.	-253.	-547.	•	.2562.	-3	38.
88.7	1-	7	~	7.	92	-457.	•	507	-2	57.
77.5	1	7	6	•0	4	-428.	1	-6394.	-3	78.
.2	7	1045.	99		418.	-525.	•	-5843.	£-1	-366.
55.0	Ī	9	0	4.	532.	-551.	,	.5729.	-111	77.
43.7		9	Q,	4.	305.	-435.	,	-7366.	1-	108.
32.5	ĺ	_		8.	-14.	-398.	'	-8829.	Ī	65.
21.2		~	-	•	-180.	-569-	•	-8082.		27.
10.0	<b>→</b>		-	3.	-58.	-814.	,	-6265.		•6
58.7	-	$\sim$		••	190.	-853	•	-5954.		13.
87.5		$\sim$	4	2.	161.	-911.	1	-7207-	~	12.
76.2	f	~		• 9	-153.	-730.	•	-7485.		70•
65.0	•	_	_	.6	7	- 508 -	•	-5695.	•	16.
53.7	Í	~	_	5.	178.	-569-	1	-4169.		52.
42.5	•	3	9	.0	728.	-22.	•	5139.		80.
31.2	7	O		5.	1157.	163.	•	-7074.		46.
20.0	-	13	16	۶.	1583.	284.	•	-7049.	~	118.
09.7	7	~	37	7.	2076.	410.	•	-5485-	-	113.
7.5	7	12	S	3.	2425.	515.		-5312.		3.
6.2	7	0	11	• •	2422.	503.	1	-7021.		.69
5.0	7	$\sim$	43	۷.	2103.	594.	•	-7814.	1	150.
3.7		σ	72	.6	1643.	585.	1	-6125.		15.
2.5	1	v	90	5.		462.	J	3964.	1	91.
1.2	ſ	S	~	٠. د	119.	240.	1	3607.	-1-	-160.
0.0	-1	$\circ$	0	٠,	500.	-54.	•	-4145.	£-	-350.
9.1	i	Ð	άŏ	• 9	248.	-369.	1	.3231.	£-	-363.
• 5	-1	0		•	-128.	-553.		-895.	-	185.
56.2		~	83	.00	-641.	-553.		179.	7-	271.
45.0	-3	0	111	1	111	-516-	1	3	<b>5</b> -	59.
333.75	-34	417.	961-	l	128	-524.	•	-2607.		375.
22.5		75	149	•	ァ	-543.	1	.5355-	٤-	319.
11.2		4	7	7.	-508•	-565.	•	-1530.	4-	14.

21 -4		v	
= 0.2212 =-0.0151	•6R SIN	-2259.5 -1636.4 389.7 519.1 -192.1 499.8 15.3 -157.9 16.5	
CHY/S,R CHX/S,R	• 500	-13.1 2209.7 -2102.5 198.9 645.7 646.4 183.5 -239.7 -239.7	
=0.13127 =0.01556	MUMENT SIN	-84.5 -961.1 59.1 -149.3 -206.6 -26.6 -26.6 -27.3	SIRESS SIN SIN -3869-1 -661-5 -406-3 -498-1 -161-9 151-6 -530-4 -60-8
CLK/5,R CDK/5,R	AL BENDING MUMENT  • 3K CGS SIN		0PPER 1 SHAFT 0 COS 1 -2439.6 - -326.7 - -326.7 - -326.7 - -326.7 - -326.7 - -326.7 - -326.7 - -264.6
* 8.5 0.007816	BLADE NURMAL SIN	362.3 -1495.6 1.1 -375.2 62.3 -461.6 84.9 15.1 -104.6 52.6	338.6 LOAD SIN -1.6 -17.4 -17.4 -14.9 -14.9 -13.2
ALF3,C CP/S =	UPPEP RCTCR .2R CCS	3239.1 2285.0 -1123.5 -1 -57.7 -98.7 -502.9 -64.7 -114.1 234.9	-407.8 -407.8 -125.1 338 -125.1 338 -125.1 338 -125.1 -13.8 -15.0 -17 -26.8 -72 -19.0 -14 -44.1 29 -44.1 29 -44.1 29
*R = 601.7 00 = 0.2210	NIS	u	NOT MOMENT . 1R SIN
PCINT 13 107.0 GMEG*R 0.500 RHUIOO	. 18 . 18		E E E E E E E E E E E E E E E E E E E
KUN 23 P		11 12 12 13 14 14 15 15 15 15 15 15 15 15 15 15 15 15 15	HAR 4CN IC 0 1 2 3 4 4 10

= 0.2212 =-0.0151	8 <b>9</b>	SIN	224.5	-73.4	44.2	-133.1	22.3	-54.3	0-8-	14.7	43.9	-11.5																
CMY/S,R =	•	Sno	88.1	. •	154.3	50.2	3.4	-37.4	1-64-4	4.6-	1.1-	1.9																
=0.13127 =0.01556	MOMENT	SIN	-759.9	417.9	20.8	179.6	-21.1	206.5	-30.0	7.6	-2.8	17.2																
CLR/S,R CDR/S,R	MAL BENDING MOMENT	SOO	3138.2	-1653.3	-187.3	-66.1	22.2	103.1	18.6	16.7	15.1	-3.2																
C = 8.5 = 0.007816	R BLADE NORMAL	NIS	-1468.9	799.2	22.6	447.3	-89.5	311.3	-176.9	-64.6	-175.4	25.4		ROTOR	NK LUAD	215			293.0	60.5	110.7	42.1	53.6	22.3	-58.5	-14.7	-191.7	-27.3
7 ALFS,C CP/S =	LOWER ROTCR	SOO	4492.2	2032.4	-375.4	-76.9	21.0	298.1	230.0	1.1	-60.1	25.0		LOWER	PITCH LINK	cos		78.	-266.9	-47.9	110.5	-35.1	0.44	26.2	48.2	-19.4	6.41-	16.2
OMEG*R = 691.7 RHU100 = 0.2210	~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~	NIS	7-2108-	680	6.691-	698.5	-132.7	676.4	61.9	-138.4	-401.2	53.8		DR EDGEWISE	MCMENT . 1R	NIS			6106.3	-649.7	475.1	-39.9	-30•6	-102.3	-926.8	-82.5	1.901	-33.2
PCINT 13 107.0 GM 0.300 RH	•	<b>SOO</b>	5436.1			•	•	•	•	_	_	5.8		LCHER ROTOR	BENU ING	SOO		•	4537.4	3469.1	430.7	8 - 18 6 - 8	73.7	9.68-	8-868-	37.0	138.3	13.7
RUN 23 VKTS = V/DR =		SINUNOMH	0 -	• ~	· ~	4	5	•	_	8	6	01	<del>-</del> .	17	77		HARMONIC	0		2	•	4	5	9	7	හ	6	C <b>1</b>

į

S,R = 0.2212 S,R =-0.0151	UPPER KUTÜR SHAFT STRESS		12	2272•	1654.	1281.	354.	-377.	373.	2098	3224.	3639.	4428.	5750.	6540.	6201.	5369.	5791.	7818.	9579.	9774.	9572.	016	10766.	045	9759.	9535.	9104.	9513.	8471.	7075.	6262.	5991.	5264.
0.13127 CAY/S,R 0.01556 CAX/S,R	UR PITCH LINK LUAD		-568	-555.	-310.	-106.	-122.	-81•	-36.	-229.	4	-348	2	-238.	-114.	- 19.	-46.	135.	163.	-06-	-315-	-486.	-141.	-935.	6	$\boldsymbol{x}$	-739.	-664.	$\infty$	-874.	-680-	-546	S	3
CLR/5, K = CDR/5, R =	UR EDGEWISE BENDING .IR		<b>.</b>	•0	•			•			• 0	• 0		• •			•		o		•0			•			•					•		•0
S,C = 8.5 S = 0.007816			58		9	-2456.	-2998•	-2212.	-742.	260.	-52•	-957.	-873.	123.	-167.	-2539.	-4417.	-4306.	-3789.	3966	-3515.	-2622.	-2386.	-1427.	1244.	3729.	5134.	6379.	6713.	5175.	3262.	2199.	1500.	1254.
7 ALF 0 CP/	L BENUING MOMENT		1930.	77	17	72	85	1615.	44	47	83	18	85	9	3	~	_	Ŷ	m	20	7.7	Ð	0	-134.	819.	4	0	S	0	30	44	3309.	03	19
UMEG*R = 601. RHUIOO = 0.221	BLADE NCRMAL .2R		13	2968.	2864.	96	62	27	95	98	59	15	44	80	16	11	2663.	56	14	2	46	36	14	45	37	2973.	82	59	5077.	70	43	6516.	16	91
PCINT 13 107.0 CME 0.300 RHU	UPPER ROTOR		_	821.	1535.	3308.	~	3545.	3300.	\$222.	3627.	5391.	5781.	2382.	-378.	1139.	2313.	-390.	9	450	-2883.	490	245	-486.	-68	824.	2325.	3024.	3562.	5001.	6362.	6300.	4998	9
RUN 23 VKTS = V/CR =		S	0	1.2	2.5	3.7	5.0	6.2	7.5	9.7	0.0	91.2	12.5	23.7	35.0	146.2	157.50	168.7	80.0	91.2	02.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	95.5	03.7	15.0	26.2	37.5	48.7

	13 CMEG*R = 601.7 RHU100 = 0.2210	ALFS,C = CP/S = 0	8.5 0.007816	CLR/5,R =( CDR/5,R =(	0.13127 CMY/S,R = 0.2212 0.01556 CMX/S,R =-0.0151
ROTOR BLADE NORMAL • IR		BENDING MUMENT .3R .6R	<b>.</b>	R EDGEWISE SENDING .IR	LR PITCH LINK LOAD
``	•	r	•	,	-
•	700	2	. 01	-02739-	-313-
5. 69	505	. 4	94.	1954	130
5. 8	557	9.	39.	-14656.	61.
0. 86	ထ	9• 6	19.	44	64.
9. 83	519	7. 6	12.	-12402-	219.
5. 78	541	m	.07	-11668.	196.
7. 75	491		20.	-11936.	246.
0. 74	47	<u> </u>	32.	-10919.	95.
8. 749	453		97.	-8325.	- 697
3.	403	יני. ר	• 0 •	-5819°	342.
3.	326	7-	25.	-1095-	125.
2. 3	7	•	. 7 .	1914	231.
63. 4021. 95. 4544.	335	355.	15. 63.	-2896.	837.
1 ·	375		74.	19.	511.
0• 50	396		743.	-1775.	561.
7. 52	381		•09	-3336.	157.
4. 48	385	7	032.	-2189.	460.
1. 45	381		86.	-199.	207.
7. 45	369		.66	-113.	418.
0. 42	313		373.	-630.	372.
5. 32	236		60.	1222.	36.
5. 22	2	4.	34.	4636.	203.
8. 12	73	4.	35.	6108.	482.
5. 2	25	3.	566.	4950.	163.
21			685.	3750.	- 86.
-2	- 56	•	619.	3793.	102.
25	19-	8.	79.	ď	-132.
7		5.	22.	722.	-
4. 14	135	84	16.	2	
3. 43			. 10	-6997	-107-

İ

= 0.2056 =-0.0071	-2342.0 -1064.4 58.7 894.5 21.7 393.2 -52.8 65.0	
CMY/S,R CMX/S,R	CUS -229.7 1064.0 -2184.0 -258.3 -413.5 199.7 -1.4 -556.3 -366.2 52.5	
=0.11709 =0.01566	AUMENT R SIN -300.7 -628.8 -24.6 -200.9 -30.1 -170.0 -170.0 -170.0 -170.0 -170.0	STRESS STRESS SIN 1079.5 -834.1 -26.7 892.1 -232.5 56.3 -281.8 -281.8
CLK/S,R CDR/S,R	L BENDING MUMENT • 3R • COS • SIN 1028.4 217.6 - 300.7 -689.2 - 628.8 -38.0 24.6 166.6 - 200.9 -40.4 - 50.1 54.8 - 170.0 37.9 - 38.0 6.7 47.1 -1.1 - 15.0	UPPER SHAFT COS -5972.7 -2006.2 -618.1 72.7 -224.2 215.8 -34.4 -101.8 -18.5 -18.5
c = 8.4 = 0.004506	CK BLADE NORMAL 2R SIN -6.1 -975.4 31.1 -419.0 -20.5 -307.1 88.9 -100.9	OR LUAU SIN 37.9 25.7 41.4 41.4 41.6 6.3 1.4.7
ALFS,C CP/S =	JOPPER RCICK • 2R • 3075.8 • 35.0 • 850.6 • 29.5 • 10.8 • 162.0 • 205.9 • 26.2 • 148.7 • 290.4 • 47.3	UPPER ROTOR COS SI -459.1 -459.1 -167.0 337 135.9 -25 -116.6 41 28.3 -37 -43.0 -76 6.7 -18 -55.5 44 -13.5 0
604.1 0.2198		T
OMEG*R = RHU100 =	597.8 -1334.3 -911.3 -911.3 -584.9 -296.5 -164.8 -185.4	ROTUR EDGEM NG MUMENT . .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0
41	534.3 534.3 534.3 539.5 620.0 620.0 620.0 620.0 620.0	<b>-</b> 0 000000000
PUINT 107.0 0.299	-1	UPPER BEND C
RUN 23 VKTS = V/OR =	HARMONIC 0 1 2 3 4 4 7 7 10	HARMONIC 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2

-

. . . 7 . . 91

= 0.2056 =-0.0071	492.3 492.3 262.7 -15.9 -15.9 -11.8 23.8 23.8 23.8 45.5
CMY/S,R CMX/S,R	122.3 215.3 215.3 215.3 -505.0 57.6 -23.3 -7.9
=0.11709	MUMENT S SIN 3411.8 974.4 101.1 154.1 154.1 15.2 15.2 15.2
CLK/S,R COR/S,R	AL BENDING MUMENT
8.4	SIN 676.7 1415.5 130.9 716.2 269.1 341.5 -183.9 -173.2 -183.9 -173.2 16.4 16.5 16.4
ALFS,C CP/S =	COS SI  COS SI  2004.8 676 -1440.2 1415 -1440.2 1415 -18.1 130 86.8 269 291.0 341 62.7 -183 -27.9 -173 -27.9 -173 54.8 16 CUS SI -10.5 -44.1 111 -2.7 -9.5 40 29.9 53 35.3 -12.5 -35.8 1
UMEG&K = 604.1 RHU100 = 0.2198	######################################
PUINT 14 107.0 UME 0.299 RHC	LEST.3  1857.3  1857.3  472.5  1840.9  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  183.0  184.2  183.0  183.0  183.0  183.0
RUN 23 VKTS = V/CR =	HARMON CC 190 HARMON IC 190 HA

William Control

5,R = 0.2056 5,K =-0.0071	JPPEK KOTOK SMAFT STRESS		3214.	2	22	4413.	4667.	4934.	5222.	6082.	7512.	8716.	9333.	9682.	9782.	8997.	7220.	6025.	6817.	8099.	7685.	6397.	5938	5591.	4594.	4303	5376.	6398.	6292.	5365.	4326	3671.	36	12
=0.11709 CMY/S,R =0.01566 CMX/S,K	UR PITCH LINK LUAD		0	-643.	-483-	-265.	-270.	-228.	-87.	-239.	-411.	-359.	-155.	-154.	-169.	-130	-61.	92.	107.	-153.	-413.	-582.	-178.	-884	-878-	-885.	-800•	-707-	œ	-1023.	-786.	-565.	-605.	-619-
CLK/3,R CDR/5,R	UR EDGEWISE BENDING • LR		•	•	•	ં	•	•	•	•	•	o	•	· 0	•	•	•0	•	•	• •	•	•0	•	•	ċ	•0	0	• •	•	•	•0	•	•	•
,C = 8.4 = 0.004506	MCMENT UR		46	-1130.	6	-2388.	-1925.	$\sim$	3	$\circ$	-404-	-379.	-881.	-451.	-131.	-2041.	-4546.	-4562.	-3100.	-2558.	-1986-	-543.	26.	-128.	1090.	2979.	3896.	4769.	5911.	5603.	3791.	1780.	-328.	-1992.
L ALFS	BENDING .3R		810.	83.	-588.	44.	516.	763.	981.	1181.	1437.	1751.	1615.	1073.	•906	1063.	937.	682.	459.	-0-	-377.	-159.	360.	888.	1441.	1841.	2101.	37	2343.	92	1692.	1685.		9
UMEC#K = 604.1 RHU100 = 0.2198	BLAUE NURMAL		œ	1632.	99	1489.	2239.	2659.	3241.	3867.	3942.	4100.	4671.	4237.	2816.	2763.	4062.	4012.	2486.	1606.	1379.	1008.	1448.	2858.	3666.	3716.	4117.	53	4175.	3625.	3562.	40	3605.	40
PLINI 14 107.0 UME 0.299 RHU	UPPER RUTGR •18		m	-1320.	-1480.	764	472.	1341.	30	3481.	.1162	4	37	823	920.	1702.	4685.	3742.	472.	-538	•	0	•	3	2035.	1795.	2714.	2790.	1711.	1414.	1770.	1906	2060	1730.
PUN 23 VKTS = V/OR =		S	C	.2	2.5	3.7	5.0	6.2	7.5	9.7	0.0	2.10	12.5	7.7	35.0	46.2	57.5	168.7	80.0	91.2	202.50	13.7	25.0	36.2	47.5	58.7	70.0	81.2	92.5	03.7	15.0	26.2	37.5	48.7

RUN 23 VKTS = V/OR =	107.0 107.0 0.299	<b>.</b>	UMEG#R = RHU100 =	604.1	ALFS+C CP/S =	8.4 8. = 0.004506		CLR/S, K :	=0.11709 =0.01566	CMY/S,R = 0.2056 CMX/S,R =-0.0071
	LOWER	ROTOR	BLADE	: NORMAL	BENDING 23R	MUMENT .6R	LR EDGE	EDGEWISE DING . IR	LR PITCH	I Q
per		:		ı	: }	•	• • • • •			•
000		3556.		Φ	1379.	- 786.	•	.2055.	ĭ	80.
88.7		•		43	20	-430	•	3806	-31	19.
77.5	. : 🔻	5			1552.	-116.	1	-6798.	-424	54.
266.25	. •	3393.	24	S	1824.	-11.	•	-9135.	-23	32.
55.0	•	3815.	ᢐ	.197.	2056.	21.	•	-9784.	-152	52.
43.7	,	3619.	0	.600	1952.	6	7	10311.	-106	.90
32.5	. •		S	3	ø	-127.	7-	.11670.	27	.90
21.2	•	2034.	ው	155.	1239.	-363.	1-	-12314.	~	32.
10.0	•	2221.	•	.56.	874.	-665.	1-	1127.		11.
98.7	•	2268.	Ð	.47.	573.	-961.	•	-9328.	~	87.
87.5		342.		.260	200	-1013.	•	-8188-	17	78.
76.2	ĭ	-1817		111.	-360.	-795.	1	-7229.	<b>J</b>	92.
65.0	ï	2461.		97.	-733.	-617.	•	.5671.	•	20.
53.7	7	1268.		715.	-446.	-530.	1	-3933.	-1	58.
42.5	•	-509.	~	O.	370.	-317.	•	.3013.	91	61.
31.2		817.	10	37.	1206.	-55.	•	-3228.	24	240.
0.	•	2889.	22	:23.	1859.	124.	1	-3783.	51	194.
08.7	•	3574.	32	.29.	2495.	400	1	-3691.	-	178.
.5	. •	3495.	36	.17.	3192.	766.	1	-3339.	3(	300.
?	•	46.94	41	.65.	3688.	937.	1	-4013.	15	314.
0	••	5382.	14	.11.	3749.	971.	•	-5630.	2!	254.
	,	3945.	77	.20.	3560.	1059.	1	-5981.	3(	•60
5	•	3198.	31	.90	3382.	968	•	-4553.	21	67.
• 2	•	4464.	33	.091	3170.	521.	1	-3053	-15	25.
0	J	9	1+	~	2864.	37.	•	-2399.	•	25.
	•	4	35	.269	2464.	-223.	•	-1630.	2.5	51.
.5	•	0	24	~	1721.	-353.		-149.	71-	121.
56.2	•	-373.	11		528.	-401.		1396.	-4	57.
45.0	ĭ	4	7-			-323.		6	-29	94.
. 7	1	36	<b>71-</b>	-	-724.	- 588 -		1749.	-36	61.
72.5	•	5 7	1.5		-92•	-527.		<b>.</b> 58.	?9-	627.
11.2	•	~	14	$\sim$	862.	-818-	•	-1137.	[f-	72.

CMY/S,R = 0.0939 CMX/S,R =-0.0060	•6R	CDS SIN	-1463.2	741.3 -2374.4	-2		-292.9 -61.4	371.4 -302.1		-99.5 -48.7																			
R =0.08479 R =0.00627	BENDING MUMENT . 3R	ZIS		-587.7	-275.9	63.6	10.3	30.4	-124.7	-27.6	1.4	8.6-	7.4			STRESS						-1.3					1.5		
CLR/S, R COR/S, R		cns	- 761.7	-27.5	-348.7	-27.5	100.3	-105.3	-15.2	35.2	11.5	-1.7	-1.2		UPPER	SHAFI	<b>COS</b>		5546.7	-3597.3	-411.9	298.3	-188.9	107.2	0.46-	-106.7	33.0	17.7	-30.2
= 3.1 0.002807	BLADE NURMAL	SIN		-506.7	-497.1	123.5	45.0	4.16	-291.3	77.6	23.1	13.1	-18.1		$\overline{}$					235.1	6.44	47.6	-20.1	-24.1	8.89	0.99	20.9	-26.7	-10.7
ALFS,C CP/S =	UPPER RUTUK .2R	\$00	691.3	-238.7	-384.8	-62.1	194.1	-326.9	1.3	40.4	-22.2	112.7	-29.6		UPPER KOTOR	PITCH LINK	cos		-592.3	9.5	-31.8	-44.1	-48.4	49.6	49.8	29.3	1.95	6.9	-11.6
3#R = 607.3 100 = 0.2194		SIN				1.99	-29.4	304.7	-404.6	153.6	83.8	-88.3	-1.3		EDGE	DMENT . LR	SIN			0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
PGINT 15 1UT-8 UNEG#R 0.299 RHUIO0	81.	500	->333 B	-707-	-561.9	-37.6	272.6	-526.5	-138.5	207.9	-59.9	242.8	1.46-		UPPER RUTUR	9	SOO		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
FUN 23 VKTS = V/OR =			HARMONIC	> ~	. ~	, (**	• •	, rv	•	. ~	• •	6	01	18	84			HARMONIC	0		2	· (C)	•	· 10	. 9		ေတ	6	10

= 0.0939	α •	NIS			384.6	0•9	18.4	-18.5	22.1	-54.8	-13.4	5.2	3.5	<b>4.9</b> -																
CMY/ S.R.		cos		-316.3	130.1	-233.6	49.1	-51.6	49.5	7.6	-35.9	7.0	8.5	9.0-																
=0.08479	MUMENT	NIS .			343.8	68.1	-126.2	9.6	-26.4	126.6	-33.4	9.1	-3.6	1.3																
CLR/S, R CDR/S, R	. BENDING MOMENT	cos		-309.7	-43.2	-492.4	3.1	101.4	-127.7	6.6	38.1	13.6	-4.5	-12.3																
= 3.1 0.002807	BLADE NURMAL	NIS			55.6	1.061					0.06-	-34.9	-1.9	44.3		KOTOR	. O.A.D		:		73.5	12.5	-37.1	6.0-	3.6	8.0	1.1	15.6	-15.2	-11.2
ALFS,C CP/S =	LOWER RUTOR	CGS		-661.4			•					80.	-1.1	24.3		LUWFR KO	DITCH INK	COS	)	-153.8	-162.1	26.1		-4.2	5.8	38.4	21.3	2.9		
DNEG*R = 607.3 RHU100 = 0.2194	31	NIS		<b>.</b>	-355.	220.	-453.	69		430.		-88		106.		ROTOR FOGEWISE	C. C	SIA	•	<b>ا</b>	.3 -376.1	-515-	-16.	-31.	-26.	-116.	-439.	1	ċ	•
POINT 15 107.8 0.299		SUO		-1933.	-571.	-747.5	-12.	239.	-427.	-175-	385.	1.	-3.	-11-		LUMERR	_	COS	)	-4365	1732.	497.	44.	-609-	65.	-59.	355.	-57-	-35.	-11-
RUN 23 VKTS = V/OR =			HARMUNIC	0		2	m	4	2	•	7	æ	6	10	18	35			HAP MONTC	0	-	2	3	4	ď	9	_	<b>c</b> c	0	01

KUN 23 VKTS = V/CP =	107.8 0.299	15 UMEG#K RHULCO	6+K HCO H	607.3 0.2194		ALFS,C = CP/S = 0.00	3.1	CLR/S, R COR/S, R	=0.08479 =0.00627	CMY/S,	S*R = 0.0939 S*R =-0.0060	<i>ن</i> ئ
	UPPER F	KU1 UR 1	BLADE NU	NURMAL 28	BENDING	MCMENT	UR E	UR EDGEWISE BENDING . LR	UR PITCH	_	UPPER RUTUR SHAFT STRESS	ጃ ላ
U	•	<b>.</b>		<b>:</b>		•					,	•
, 0	-37	~	- 1	4	-1142.	-1661-		• •	-53	.7.	1508	•
1.2	-39	74		·	415	227		· •	4	O	0	
2.5	96-	154.	-5	· O	458	16		0	-533		40	•
3.7	-34	.05	-22	28.	0	-3229.		•	-548	.84	2066	•
5.0	-32	.46.	Ĩ	81.	-1276.	-2926-		<b>.</b>	-353	.3.	2191	•
6.2	-36	51.	4-		-1433.	-2263.		•	-108	.8	9102	•
7.5	-37	. 42.	-7.		an	-2012.		ં	-11		2435	•
8.7	-28	392.	-3	85.	-1305.	-2638.		•	46-	41.	3753	
0.0	<b>51</b> -	.71.	4	74.	-888-	-3561.		<b>.</b>	-530	.0	5134	•
01.2	<u> </u>	191.	11	97.	-632.	-3906 -		°°	-560		6058	•
12.5	<u> </u>	.661	17	75.	-739.	-3445.		•	-614	.6,	7102	•
23.7	-11	186.	Ś		-1045	-2514.		•°	-31	.0	8376	•
35.0	-29	63.	7		-1184.	-2065.		•	-340	•	9668	•
46.2	-20	.110	÷		-1041-	-2937.		•	-45	.7.	8463	•
57.5	۲- ۲-	191.	11		-848-	-4238		• •	-548	.8	1191.	
68.7	7	126.	13	15.	-803.	-4338.		•	-624	. 4.	7661	•
80.0	-21	.00	9	75.	-886-	-3501.		•	-639	.61	8130	•
91.2	-25	.069	~	99.	-1032.	-2844.		•	-650	.0	8834	•
02.5	-28	167.	·	36.	-1115.	-2130.		•0	-707-	.7.	9152.	•
13.7	-33	.601	Ī	85.	-995-	-1110-		•	-738	. 8	8866	•
25.0	-28	111.	<u>-</u>	82.	-713.	-417.		•	-712	.2.	8388	•
36.2	61-	.650	7	72.	-423.	116.		·	91-	.2.	1933	•
47.5	PT-	197.	0	83.	-146.	1005.		•	185	.10	7379	•
58.7	-11	.80.	71	72.	133.	1650.		0.	-112	72.	6903	•
70.0	11-	.82.	16	80.	318.	1768.		•	-672	72.	n	•
81.2	-13	157.	18	.90	350.	2057.		°	-809	.61	58	•
92.5	-20	.88	14.	29.	261.	2321.		o	16-	.4.	96	•
03.7	-20	124.	11	59.	52	1766.		o	-71		6625	_•
15.0	91-	.44.	11,	29.	-229.	0		•	-586	16.	55	_•
26.2	-20	177.	80	77.	5	123.		•	61-	96.	92	.•
3	-29	.2911.	•	28.	-612.	3		•	96-	3.		
8.7	-34	18.	~	102.	-823.	-1072.		°	61-		40	•

KUN 23 VKTS = V/CR =	107.8 3.299	ZANO SHO	OMEG#R = RHU100 =	607.3		ALFS.C = CP/S = 0.00	3.1	CLR/5, R CDR/5, R	=0.08479	CMY/S,R = 0.0939 CMX/S,R =-0.0060
	LUNER	ROTOR	BLADE	E NGRMAL	BENDING	S MOMENT	LR E	LR EDGEWISE BENDING . 1R	LR PITCH	Į.
v		4	•	J	<u> </u>	Š				c C
00.0	7	917.		.10.	-519.	-486.		-2456.	-2	.94•
88.7	-2		-10	126.	4			-3446	-3	326.
77.5	7-	908		188.	-414-	-428.		-4624.	-3	132.
.2		•	•	-69-	-65.	-599.		-4941.	£-3	118.
55.0		383.	9	112.	63.	-630.		-4798.	7-	-229.
43.7	1-	324.	~	151.	-151-	-492.		-5167.	1-	-119.
32.5	-2	118.	-1	136.	-535.	-428.		-5938.	í	.74.
21.2	1-	768.	-10	134.	-774.	-551.		-6159.	•	.58.
10.0	1	837.	9	.191	-664.	-751.		-5607.	•	.19.
98.7	'	455.	7-	164.	-401.	-893.		-5356.		37.
87.5	1-	112.	7-	. 80.	-397.	-887.		-5843.		73.
76.2	7-	161	-1	768.	-651.	-732.		-6238.		41.
65.0	7-	718.	-12	:61.	-840•	-531.		-5739.	•	.16.
53.7	-2	859.	-	335.	-758.	-345.		-4863.		-6-
42.5	7-	983.	-12	.69:	-462.	S		-4761.		3.
31.2	-2	523.	_	113.	-115.	5.		-5529.	1	45.
20.0	-1	_	4-	122.	194.	91.		-5960	1	-43.
08.7	1-	013.	_	.901	495.	150.		-5357.		3.
7.5	•	.896	M	315.	735.	225.		-4104-	i	-09-
6.2	-1	380.	E.	331.	745.	275.		-5013.	1-	-153.
5.0	7-	517.	~	121.	527.	261.		-5536.	1-	-118.
3.7	-1	. 566		:65.	263.	204.		-5042.	1	-84•
2.5	-2		-5	562.	5.	132.		-3850.	7-	-171.
1.2	-2	758.		373.	-263-	<b>*</b> 0 <b>*</b>		-3198.	-5	.69.
0.0	£-	.695		:84∙	-478.	-66-		-3353.	£-	314.
8.7	۳-	-662	~	131.	-604-	-592-		-3412.	£-	316.
7.5	<u>.                                    </u>	083.	_	_	-135.	-371.		-2039.	-2	.52.
56.2	£-3	355.	-13	S	-857.	-397.		-1541-	7-	.21.
45.0	-3	345.	_	0	-878-	-425.		-1325.	-3	317.
•	-2	2553.		327.	9	-200•		-2130.	۴-	175.
22.5	17	. 499	9	~	Š	-579.		~	-2	.97.
11.2	7	- 3		. 24:	-433.	-588.		-2481.		.49•

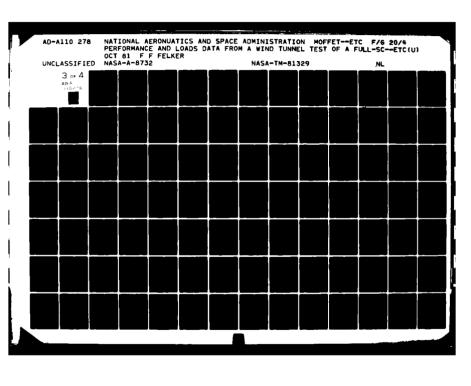
CAY/S,R = 0.0933 CAX/S,R =-0.0060	.68 SIN -1860.7 1833.9 -2635.0 -2262.9 -495.5 514.3 -264.9 102.2 268.9 -186.7 -32.4 5.0 -147.0 51.3 -34.6 66.5 -92.2
CHX CMX	1860. 1833. -2262. -2262. -264. -186. -186.
=0.07811 =0.00711	BENDING MLMENT  - 3R  - 50  - 692.7  - 71.5  - 692.7  - 77.9  - 100.1  - 71.5  - 50.4  55.6  - 242.4  - 100.1  - 71.5  - 50.4  - 55.6  - 242.4  - 100.1  - 100.1  - 100.1  - 100.1  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.2  - 100.3  - 1
CLR/S,R CDR/S,R	
2.8	R BLADE NGRMAL S IN 81.0 -855.6 -855.6 -300.1 63.3 -21.1 8.1 RUTOR NK LUAD S IN 198.8 116.2 -8.9 53.4 -37.0 86.0 86.0 86.0 87.0 8
ALFSIC CP/S =	UPPER RCTCR E COS . 2R COS . 3 -109.3 -1442.8 -170.9 -170.9 -277.5 50.3 -277.5 50.3 -27.5 -29.8 -29.2 -29.8 -29.2 -29.8 -27.5 -29.8 -27.5 -29.8 -29.8 -27.5 -29.8 -29.8 -27.5 -29.8 -27.5 -29.8 -27.5 -29.8 -29.8 -29.8 -29.8 -27.5 -29.8 -29.8 -29.8 -29.8 -29.8 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -29.8 -45.0 -45.0 -20.3 -20.3 -20.3 -20.3 -20.3 -20.3 -20.3 -20.3 -20.3 -20.5 -20.3 -20.5
OMEG*R = 607.3 RHU133 = 0.2176	SIN 778.9 188.5 183.1 863.4 39.4 182.8 6.7 31.5 31.5 0.0 0.0 0.0 0.0 0.0 0.0 0.0
PUINT 16 142.6 OME 0.396 RHU	-3080.6 -3080.6 -2130.1 -318.7 -177.2 -177.2 -177.2 -177.2 -23.6 -105.2 -105.2 -08.9 -0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.
FUN 23 VKTS = V/PR =	HARMONIC 10 10 10 10 10 10

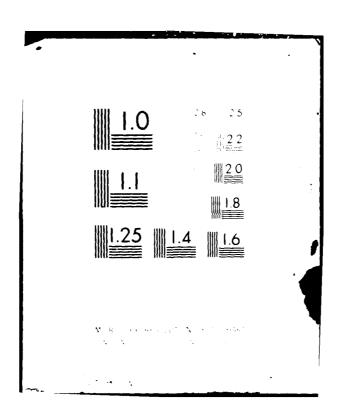
CMY/S,R = 0.0933 CMX/S,R =-0.0060	-386.8 501.7 -502.1 -84.7 79.6 -106.0 59.6 -106.0 59.6 -106.0 -25.7 17.5 -45.0 -0.1 33.7 15.6 6.5 -6.4
=0.07811 =0.00711	BENDING MUMENT  3R  COS  SIN  673.9  30.1  497.9  -46.2  -46.2  -120.7  28.1  144.3  125.2  -28.9  -18.4  11.2  11.2  17.4  -2.9  -11.3  -4.3
CLR/S, R CDR/S, R	1 1
2.8	R BLADE NURMAL R SIN -81.8 278.2 -237.4 368.7 -368.7 -36.9 343.1 -72.7 -27.9 33.3 60.2 -0.3 -0.3 -1.5 -1.5 -1.5 -1.5
ALFS,C CP/S =	COS -2R COS -2R COS -2R COS -2R -291.4 -1937.2 -159.2 -159.2 -159.0 -154.0 -15.7 -15
*K = 607.3	SIN 1744.2 123.8 452.7 587.6 587.6 136.6 136.6 124.6 124.6 120.5 100.5 1
PUINT 16 142.6 UMEG*R 0.396 RHUIOO	COS -1R -2670-3 -7210-9 -7256-
RUN 23 P 1 VKTS = 1 V/CR = 0	HARMUNIC 199 109 109 109

CMY/S,R = 0.0933 CMX/S,R =-0.0060	UPPER KUTUK SHAFT STRESS		31		86	49	60	•	2830.	4490	6170.	7236.	8430	9578.	9419.	8086.	•6669	.4069	7651.	8572.	8815.	8308•	7502.	6455.	5590.	5708.	6349.	6452.	6105.	5555	4428	3177.	2734.	12
=0.07611 CMY/ =0.00711 CMX/	UR PITCH LINK LGAD			-346.	-405.	-694-	-389.	-505-	-1661-	-365.	-465.	-491.	-482.	-0440-	-540.	-751.	-191.	-737.	-777.	-722.	-546.	-534•	-652.	-168.	-887.	-835.	-625.	-687.	-833•	-852.	-663.	-802.	Ñ	-681.
CLR/5, K CDR/5, R	UR EDGEWISE BENDING • IR		ဝံ	ი	•	•	•	ं	•	ċ	•	• •	ં	•	ं	ं	ċ	•	•	•	ċ	ò	•	·°	·	•	°	ċ	•	•	ô	o	•	•0
S <sub>3</sub> C = 2.8 S = 0.002998	MUMENT U		-1208.	-1997.	38	-5909-	80	-3743.	-2736.	-2346.	-2679.	-2643.	214	210	-3403.	-5173.	-7443.	-7317.	-6183.	-4849.	-3538.	-2711.	-2132.	-901.	816.	2364.	3665.	4210.	3482.	17	895.	Ð	~	-898-
607.3 ALF	NURMAL BENDING		91	~	-1969.	-1549	-1131.	-917.	-722.	-418.	-196•	-289.	-134.	-1363.	-1812.	-1860.	-1804.	-2112.	-2770.	-3309.	-3326.	-2766.	-1888.	-1100.	2	-65.	~	S	G	215.	• 4-	-325-		-11511-
UMEG*K = 6 RHU100 = 0.	BLADE		601-	-148	-149	-101-	-3	11	. 792.	95	~	19	117	6-	-75	-41	-2	-59	-187		-336	-280	-151	-29	45	92	116	119	135	15	140	66	46	-31
PLINT 16 142.0 0.396 H	UPPER ROTOR		5375	-5454	513	-4085	ഴ	60	-1454.	9	മ	563.	101	2840	3056	2932	1775	3332	5713	-7492.	1944	5650	7064	337	2596	217	9112	214	3	6	86	2	3052	٠
RUN 23 VKTS = V/CR =		S	0	1.2	2.5	3.7	5.0	6.2	.5	8.7	0.0	01.2	12.5	23.7	35.0	46.2	57.5	168.7	PO.09	191.25	02.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	95.5	03.7	15.0	26.2	37.5	48.7

L CMY/S,R = 0.0933 L CMX/S,R =-0.0060	PITCH		-270.	-324.	-372.	-264.	-130.	-67.	-24.	• 9	20•	50.	76.	75.	49.	-4-	-33.	-18.	-62.	-184.		-323.	-367.	-327.	-260.	-276.	-269.	-200.	-239.	-346.	-552.	-344.	Ø	-345.
=0.07811 =0.00711	LR PI																																	
CLR/S, R CDK/S, R	LR EUGEWISE RENDING JR		-2773.	665	-5814.	-5771.	-5307.	-5652	S	-6418.	-5119.	-4436.	-4904.	-5115-	-4135	-3179.	-3820.	-5267.	-5903	· 🔿	-5795.	-6630.	-7073.	-6148.	-4262.	-2923•	ð	-2345.	-988.	196.	-414-	-2045-	-2638.	-7506.
2.8 = 0.002998	MOMENT LI		-574.	30	-253.	7	-498*	-497.	æ	-1028.	-1310.	-1451.	-1381.	-1077.	-715.	-447.	-219.	24.	220.	364.	525.	655.	.919	407.	155.	-103.	-377.	- 508.	-470.	9	-567.	-621.	-651.	-691.
3 ALFS.C	BENDING M	<u>.</u>	-124.	-17.	245.	468.	352.	-162.	-877.		1468.				2243.	1787.		-241.	433.	993.	1365.	1331.	904.	385.	-86.	-610.	-1185.	-1677.	-2032.	-2259.	-2244.	-1733.	Ġ.	-356.
*R = 607.3 00 = 0.2176	LADE NORMAL	<u>.</u>	174.	~	-149.	875.	1229.	115.	6	207.	1145.	1242.	1763.	2793.	3509.	3114.	•	114	$\sim$	•	0	196.	2	~	O	~	2006.	2475.	330.	4004	3785.	2830.	1 7	-514.
16 OMEG*R RHJ100	ROTOR BL	•	23	87	20	•	1 4	11	197	1+1	1555	7967	3340	5283	67.09	4664	.5023.	5454	1123	70	25	Δ	9	5,7	70	7 +	9	29	90	7	43	56	Φ	3.
PLINT 142.6 0.396	LGNER		•	1	•			1	1	1	,	ĺ	١	1	ĩ	i	ľ	ľ	1	•	•	ı	1	ĺ	Ì	1	ĺ	Í	Ĭ	•	1	Ĭ	ľ	•
RUN 23 VKTS = V/OR =		S	00.00	88.7	77.5	66.2	55.0	43.7	32.5	21.2	10.0	98.7	87.5	76.2	45.0	153.7	142.50	131.2	20.0	7.80	7.5	6.2	5.0	3.7	2.5	1.2	0.0	8.7	5	56.2	45.0		22.5	11.2

CMY/S,K = 0.1176 CMX/S,K =-0.0070	-08 SIN -784.7 -784.7 1277.4 -635.2 -2110.9 -314.9 277.6 57.8 380.2 1084.8 221.2 -470.6 144.5 325.0 -158.2 -15.1 -16.1 -55.0 144.6 -55.0	
=0.10987 C		22.0
CLR/S,K COR/S,R	259.0 147.9 147.9 119.8 119.8 119.8 19.9 19.9 19.0 19.0 19.0 19.0 19.0 19.0	26.5
2.9 3.034461	R BLADE NORMAL R SIN 3465.1 -934.2 -698.4 -893.3 -365.0 -18.0 -27.8 -20.4 -236.0 -236.0 -32.3 -36.9 -32.3 -55.6 -61.5	22.0
ALFS.C CP/S =	UPPER RUTUR B  2047.4 -142.8 -1308.8 -1308.8 -229.4 -229.4 -247.3 -24.9 -247.3 -24.9 -36.0 -24.9 -36.0 -24.9 -15.5 -10.9 -12.4 -12.4 -12.4 -12.4 -12.4 -12.4 -12.4	42.3
0.456*R = 604.7 RHU100 = 0.2157	** SIN SIN ***	000
PUINT 17 143.0 04E 0.599 RHU	CLS	
FIIN 23 VKTS = V/OR =	HARMONIC 100 100 100 100 100 100 100 10	<b>~</b>





= 0.1176 =-0.0070	210.2 210.2 210.2 7.44.2 -144.2 -144.2 -15.9 15.9
CMY/S, R CMX/S, R	165.7 -165.7 -226.6 -527.1 84.5 -33.6 -33.6 -33.6 -33.6 -33.6
=0.10987 =0.00754	MUMENT R SIN SIN 295.4 -133.8 219.9 33.1 -13.5 -12.1 -12.3
CLR/S, R CDR/S, R	AL BENDING .3R .3R .989.1 122.5 -1575.0 -67.4 -93.2 12.8 8.3 8.3 21.9 1.9
2.9	SIN SIN SIN 569.7 249.1 562.7 444.7 -57.5 -40.8 61.1 50.4 50.4 51.1 50.4 51.1 51.
ALFS,C CP/S =	LOWER ROTOR BLAI COS SIR 1242.6 -197.8 -2886.9 -2010.7 -249 -214.4 -249 -152.5 562 -152.5 562 -152.9 -43 -178.8 61 11.5 50 -178.8 61 11.5 50 -178.8 61 -178.8 61
UMEG*K = 604.7 RHULOO = 0.2157	840 964 997 9 8 8 8 8 9 8 9 9 9 9 9 9 9 9 9 9 9
PUINT 17 143.0 UME 0.399 RHC	680-1 -224-3 -4740-3 -224-3 -4740-3 -2754-3 -4740-3 -2754-3 -487-6 -268-3 -487-6 -19.5 -90-7 -268-3 -90-7 -268-3 -487-6 -19.5 -178-7 -441-4 -206-7 -106.8 88-7 -472-8-2 -178-7 -472-8-2 -178-7 -472-9 -106.8 827-7 -472-9 -106.8 88-7 -472-9 -106.8 81-7 -472-9 -106.9 -1153-7 -473-9 -73-4 -25-7 -73-4 -25-7
RUN 23 VKTS = V/CR =	193 HARMONIC 1 198 8 4 5 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6

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	PCINT	11						,		
VKTS =	143.0	OALC#R	11	604.7 ALF	ALFS,C =	2.9 CLR/5,R		CMY/S, K	11	
œ	0.399	RHOL	O H		S = 0.004461		11	S / X & Z	'n	
	UPPER		ADE		BENDING MCMENT	UR EDĞEMISE	UR PI		UPPER KUTUR	
		• 1R	•2R	•3R	• <b>6</b> K	BENDING . IR	LINK	LUAD		
S										
Ċ	£-	N	218.	-703.	-260.	• •	7	459.	2318.	
1.2	-2	3	229.		0	•0	1	384.	2523•	
5	1		-	-104-		0			3017.	
	• ~-	0	2309-	840.	-877.		' 'i		3440-	
- C	4 11	, ת ט	200	1750	- 1480		Ī		3586.	
	יא ני		5312	2203	-1251-		ī	197	3701.	
	י ער		5786.	2664	•		•	777.	4576	
	· •	9	6149	3139	473		1	553	6423	
	) <b>^</b>	20	7013	3480.	207		ļ	320-	R742	
2.0	- 10	- 1	7373.	3423	496		•	505	9538	
12.5	•	10	6398	2996	1142.		'	528.	10801	
23.7	45	77	5061.	2342	721.		•	426.	11632	
35.0	•	35	4575.	1789.	-1180	•	•	537.	11116	
46.2	S	90	4752.	3	-3656	•	•	312.	9739.	
57.5	4	အ	4591.	1358.	-5337.	•		929.	8666.	
68.7	2	20	3399.	538.	-5368.	•		-857.	8372.	
80.0	7-	24	1304.	-660.	-4085.	•0		719.	8838	
91.2	4-	54	-805-	-1649.	-2598.	•0		571.	9435.	
02.5	91	m	-1940.	-2154.	-1910.	• 5	ļ	535.	9230	
13.7	-5	•	-1855.	-2121.	-2132.	•0	ĩ	638.	8217.	
25.0	4-	~	113	-1685.	-2264.	•	ï	-703.	7223.	
36.2	4-	0	-524.	-1245.	-1523.	•0	ï	723.	6284.	
47.5	-3	6	-237.	-1026.	-282.	•	ĩ	833.	5492.	
58.7	-3		-151-	-877.	1160.	•0	ĩ	-892.	5315.	
70.0	<b>7</b> -	$\sim$	-256.	-673.	2755.	•0	ï	778.	5473.	
81.2	4-	à	-331.	-468	3486.	•0	ī	-746.	5315.	
92.5	-3	712.	-26.	-447.	2679.	•0	Ĭ	.905	4782.	
03.7	-2	•	443.	-497.	1365.	•0	ĭ	949.	3856.	
15.0	7-	0	625.	-200•	0	•	ī	793.	2662.	
26.2	-2	Ø	711.	-390•	-	•	1	718.	2014.	
337.50	-20	30	874.	-351.	44	•	ï	757.	2177.	
48.7	-2	0	688.	-515-	7	•0	ì	662.	2363.	

KUN 23 VKTS = V/OR =	143.0 0.399	ONEG*R RH0100	= 604.7 = 0.2157	1.1	ALFS,C CP/S =	C = 2.9 = 0.004461	2.9	CLK/S,R CDR/S,R	=0.10987 =0.00754	CMY/S,R = 0.1176 CMX/S,R =-0.0070
	LUWER ROT	OR BL	ADE NORMAL		DING	MUMENT .68	LR EDGE	LR EDGEWISE Bending .1R	LR PITCH LINK LUAD	- Q
10		•		•	:	:		•		ŀ
000	ľ	•	3	327	7.	-265.		-3136.	-16	64.
88.7	N		5029.	345	a	136.		Š	-2	29.
77.5	9			365		316.		-6171.	-36	81.
~	-		5826.	3948	<b>.</b>	213.		-6672.	-244	44.
55.0	9	•	3	398	2.	141.		-6776.	7	-15.
43.7	~	•	N	348	.2.	96.		-7251.	•	55.
32.5	•	•	O.	260	1.	-164.		-8180.	•	52.
21.2	•	•	ഗ	186	3.	- 594 •		-8332	~	81.
10.0	~	•	~	1440	• •	-957.		-7206-	7	113.
98.7	•	•	-	89	899.	-1137.		-6375.	7	113.
87.5	4	5.	892.	-2	-28.	-1096.		-6631.	7	119.
76.2	•	•	σ	-98	986.	-856.		-6311.	7	148.
65.0	490	•	~	-141	478.	-582.		-4551.	` <b>~</b>	104.
53.7	442	•		-137	370.	-415.		-3143.	_	16.
42.5	329	•	1767.	-87	5.	-287.		-3458	•	63.
31.2	254	•		-291	1.	-100-		-4344.	77	23.
20.0	178	•	4	23	31.	97.		-4281.	7	-48•
08.7	112		161	19	677.	265.		-3580.	77-	246.
5	ω		529.	100	.600	467.		-3498	-267	57.
2.	194		384.	113	. 6.	<b>.049</b>		-4252.	-3(	300.
0	170	3.	219.	100	.002	616.		-4780.	-3(	.309.
1	135		218.	67	•	435.		-4186.	-17	127.
Š	200		-42.	35	52.	262.		-2793.	ĩ	-80•
.2	257	•	S	14	.2.	45.		-1705.	-5	45.
0	183	•	5	-64	4.	-256.		-1440.	-131	31.
٠,	168	•	-438-	-31	15.	-403		-1129.	1(	104.
5	330	•	φ	64-	.6	-310.		•66	-121	21.
56.2	398	1	15	-57	73.	-228.		1153.	644-	•6•
45.0	243	•	12	-41	7.	-260.		414.	-363	63.
33.7	O	•		3	.2.	-295-		-1300	-28	286.
•	3198	8•	1982.	9	41.	-372.		90	4-	51.
11.2	0	•		278	.7.	-453.		-5169.	-3	•06

0.1337 -0.0059	21N 2047 - 206 - 3 - 206 - 3 - 206 - 3 - 206 - 3 - 114 - 5 - 114 - 5 - 206 - 3 - 207 - 3 -
CAY/S, K = 0 CAX/S, R =-0	Cus -1339.5 1479.2 1479.2 1479.2 468.1 152.3 152.3 -175.0 -175.0 -175.0 -175.0
=0.09291 =0.00717	SR SIN 507.4 -396.3 -69.4 -273.7 133.5 -172.8 -172.8 -173.8 -
CLR/5, R CDR/5, R	BENDING CCC
2.9 0.003489	R BLADE NCRMAL SIN -510 -756.9 -756.9 -756.9 -611.5 320.1 -60.5 18.7 9.5 9.6 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5 9.5
ALFS.C CP/S =	UPPER RCTGR E CCS .2R CCS .2R CCS .2R 2974.9 18 -1391.6 -176.8 -176.8 -176.9 -176.9 -176.9 -176.9 -176.9 -18.6 -13.0 19.6 31.2 29.4 29.4
UMEG*R = 605.4 RHU100 = 0.2149	R SIN 3354.7 -1045.6 -972.8 -972.8 -488.9 -488.9 -488.9 -488.9 -488.9 -488.9 -488.9 -75.0 146.9 137.6 28.7 28.7 28.7 28.7 0.0 0.0 0.0 0.0 0.0
PCINT 18 143.2 UM 0.399 RHK	CUS .1R
RUN 23 VKTS = V/CR =	HARMONIC 10 10 10 10 10 10 10 10 10 10 10 10 10

= 0.1037	x Sin		408.6	70.3	-101-0	-56.4	-15.4	8.6	28.6	-2.3															
CMY/S,R =	. 6k	-290.4	230.8 -523.8	84.0	64.4	23.9	-31.1	-1.5	29.3	4.5															
=0.09291	MOMENT S SIN		-298.6	-127.3	161.1	189.3	-19.7	5.9	<b>2.</b> 9	-5.5															
CLR/S, R COR/S, R	BENDING • 3R COS	32.1	181.4-1576.3	-55.4	-33.8	-38.2	75.3	12.6	18.8	-8.5															
2.9	BLADE NORMAL SIN		050.0 349.6	257.9	403.0	406.4	-2.9	-28.8	•	51.4	POTOR	LUAD				0.2	53.2	44.7	1.6	8•3	21.7	1.4-	-8.0	19.1	8.1
ALFS,C CP/S =	LOWER RUTOR .2R COS	-167.4	-61.1 -1-2041.9	- 186.9 -	-141.5	-26.1	223.4	25.	-158.3	-18.9	Ja auno i	PITCH LINK	COS	;	-157.9	-192.5	75.8	12.3	-41.8	-13.4	35.5	-5.6	-12.3	-35.8	-15.0
OMEG*R = 605.4 RHG100 = 0.2149	LO SIN		,		554.3	563.7	286.4	-107.3	4	55.1	7000	<u>;</u>	SIN						-12.0		4.2				
PCINI 18 143.2 DM 0.359 RH	• soo	-1315.3	-255.6	•	1-575-	7-808-				-101-		BEND ING	0.05		-4103.6	2037.7	1624.0	298.1	6.2	33.4	21.4	2.618	-56.2	80.4	4.3
FUN 23 VKTS = V/OR =		HAPMONIC 3	- ~	, w	41	Λ <b>«</b>	, <b>~</b>	nc	6	10	19	<b>3</b> 7		HAR YUN IC	c		۲,		4	<b>ب</b>	4	•	ю	5	10

Marie Commence

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CAY/S, K = 0.1037 CMX/S, K =-0.0059	UPPER RUTUK SHAFT STRESS		5128				4066.		5202.				10808		11055.	9468.	8315.	8077.	8453	8745.	8269.	7265.	6254.	5174.	4433	4689*	5198.	4985.	46	3901.	293	16	3	2
=0.69291 =0.00717	UK PITCH LINK LUAD		-441.	-384.	-0440.	-415.	-263.	-198	-297.	-386-	-435.	-200	-491.	-419.	-149-	-845.	-865.	-825.	-780-	-634.	-543.	-635.	-737.	-811.	-868-	-839.	-116.	2	~	-853.		~	9	-673.
.9 CLK/S, K 89 CDK/S, A	UR EUGEWISE BENDING - 1R		•	•	• •	•	•	•	•	•	၁	<b>•</b>	•	ċ	•	ċ	•0	0	•	•	•	•	•0	•0	•	•	•	•	•0	•	•0	•0	•	-0
fs.t = 2.9 /s = 0.003489	G MOMENT		-903•	134	151	199	-2702.	558	119	-086-	-1275.	-046-	-465.	-955.	-2732.	-5129.	-6587.	-6172.	-4695。	-3365•	-2649.	-2422.	-2048	-666-	<b>.</b> 644	1978.	3334.	3674.	2751.	1476.	201.	-1046	6	-922
605.4 ALF	NURMAL BENDING		-1197.	-1281.	-603	-182.	447.	783.	1082.	1463.	1716.	1560.	1062.	424.	5.	S	-211.	-892	-1822.	-2486.	-2651.	-2284.	-1608.	-1052.	-737.	-465.	-225.	-139.	-165.	-226.	-323•	-1441-	-603.	-881
UMEG*R = 6 RMuloj = 0.	BLAJE	,	7	-	14	19	259	-	349	•	43	S	S	35	97	2	31,	24	55	207	584	206	110	28	Ò	9	0	24	0	58	~	87	~	_
PLINT 18 143.2 UM 0.399 RH	UPPER KOTOR	•	434	390	-2987.	2	1303.	9	3	-	3	•	2273.	-	3	1791.	3	1	9	93	894		2	3	0	4	7	3	_	-2210.	S	3		95
PUN 23 VKTS = V/CR =		S	Ç,	1.2	2.5	3.7	45.00	6.2	7.5	8.7	0.0	01.2	12.5	23.7	35.0	6.2	157.5	68.7	80.0	91.2	02.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	92.5	03.7	15.0	26.2	37.5	48.7

19:00

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	0	18							
VKTS #	143.2	DMEG*R RHO100	H 00 H	605.4 0.2149	CP/S =		CLK/S, K CDR/S, R	=0.09291 =0.00717	CMY/5,K = 0.103/ CMX/5,R =-0.0059
	LOWER R	ROTOR E	BLADE N	NORMAL	BENDING •38	MOMENT .6R	LR EDGEWISE BENDING .IR	LR PITCH Link Load	_ 9
S		•			; }	,			ļ.
000	21	N	2	•	1273.	-394.	-2882.	-22	• 7
88.7	UT	٠	72	•	1357.	-69-	-4832	-307	.7.
77.5	22	7	æ	•	1595.	-24.	-6120	-376	.6.
66.2	42	Õ	2917	.•	1833.	-183.	-5974.	-23	.0.
55.0	35	37	-	•	1729.	-236.	-5654.	-65	5.
43.7	01	27	1870	•	1148.	-275.	-6384.	91-	• 9
32.5	<b>31</b>	37	78	•	331.	-536.	-7386.	~	.1.
~		61	•	•	-244.	-911.	-7080.	4	40.
10.0	7	70	₹	•	-452.	-1197.	-5685.	m	37.
7.86	9	25	-122	•	-722.	-1339.	-5045.	B	50.
87.5	-27	m	œ	•	.1311.	-1270.	-5588.	100	.00
76.2	547-	8	-2411	•	.1859.	-974.	-5481.	116	•9
65.0	-56	44	316	•	.1953.	-652.	-3898	S	56.
153.7	-45	53	-		.1565.	-0440	-2786.	•	-6.
42.5	-33	97	_	•	-882.	-230.	-3639.	1	• 9:
131.2	-24	81	0	•	-135.	32.	-5019.	m	33.
20.0	11-	88	-168	•	503.	233.	-5167.	-78	.8.
08.7	2-	15	676	•	1028.	377.	-4674.	-22	24.
7.5	ĭ	10	1056	•	1412.	560.	-4664*	-292	.2.
6.2	-12	8	•	•	1462.	692.	-5965-	-336	.98
5.0	-12	53	513	•	1141.	618.	-6455.	-33	.99
3.7	-13	9	~	•	681.	411.	-5406.	-229	.63
2.5	-23	00	-	•	247.	210.	-3523•	-174	. 4.
1.2	-30	99	-883	•	-181-	-32.	-2412.	-231	11.
0.0	-29	8	2	<b>.</b> .	-605-	-306-	-5394.	-200	•00
8.7	-36	94	7	•	-985.	-431.	-1840	-130	.00
7.5	-54	58	30	•	-1326.	-380-	• 46-	-245	12.
56.2	-58	56	301	•	-1566.	-366.	974.	-379.	.61
45.0	74-	49	-2651	•	-1450.	-439	-43.	-35	1.
333.75	-21	. +01	14.	•	-761.	-512.	73	-34	.7.
22.5	r1)	99	0	•	262.		N		.1.
11.2	54	•	~	•	1024.	-626.	-5004•	-32	•60

= 0.1258 =-0.0126		SIN		3777.3	-1396.2	403.6	897.3	-574.9	538.1	-118.6	7	93	•															
CMY/S,R = CMX/S,R =-1	• 6K	\$00	-2473.8	7.4		_	78.8		-15.6		74.6	156.9																
=0.07855 =0.01014	MUMENT	NIS		-1537.1	-804.5	-0-1	-240.0	204.2	-266.7	-39.0	-3.8	-19.9	-21.6	ROTOR	STRESS	NIS	1		-4718.7	-199.9	-390.6	1071.7	-614.6	48.8	-477.0	-92.8	-32.0	
CLR/S, R CDR/S, R	L BENDING MÜMENT • 3R	SOO	-2095.9	1669.1	-1104.8	-41.9	176.6	-200.4	70.9	37.7	36.6	9.5	12.6			, SO3	!  - 	1482.4	-3287.6 -	-672.9	492.4	65.3	379.6	10.5	-289.0	291.6	02.2	7
= 5.3 0.002754	BLADE NORMAL	NIS		-1737.2			-536.0	352.6	-460.5	127.3	93.8	-52.3	-2.1	OTOR	K I O AD				205.9	90.5	-1.4	17.2	-22.5	59.3	80.3	51.3	•	
ALFS,C CP/S =	UPPER ROTOR	COS	-1293.5	6.		-111.6	321.1	-473.5	255.3	178.7	-80.7	-92.8	•	HPPER ROTOR	PITCH - INK	C08	1	-303.9	31.7	-0-3	-13.8	-41.9	104.2	27.1	8.1	19.2	0	١
UMEG*R = 590.9 RHU100 = 0.2204	J.	NIS	·	-1951.5	-1814.8	-61.1	-1081.7	765.0	-836.7	204.2	339.8	54.2	67.3	ROTOR FOGFWISE	MOMENT	SIN			1083.2	2074.7	141.1	23.0	-3.0	-56.4	-329.8	-47.5	48.1	
PUINT 6 140.9 UNE 3.403 RH		500	-4555.2	2478.0	-2150.1	-274.9	120.9	-706.6	162.1	485.8	-139.5		-27.5	UPPER ROTO	_	002		-4760.9	837.4	393.8	36.6	•	•	-27.5	-34.0	-106.7	34.8	
RUN 24 VKTS = V/OR =			HARMUNIC 0		7		4	5	9	7	<b>6</b> 0	6	10	20	0		HARMONIC	0		7	3	4	2	9	7	∞	o	•

-1989-1 -65.8 -1146.8 343.0 -310.7 -52.8 -2380.1 393.7 -1889.8 47.7 -673.2 -105.2 -1230.1 393.7 -1889.8 47.7 -673.2 -105.2 -125.1 -162.7 -38.6 -77.9 43.3 38.4 185.0 658.4 91.3 286.0 -12.4 -210.7 -193.9 144.0 -97.4 84.8 47.8 -14.7 -103.9 144.0 -97.4 84.8 47.8 -14.7 -103.9 144.0 -97.4 84.8 47.8 -14.7 -11.3 14.3 -100.4 0.4 0.9 1.5 5.2 -3.5 14.3 -100.4 0.9 1.5 5.2 -3.5 14.3 -200.5 2.0 10.3 -11.7 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -11.7 -200.5 2.0 10.3 -
2380.1 393.7 -1889.8 47.7 -673.2 -125.1 -162.7 -38.6 -77.9 43.3 185.0 658.4 91.3 286.0 -12.4 -193.9 144.0 -97.4 84.8 47.8 174.9 -55.0 80.2 -82.7 -19.7 -19.7 174.9 -55.0 80.2 -82.7 -19.7 -19.7 -100.4 0.4 16.4 -21.1 47.6 -9.2 103.7 -20.6 2.0 10.3 -20.2 103.7 -20.6 2.0 10.3 -45.7 -21.2 6 79.7 -20.6 2.0 10.3 -45.7 -21.2 6 79.7 -20.6 2.0 10.3 -45.7 -21.2 6 79.7 -20.6 2.0 10.3 -45.7 -20.6 2.0 10.3 -21.2 6 79.7 -20.5 -20.6 2.0 10.3 -27.9 23.8 -6.1 -27.9 23.8 -27.9 23.8
-162.7 -38.6 -77.9 43.3 -152.7 -58.6 -17.9 -12.4 -12.4 -12.4 -12.4 -12.4 -13.1 160.6 -12.5 -13.2 -82.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -19.7 -10.3
144.0
352.8 -13.1 160.6 15.5 -55.0 60.2 -82.7 -19.7 0.4 0.9 1.5 21.3 28.6 16.4 -21.1 47.6 103.7 -20.6 2.0 10.3 3 ROTUR 3 INK LOAD 5 SIN 79.7 69.6 41.5 11.0 44.4 50.7 -6.1 22.7
-55.0 80.2 -82.7 -19.7 0.4 0.9 1.5 21.3 21.3 28.6 16.4 -21.1 47.6 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3
28.6 16.4 -21.1 47.6 10.3 10.3 10.3 10.3 10.3 10.3 10.3 10.3
103.7 -20.6 2.0 10.3  ROTUR INK LOAD SIN 79.7 69.6 41.5 11.0 44.4 50.7 -6.1 23.8
LOWER ROT COS -45.7 212.6 59.2 19.3 1.7 1.7 3.4 -50.5
17CH LINK COS -45.7 212.6 59.2 19.3 -8.3 1.7 1.7 3.4 -50.5
212.6 212.6 212.6 19.3 19.3 19.7 19.7 19.7 19.7
212.6 212.6 59.2 19.3 18.3 1.7 20.5 88.2
212.6 59.2 19.3 19.3 1.7 1.7 50.5
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18.3 18.3 20.5 8.2 8.2 8.2
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1.7 3.4 50.5 27.9 88.2
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Black Commence

VVOR = 140.9 DNEGRR = 590.9 ALES.C = 5.3 CLK/S.K = 0.01014 CMX/S.K = 0.403 RH0100 = 0.2204 CP/S = 0.0027754 CDK/S.K = 0.01014 CMX/S.K = 0.403 RH0100 = 0.2204 CP/S = 0.0027754 CDK/S.K = 0.01014 CMX/S.K = 0.403 RH0100 = 0.2204 CP/S = 0.0027754 CDK/S.K = 0.01014 CMX/S.K = 0.403 CMS = 0.480 CMS = 0.44 CMS = 0.480 CMS = 0		POINT	9		,			i					1
PSI OPPER ROTOR BLADE NURMAL BENDING MOMENT OR EUGEWISE UR PITCH OPPER ROTOR BLADE NURMAL BENDING MOMENT OF EUGEWISE UR PITCH OF SHAFT OF STATE OF		140.9	A SEC		590.		17	5.3 02754	CLR/S, R CDR/S, R	) H	Z X Z Z Z Z	u 'n	. 258 1126
PSI OPPER ROTOR BLADE NURHAL BENDING MOMENT OF EUGEWISE OF PITCH OF PRINCE OF CO. 18. 0.2 k. 3. 8. 0.6 k. bits. 0.1 k. c. k. 3. 8. 0.6 k. bits. 0.1 k. c. k.											)		
PSI         -6807         -621.         -1429.         -781.         -373.         -172.           10.00         -6807         -2472.         -2802.         -2848.         -171.         -51.           22.50         -6807         -2472.         -2802.         -2848.         -171.         -117.           22.50         -6807         -2472.         -2802.         -2848.         -171.         -117.           45.00         -5207         -2208.         -6629.         -678.         -277.         -277.           45.00         -5207         -2268.         -676.         -6001.         -1855.         -277.         -276.         -6001.         -1855.         -277.         -276.			ROT UR	BLADE		BENDIN 38	G MOMENT	Z	3	UR PITC	AD AD	∞.	JTOR SESS
0.00         -4890.         -621.         -1429.         -781.         -3733.         -172.           11.25         -5800.         -2713.         -2408.         -7171.         -171.         <	U				<u>.</u>					•	)		)
11.25         -578.         -1713.         -2408.         -2167.         -3013.         -517.           22.50         -6807.         -2472.         -2684.         -678.         -678.         -678.           22.50         -6807.         -2472.         -2684.         -678.         -678.         -277.           45.00         -695.         -2208.         -2628.         -5432.         -678.         -207.           45.00         -5207.         -2208.         -2628.         -5432.         -678.         -207.           45.00         -5103.         -1342.         -2184.         -2186.         -2604.         -2604.         -2604.           10.25         -5136.         -2135.         -2109.         -5229.         -3139.         -832.           112.50         -5136.         -2109.         -5229.         -5137.         -239.         -832.           112.50         -436.         -2109.         -6015.         -5204.         -239.         -617.           112.50         -436.         -2109.         -4216.         -5239.         -617.         -618.           112.50         -436.         -2109.         -4210.         -5229.         -5137.         -6117.	200		0	4	_	1 42	-		73		~	- 1	
11.2.5         -5780.         -1713.         -2802.         -2101.         -571.           21.5.0         -6955.         -277.         -2802.         -611.         -571.         -571.           33.75         -6957.         -277.         -2802.         -673.         -678.         -671.         -571.         -571.         -570.         -570.         -570.         -570.         -675.         -671.         -675.         -671.         -675.         -671.         -671.         -675.         -671.         <		ři		) (	• (	100	4 1						4 4
22.50         -6807.         -2472.         -2808.         -1771.         -117.           22.50         -6955.         -2765.         -2684.         -678.         -177.         -177.           45.00         -5207.         -2084.         -2684.         -3639.         -678.         -204.           45.00         -5207.         -2208.         -2600.         -6856.         -204.         237.           56.25         -4014.         -156.         -2604.         -2804.         -277.         -273.           78.75         -5730.         -1344.         -2175.         -4831.         -4177.         -832.           90.00         -334.         -1344.         -2175.         -4831.         -4177.         -239.           112.50         -436.         -1344.         -2175.         -4831.         -239.         -239.           112.50         -436.         -1374.         -2753.         -6241.         -113.           112.50         -436.         -474.         -2753.         -6241.         -113.           112.50         -454.         -474.         -6245.         -6241.         -113.           113.50         -633.         -272.         -474.         -6	11.25	<u> </u>	20	71-	3.	-2408-	-7017-		-3013	•	.16	101	Λ
33.75         -6955         -2745         -2684         -3639         -678         -277           45.00         -6014         -1596         -6018         -277         -270           56.25         -6014         -1596         -6014         -1695         -270           56.25         -6014         -1596         -766         -2604         -270           67.50         -5103         -1842         -2836         -4504         -2175           70.00         -2834         -2175         -4831         -1177         -282           10.25         -334         -1346         -2109         -5229         -5139         -236           112.50         -4365         -4386         -2105         -5229         -5133         -2296         -236           112.50         -4365         -471         -775         -523         -717         -223           112.50         -6741         -773         -6235         -6143         -213           155.50         -6741         -374         -6235         -625         -623           157.50         -6234         -773         -6235         -6235         -714           166.75         -6234	22.50	9	0	-24	72.	-2802-	-2848.		-1771-	7-	17.	74-	3
45.00         -5207.         -2208.         -5432.         -858.         -204.           67.50         -1596.         -2769.         -0001.         -1855.         147.           67.50         -5103.         -1896.         -2760.         -234.         -234.           78.75         -5136.         -2135.         -2601.         -3868.         -233.         -83.           78.75         -534.         -2175.         -2622.         -5193.         -239.           10.25         -4365.         -1335.         -2780.         -4015.         -594.         -239.           112.75         -4365.         -1336.         -2780.         -4015.         -594.         -239.           112.75         -4365.         -4367.         -4015.         -594.         -239.         -239.           112.75         -4366.         -4503.         -4241.         -6241.         -113.         -113.           1157.50         -6038.         -4241.         -6245.         -6048.         -465.         -414.           1187.50         -6038.         -4241.         -6246.         -6048.         -414.         -6241.         -613.           1187.50         -6038.         -4367.	33.75	9-	5	-27	.5.	-2684.	3639		-678.	-2	77.	74-	.86
56.25         -4014.         -1596.         -2769.         -6001.         -1855.         147.           67.50         -5103.         -1842.         -286.         -2604.         234.           78.75         -5134.         -2135.         -2601.         -2829.         -2839.           90.00         -3434.         -1345.         -2175.         -4931.         -2139.         -282.           112.50         -4539.         -1335.         -2780.         -5229.         -5139.         -233.           112.50         -456.         -4503.         -4280.         -5229.         -5139.         -213.           112.50         -456.         -4503.         -4280.         -3477.         -6353.         -212.           112.50         -6038.         -4280.         -4247.         -6241.         -113.           146.25         -6038.         -2867.         -3967.         -6887.         -6241.           155.0         -5133.         -2976.         -4379.         -6241.         -6255.         -4382.           168.75         -6038.         -5246.         -5042.         -6038.         -4241.         -6241.           155.0         -6389.         -3472.         -6887. </td <td>45.00</td> <td>-5.</td> <td>~</td> <td>-22(</td> <td>.90</td> <td>-2628.</td> <td>5432</td> <td></td> <td>858</td> <td>-2</td> <td>04.</td> <td>-50</td> <td>_</td>	45.00	-5.	~	-22(	.90	-2628.	5432		858	-2	04.	-50	_
67.50         -5103.         -1842.         -2836.         -4566.         -2604.         234.           78.75         -5730.         -2135.         -2601.         -3868.         -2604.         -2839.           90.00         -3334.         -2135.         -2601.         -3868.         -2339.         -83.           101.25         -2359.         -496.         -2109.         -5229.         -5193.         -2392.           112.50         -4362.         -4780.         -4015.         -594.         -2392.           112.50         -4362.         -4780.         -4015.         -594.         -2392.           112.51         -1335.         -2780.         -4015.         -594.         -2392.           146.25         -4503.         -4280.         -447.         -6241.         -1132.           146.25         -5387.         -4241.         -6235.         -4312.           168.75         -6741.         -6235.         -6143.         -4143.           168.75         -6387.         -4242.         -6243.         -4242.           168.75         -6387.         -4374.         -6255.         -4312.           168.75         -6387.         -4388.         -4242.<	56.25	3	4	-15	96.	-2769-	6001		-1855.	-	47.	)9-	.99(
78.75         -5730.         -2135.         -2601.         -3868.         -3239.         -83.           90.00         -2334.         -1344.         -2175.         -4831.         -4177.         -282.           10.25         -234.         -2109.         -5194.         -2139.         -239.           112.50         -4565.         -1335.         -2780.         -4015.         -5994.         -239.           112.50         -4565.         -1335.         -2780.         -4015.         -5994.         -239.           112.50         -4565.         -4580.         -3447.         -6241.         -113.           145.50         -6741.         -3978.         -3447.         -6241.         -113.           168.75         -6333.         -2976.         -3957.         -8887.         -6241.         -1181.           168.75         -6338.         -2867.         -3967.         -8887.         -6144.         -4144.           168.75         -10648.         -5248.         -5026.         -6398.         -4144.         -4144.           191.25         -1264.         -5107.         -4938.         -4241.         -4241.         -4241.           202.50         -1264.         -	67.50	-5	03	-18	42.	-2836	4566		-2604.	7	34.	-56	53.
90.00         -3834.         -1344.         -2175.         -4831.         -4177.         -282.           101.25         -4365.         -1394.         -2109.         -5229.         -5193.         -239.           112.50         -4365.         -436.         -2109.         -5229.         -5193.         -239.           112.50         -4365.         -4503.         -4280.         -3447.         -6353.         -212.           112.50         -8565.         -4503.         -4280.         -3447.         -6353.         -212.           116.25         -6333.         -2976.         -9487.         -6241.         -113.         -113.           146.25         -638.         -2867.         -94887.         -6241.         -181.         -181.           180.00         -8289.         -3876.         -4379.         -94887.         -6098.         -414.         -6255.         -414.         -414.         -626.         -414	78.75	15	0	-21	35.	~	868		-3239.	ı	83.	-35	.85.
101.25         -2359.         -498.         -2109.         -5229.         -5193.         -239.           112.50         -4365.         -1335.         -2780.         -4015.         -5994.         -235.           112.50         -4365.         -4280.         -3447.         -6245.         -6245.         -235.           157.50         -8565.         -4503.         -4241.         -6235.         -6245.         -181.           166.25         -6741.         -3978.         -4241.         -6235.         -6245.         -181.           167.50         -6333.         -2976.         -43957.         -6887.         -6245.         -181.           180.00         -8289.         -3876.         -4379.         -6296.         -4140.         -6255.           180.00         -8289.         -3876.         -4937.         -4140.         -2882.         -4140.         -2883.           205.50         -10648.         -5248.         -5043.         -4031.         -4140.         -2883.           213.75         -1827.         -4937.         -4037.         -4140.         -2883.         -4140.         -4262.         -4262.         -4262.         -4262.         -4262.         -4262.         -4262. <td>90.00</td> <td>-3°</td> <td>934.</td> <td>-13</td> <td>***</td> <td>N</td> <td>-4831.</td> <td></td> <td>-4177.</td> <td>-2</td> <td>N.</td> <td>-15</td> <td>171.</td>	90.00	-3°	934.	-13	***	N	-4831.		-4177.	-2	N.	-15	171.
112.50         -4365         -1335         -2780         -4015         -5994         -235           1123.75         -7754         -3362         -3741         -2753         -6353         -212           135.00         -8655         -4503         -4240         -6241         -1131           165.25         -6741         -3978         -4241         -6235         -1181           166.25         -6038         -2867         -3967         -9442         -6056         -455           180.00         -8289         -2867         -3977         -9442         -6098         -455           180.00         -8289         -5248         -5248         -6066         -455           180.00         -8289         -5248         -506         -4582         -414           202         -10648         -578         -408         -408         -414           202         -1264         -5835         -140         -240         -240           213.75         -4882         -4068         -4068         -4068         -4068           213.75         -4882         -2843         -2541         -4262         -288           213.75         -2845         -2843 </td <td>101.25</td> <td>-2</td> <td>359.</td> <td>4-</td> <td>98.</td> <td>~</td> <td><math>\sim</math></td> <td></td> <td>-5193.</td> <td>7-</td> <td>•</td> <td>71-</td> <td>.74.</td>	101.25	-2	359.	4-	98.	~	$\sim$		-5193.	7-	•	71-	.74.
123.75         -7754         -3362         -3741         -2753         -6241         -113           155.00         -8565         -4503         -4280         -347         -6241         -113           146.25         -6741         -8565         -4280         -347         -6241         -113           146.25         -6741         -978         -9487         -6255         -382           167.50         -587         -397         -9482         -6098         -458           180.00         -8289         -387         -4379         -6296         -4582           180.00         -8289         -5248         -5026         -6572         -414           191.25         -10648         -5248         -5026         -671         -438           202.50         -11264         -5835         -5107         -4937         -4140         -283           213.75         -926         -4862         -4937         -4140         -283         -426           225.00         -11264         -5835         -2107         -4934         -426         -426         -426           236.25         -2845         -2946         -4862         -4266         -426         -426	112.50	4-	365.	-13		-2780.	015		5994	-2	35.		.22.
135.00         -8565.         -4280.         -3447.         -6241.         -113.           146.25         -6741.         -3978.         -4241.         -6235.         -6143.         -181.           157.50         -6741.         -3957.         -8887.         -6255.         -382.           157.50         -6733.         -2976.         -3957.         -6038.         -4555.           180.00         -8289.         -2876.         -6572.         -4711.         -455.           180.00         -1048.         -5026.         -6572.         -4711.         -359.           202.50         -1048.         -5026.         -6572.         -4714.         -283.           213.75         -9296.         -4882.         -4068.         -4748.         -4240.           213.75         -9296.         -4882.         -4068.         -4140.         -240.           213.75         -917.         -1683.         -2241.         -4148.         -4240.           255.00         -6246.         -2943.         -3544.         -4240.         -4240.           255.01         -6246.         -1683.         -146.         -4240.         -4240.           258.75         -134.         -146.	123.75	-1	754.	-33(		-3741.	-2753.		-6353.	7-	12.	22	53.
146.25       -6741       -3978       -4241       -6235       -6143       -181         146.25       -5333       -2976       -3957       -8887       -6255       -382         168.75       -6038       -2867       -3976       -9442       -6058       -4555         180.00       -8289       -3876       -4379       -9298       -5482       -4146         191.25       -10648       -5246       -5202       -6252       -4140       -2892         213.75       -9296       -4882       -4068       -4081       -240         225.00       -11264       -5845       -2963       -3594       -4240         226.00       -2845       -2963       -3594       -4262       -288         236.25       -4140       -2462       -4314       -2462       -288         236.25       -2717       -1653       -2241       -4242       -4240       -2402         247.50       -2845       -2943       -1653       -2241       -4314       -606       -6114         281.25       -1146       -146       2646       1200       5763       -6169       -6114         292.50       -466       2646 <td< td=""><td>135.00</td><td>60</td><td>v o</td><td>-45(</td><td></td><td>-4280.</td><td>-3447</td><td></td><td>-6241.</td><td>7</td><td>13.</td><td>21</td><td>11.</td></td<>	135.00	60	v o	-45(		-4280.	-3447		-6241.	7	13.	21	11.
157.50         -5333.         -2976.         -3957.         -8887.         -6255.         -382.           168.75         -6038.         -2867.         -3907.         -9442.         -6098.         -414.           180.00         -8289.         -2867.         -4379.         -8298.         -5682.         -414.           191.25         -10648.         -5248.         -5026.         -6572.         -414.         -283.           202.50         -11264.         -5835.         -4377.         -4937.         -4140.         -283.           21.50         -11264.         -5835.         -4081.         -2483.         -2483.         -2483.           21.50         -4882.         -4081.         -4081.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2483.         -2444.         -2483.         -2444.         -2483.         -2444.         -2483.         -2444.         -2483.         -2444.         -2483.         -2444.         -2483.         -2444.         -2444.         -2483.         -2444.         -2444.	146.25	9-	•	-39		-4241.	235		-6143	7-	81.	7,	.94.
168.75       -6038.       -2867.       -3907.       -9442.       -6098.       -455.         180.00       -8289.       -3876.       -4379.       -8298.       -5482.       -414.         202.50       -10648.       -5248.       -5026.       -6572.       -4711.       -359.         213.75       -9296.       -4882.       -4308.       -4068.       -4061.       -283.         225.00       -6246.       -2845.       -2963.       -4262.       -288.         247.50       -6246.       -2845.       -2762.       -4376.       -606.         247.50       -317.       -1653.       -2241.       -4148.       -430.         258.75       -2179.       353.       -1763.       2414.       -5656.       -611.         270.00       -1283.       1628.       452.       4629.       -611.       -437.         281.25       -192.       2051.       966.       5763.       -6169.       -753.         292.50       446.       256.       1187.       3950.       -7158.       -525.         292.50       438.       2300.       444.       749.       -6619.       -6019.         292.50       -3069. <t< td=""><td>157.50</td><td>ا ا</td><td>33</td><td>-29</td><td></td><td>-3957.</td><td>887</td><td></td><td>-6255.</td><td>£-</td><td>82.</td><td>_</td><td>-97</td></t<>	157.50	ا ا	33	-29		-3957.	887		-6255.	£-	82.	_	-97
180.00       -8289.       -3876.       -4379.       -8298.       -5482.       -414.         191.25       -10648.       -5248.       -5026.       -6572.       -4711.       -359.         202.50       -11264.       -5835.       -5107.       -4937.       -4140.       -283.         213.75       -9296.       -4882.       -4908.       -4068.       -240.         225.00       -6246.       -2845.       -2963.       -3594.       -4262.       -288.         236.25       -6246.       -2963.       -3594.       -4262.       -288.       -240.         236.25       -6246.       -2963.       -753.       14.       -4262.       -288.         247.50       -2179.       353.       -753.       14.       -4374.       -606.         270.00       -1283.       1628.       452.       4629.       -611.       -437.         291.25       -792.       2051.       966.       5763.       -619.       -589.         292.50       1024.       3015.       1187.       3950.       -7158.       -716.         315.00       446.       749.       -649.       -6419.       -619.       -710.         325	168.75	91	ထ	-284		-3907.	-9445		-6098	4-1	55.	7	.69
-10648.       -5248.       -5026.       -6572.       -4711.       -359.       6         -11264.       -5835.       -5107.       -4937.       -4140.       -283.       7         -9296.       -4882.       -4308.       -4068.       -4061.       -240.       6         -6246.       -2845.       -2963.       -3594.       -4262.       -288.       6         -6246.       -2845.       -2963.       -3594.       -4262.       -288.       6         -3827.       -917.       -1653.       -2241.       -4148.       -430.       6         -2179.       353.       -753.       14.       -5656.       -611.       7         -1283.       1146.       2414.       -5656.       -611.       7         -1283.       1629.       -6811.       -437.       7         -1283.       1200.       5163.       -6169.       -5269.         -1024.       3015.       1187.       3950.       -7158.       -525.         -128.       2300.       444.       749.       -6635.       -476.         -211.       1758.       -244.       -4444.       -607.         -2241.       -2444. <td< td=""><td>180.00</td><td>8</td><td>289</td><td>-38</td><td></td><td>-4379.</td><td>298</td><td></td><td>-5482</td><td>4</td><td>14.</td><td>31</td><td>.14.</td></td<>	180.00	8	289	-38		-4379.	298		-5482	4	14.	31	.14.
-112645835510749374140283. 702 -92964882430840684081240. 688 -62462845296335944262288. 680 -3827917165322414148430. 639 -2179. 353753. 144374606. 569 -1342. 1146146. 24145656611. 595 -1283. 1628. 452. 46296811437. 707 -1283. 1628. 452. 64696119589. 632 1024. 2646. 1200. 51956619589. 632 1024. 3015. 1187. 39507158525. 450 -721. 1758243445476607. 31	191.25	-10	548.	-554		-5026-	572		-4711.	-3	59.	9	167.
-9296.       -4882.       -4068.       -4068.       -240.       688         -6246.       -2845.       -2963.       -3594.       -4262.       -288.       680         -3827.       -2917.       -1653.       -2241.       -4148.       -430.       639         -2179.       353.       -753.       14.       -4374.       -606.       556         -1342.       1146.       2414.       -5656.       -611.       595         -1283.       1628.       452.       4629.       -611.       595         -1283.       1628.       452.       4629.       -611.       595         -1792.       2051.       966.       5763.       -618.       -437.       734.         -1024.       3015.       1187.       3950.       -7158.       -525.       450         -175.       2774.       2560.       -7377.       -476.       -476.       749.         -721.       1758.       -244.       -4444.       -439.       -439.       -439.	202.50	-117	264.	-58	•	-5107.	4937		-4140.	7-	83.	7	21.
-6246.       -2845.       -3594.       -4262.       -288.       680.         -3827.       -917.       -1653.       -2241.       -4148.       -430.       639         -2179.       353.       -175.       14.       -4374.       -606.       569         -1342.       1146.       -146.       2414.       -5656.       -611.       595         -1283.       1628.       452.       4629.       -6811.       -437.       707         -1283.       1628.       452.       4629.       -6189.       -437.       737         -1283.       1626.       5763.       -6189.       -432.       736         -1024.       3015.       1187.       3950.       -7158.       -589.       450         -1024.       2300.       444.       749.       -6635.       -476.       71         -721.       1756.       -244.       -244.       -4444.       -344.       -439.	213.75	76-	296.	-48		-4308.	4068		-4081.	-5-	•0•	39	385.
-3827.       -917.       -1653.       -2241.       -4148.       -430.       639         -2179.       353.       -753.       14.       -4374.       -606.       569         -1342.       1146.       2414.       -5656.       -611.       569         -1283.       1628.       452.       4629.       -6811.       707         -1283.       1628.       452.       4629.       -6811.       707         -792.       2051.       966.       5763.       -6169.       -437.       736         446.       2646.       1187.       3950.       -7158.       -589.       632         1024.       3015.       1187.       3950.       -7158.       -525.       450         755.       2774.       927.       2560.       -7377.       -367.       -476.       71         -721.       1756.       -244.       -4444.       -436.       -607.       31         -3069.       731.       -244.       -4444.       -439.       -432.       -432.       -432.       -432.       -537.       -244.       -4444.       -432.       -432.       -432.       -432.       -444.       -444.       -444.       -444.	225.00	·9-	246.	-28		-2963.	3594		-4262.	-2	88.	39	101.
-2179.       353.       -753.       14.       -4374.       -606.       569.         -1342.       1146.       -146.       2414.       -5656.       -611.       595         -1283.       1628.       452.       4629.       -6811.       -437.       707         -1792.       2051.       966.       5763.       -6769.       -432.       736         446.       2646.       1200.       5195.       -6619.       -589.       632         1024.       3015.       1187.       3950.       -7158.       -559.       450         755.       2774.       927.       2560.       -7377.       -367.       234         438.       2300.       444.       749.       -6635.       -476.       71         -721.       1758.       -24.       -4444.       -436.       -607.       31	236.25	-3	327.	6-		-1653.	2241		-4148.	4-	30.	9	198.
-1342.       1146.       -2414.       -5656.       -611.       595         -1283.       1628.       452.       4629.       -6811.       -437.       707         -192.       2051.       966.       5763.       -6769.       -432.       736         446.       2646.       1200.       5195.       -6619.       -589.       632         1024.       3015.       1187.       3950.       -7158.       -589.       632         755.       2774.       927.       2560.       -7377.       -367.       234         438.       2300.       444.       749.       -6635.       -476.       71         -721.       1758.       -24.       -544.       -444.       -432.       31         -3069.       731.       -244.       -444.       -432.       31	247.50	-2	179.	Ĭ.		-753.	14.		-4374.	9-	.90	26	93.
-1283.       1628.       452.       4629.       -6811.       -437.       7075.         -792.       2051.       966.       5763.       -6769.       -432.       7366.         446.       2646.       1200.       5195.       -6619.       -589.       6320         1024.       3015.       1187.       3950.       -7158.       -525.       4507         755.       2774.       927.       2560.       -7377.       -367.       2344         438.       2300.       444.       749.       -6635.       -476.       716         -721.       1758.       -24.       -344.       -4444.       -607.       310         -3069.       731.       -244.       -4444.       -439.       8	258.75	-1-	342.	11	.93	-146.	414		-5656.	9-	11.	Š	.656
-792.       2051.       966.       5763.       -619.       -432.       7366.         446.       2646.       1200.       5195.       -6619.       -589.       6320         1024.       3015.       1187.       3950.       -7158.       -525.       4507         755.       2774.       927.       2560.       -7377.       -367.       2344         438.       2300.       444.       749.       -6635.       -476.       716         -721.       1758.       -24.       -344.       -607.       310         -3069.       731.       -244.       -4444.       -439.       8	270.00	-1,	283.	16.	28.	452.	679		-6811.	4-	37	7(	5
446.     2646.     1200.     5195.     -6619.     -589.     6320       1024.     3015.     1187.     3950.     -7158.     -525.     4507       755.     2774.     2560.     -7377.     -367.     2344       438.     2300.     444.     749.     -6635.     -476.     716       -721.     1758.     -24.     -344.     -5476.     -607.     310       -3069.     731.     -537.     -244.     -4444.     -439.     8	281.25	ĺ	92	20,	51.	966.	763		-6169.	4-	32	7	Φ
1024.       3015.       1187.       3950.       -7158.       -525.       4507         755.       2774.       2560.       -7377.       -367.       2344         438.       2300.       444.       749.       -6635.       -476.       716         -721.       1758.       -24.       -344.       -5476.       -607.       310         -3069.       731.       -537.       -244.       -4444.       -899.       8	292.50	•	46	•	•6•	2	195		-6199-	5	83	9	0
755.       2774.       927.       2560.       -7377.       -367.       2344         438.       2300.       444.       749.       -6635.       -476.       716         -721.       1758.       -24.       -344.       -5476.       -607.       310         -3069.       731.       -537.       -244.       -4444.       -439.       8	303.75		24	0	15.		950		8	S	25	*	-
438. 2300. 444. 7496635476. 716 -721. 1758243445476607. 310 -3069. 7315372444444439. 8	315.00		55	-	74.	927.	560		~	3	67.	2	4
-721. 1758243445476607. 310 -3069. 7315372444444439. 8	326.25	•	38	3	20.	444.	749.		5	<b>\$</b> -	16	•	•
-3069. 7315372444444439. 8	337.50	Ĩ	21	7	58.	~	344		5476	•	07		0
	348.75	G	•	-	31.	53	244		555	4			8

RUN 24 VKTS = V/OR =	PCINT 140.9 0.403	6 CAE RHU	CMEG*R = RHU100 =	590.9 0.2204	ALFS,C CP/S =	. = 0.002754	5.3 CLR/S, F	~ ~	=0.07855 =0.01014	CMY/S,R = 0.1258 CMX/S,R =-0.0126
	LOWER	KOTOR	BLADE !	NURMAL R	BENDING .3R	MOMENT .6R	LR EDGEWISE BENDING . 1R		LR PITCH Link Luad	
- 10			•							
00.00	7	63	60	•	582.	-593.	-400	13.	-168	3.
88.7	-	N	30	•	968.	-259.	-122		-210	•0
	~	-	145	5.	1363.	-66-	-834	48.	-371	•
66.2	4	72	61	9.	1746.	-166-	-7432	,Z.	-158	•6
55.0	4	2	14	•	1819.	-213.	-7374.	. *	38	• 60
43.7	, 7	35	18	••	1479.	-201.	1406-	.1.	ï	э.
32.5	~	8	36	<b>4</b> •	852.	-469	-9934.	4.	66	• 6
21.2	. 1	9	3	١.	337.	-868-	-8008	.8∙	707	<b>1.</b>
10.0	2	-	4		269.	-1226.	-532	•	19	• -1
98.7	, 7	3	3	۲.	300.	-1402.	-5078	.80	89	•
87.5		Ò	96	<b>4.</b>	-84.	-1332.	-6501	11.		3.
76.2	7-	~	-32	•9	-591.	- 796 -	-5859	.6.	259	•
65.0	7-	_	60	æ.	-604-	-538.	967-	.1.	88	• \$
153.7		94	~	8	-119.	-218.	-2039	.6.	173	٠.
42.5	•	92	6	1.	547.	•09	-4397	.7.	566	• •
131.2		œ		1.	1277.	301.	-6553	3.	144	•
20.02	2	7	3	٠	2006.	459.	-6057	7.		7.
08.7	, <b>*1</b>	00	0	7.	2607.	529.	1115-	1.	-39	•
7.5	7	•	2	٠ ۲	2891.	720.	-6204.	14.	55-	•
6.2	~	J		۲.	2607.	891.	-8197	.7.	-35	٥.
5.0		5	4	•	1764.	855.	_	<b>40</b> •	- 40	•0
3.7	- 1	m	4	4.	765.	•	-537	74.	-56	• 5
2.5	7-	30	15	2.	-45.	345.	-2511.	.7.	-118	'n
1.2	7-	0	180	£.	-691.	-88-	-7066.	• •	<b>76 I -</b>	• .*
0.0	स 	3	22	•	-1291.	-651.	-221	•	- 55	٥.
8.7	7-1	•	245	5.	-1915-	-983.	24-	3.	156	• •
Š	<b>\$</b> 1	~	356	' '	.2511.	- 406 -	7305	,2.	-61	1.
56.2	ı	0	493	•	.2941.	-752.	2646.	Ĭ6.	-436	•9
45.0	-1	$\sim$	165	3	.3030.	- 734 •	15	53.	-350	•0
333.75	3-	5,505.	-400	•	.2565.	-678.	1161-	.7.	-1 86	• 0
22.5	4	85	267	۰,	-1472.	7	9681-	٠8.	-397	7.
11.2		•	49	2.	-216•	-685.	-111	<b>.</b>	-436	5.

RUN 24	PCINT	<b>7</b>		6	) O U * 4	,		7 T T T T T T T T T T T T T T T T T T T		7071
VKIS II	140.0	RHU100	11 11	0.2188	CP/S =	0.03186	86 CUK/SIR	R =0.01295	CMX/S, R	# 10.01-8 =-0.0128
				J. O. D.	UPPER KCICK	K BLADE NORMAL		BENDING MUMENT		:
		• 1.R			• 2 P.			• JK		• <b>6</b> %
	u	SO	NIS		SUS	21S	SOO	Z S	SU 3	NIS
HARMONIC	•				3 3 6 1 6		F 030		C 700	
c	7	5.5			n		7.002		7.060-	
_	_30 <b>0</b>	,o. ~	4583.4			2542.4	-1115.9	1378.4	109.2	-1332.8
2	1681-	1.4	Δ			-505-3	-1029.7	-196.6	-5590.6	398.1
~	911-	7.9	248.1			109.5	-45.7	40.7	30.8	33.3
\$	49-		•			-640.0	74.3	-286.8	4.04	1022.2
'n	-239		~			342.6	-120.3	1.88.7	213.7	8.615-
9	-136	6.5	S		1.5	-409.8	-45.8	-222-1	172.2	538.7
7	34	•	33		198.0	-20.9	9.61	-24.6	-195.0	79.6
c	8	7	236.2	•	-34.4	88.1	1.9	-21.8	-12.6	-162.8
6	-34	•	45		-153.1	0.1-	32.8	-7.8	163.6	-227.1
1.0	10	8	44		-16.8	-16.0	7.0-	23.7	9 * * 6	-76.8
20	UPPER	ROTUK	EDGE		UPPER KLTOR	U.T.OR	UPPER			
04	BEND	ING	ENT	.1R	PITCH LINK LGAU	K LGAD	SHAFT	I STRESS		
	SOO		4		COS	215	COS			
HAFMONIC										
0		•			-305.4		2183.8			
7		0.0	O•0	_	43.3	286.6	-4605.6	-2161.5		
2		•	0.0	_	-2.6	108.3	-762.1	-781.1		
~		•	0.0	_	-10.7	-41.0	422.1	-322.5		
4			0	_	25.6	24.9	-182.7	1201.1		
5			0.0	~	9.1	-33.2	-26.0	-234.2		
9			0	_	0.64	10.7	11.9	51.6		
7		0.0	0.0	~	-35.2	48.5	-237.1	-278.5		
œ		•	0	_	41.8	14.1	140.8	-188.3		
6		•	0.0	_	4.1	39.1	87.2	-21.9		
10			0.0	_	6.0-	-15.1	-19.2	33.8		

.1R SIN	RUN 24 VKTS = V/GR =	PCINT 7 140.9 0.394	OMEG*R = RHJ103 =	603.8 0.2188	ALFS,C CP/S =	= 5.5 0.003186	CLR/5, R CUR/5, R	( =0.11311 ( =0.01295	CMY/S,K = CMX/S,R =-	= 0.1694 =-0.0128
LDS SIN 1587.1 1787.5 -5947.8 -2677.2 1311.3 -129.0 -261.7 -550.2 890.6 -244.8 -502.9 -362.0 631.1 297.6 264.4 -47.4 -172.5 -321.1 -281.1 -198.7 43.4 CDS SIN -4959.5 1101.9 310.7 -1715.5 352.6 41.2 -59.8 16.3 88.6 -10.2 -130.0 587.1 -510.4 -510.4				j	LUWER ROTOR	BLADE NURMAL		BENDING MUMENT	<b>3</b>	
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-244.8 -502.9 -362.0 631.7 297.6 264.4 -47.4 -172.5 -321.1 -281.1 -198.7 43.4 COS SIN -4959.5 1101.9 310.7 -1715.5 352.6 41.2 -59.8 16.3 88.6 -10.2 -130.0 587.1 -510.4 -31.3 -76.8	4	- 550	068			609.6	7 · · · · · · · · · · · · · · · · · · ·	7.087	20.0	1.74
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-321.1 -281.1 -198.7 43.4 LUWEK RUTUK EUGEWISE BENDING MOMENT .1R COS SIN -4959.5 SIN -4959.5 LIUI.9 310.7 -1715.5 352.6 41.2 -59.8 16.3 88.6 -10.2 -130.0 587.1 -510.4 -31.3 -76.8	80	-47.	-172		-58.3	-45.1	6.2	-11.0	ν. Υ.	14.0
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1 0 41	6	S	-57		-60.4	•				
0.01	1.3	-16.	.9- 6	8	-60.0	39 • 4				

ab.

RUN 24 VKTS # V/OR #	POINT 140.9 0.394	7 OMEG*R RHO100	3#R =	603.8 0.2188	8 ALFS,C 8 CP/S =	S.C = 5.5 S = 0.003186	5.5 3186	CLR/S, R CDR/S, R	=0.11311 =0.01295	CHY/S,R CHX/S,R	= 0.1694   =-0.0128
	UPPER R	OTOR	BLADE	: NORMAL	BENDING 38	MUMENT	UR EDGE	EDGEWISE DING LIR	UR PITCH	<i>-</i>	UPPER ROTOR
V	•	<b>.</b>	;	í	Ś	•					
00.0	-52	33.	-132		-1978.	-2550.		0	1-	82.	-3047
7	143	6			1955	2661		6	•	0	• •
5.5	14-	0	(4-		1371	1895		d	-151	57.	3151
•	-14	5	712		-323	-1301		•	-17	75.	283
5.0	16	.23.	238	38.	559.	-1838.		•	•	-7-	-3383.
.2	36	3860.	385	54.	1042.	-1531.		•	-	137.	-4124.
7.5	38	.79	440	.20	1583.	-69-		•	Ĭ	107.	-3295.
8.7	35	112.	503	31.	2317.	31.		ċ	•	42.	-976.
0.0	78	126.	648	32.	2836.	-1037.		<b>.</b>		1.	1099
01.2	88	18.	725	52.	2936.	- 784 •		ċ	ĭ	-91.	2510.
2.5	56	.88	623	12.	2654.	395.		ċ	-156	26.	4424.
23.7	45	.069	490	32.	2097.	230.		•	ĩ	-67.	5955.
35.0	55	.80	484	15.	1718.	-1596.		°	161-	91.	5500.
46.2	99	.44.	553	33.	1829.	-3818		•	-487	87.	4011.
Š	<b>9</b>	363.	571	.91	1925.	-5173.		• •	-5	19.	3417.
68.7	949	,71.	485	.96	1413.	-4884-		°	-5-	.279.	4140.
180.0	14	9	326	)5.	481.	-3235.		•	-203	03.	5672.
91.2	-16	,50.	135	.90	-340•	-1379.		•	-3.	324.	7118.
02.5	-26	. 99	40	)2.	-717-	- 594.		ċ	-3(	-369.	7577.
13.7	-18	399.	9	38.	-550.	-66-		<b>.</b>	-3	-356.	7276.
25.0	C1-	152.	133	34.	-92•	-95.		•	<b>) 7</b> -	07.	6800
36.2	9-	.60	180	.86	222.	302.		•	64-	93.	5918.
47.5	1	. 82	193	30.	267.	1024.		•	-5	-590•	4882.
58.7	-14	Ø	191	14.	167.	2115.		ċ	-638	38.	4611.
70.0	-29	œ	88	11.	-31.	34		•	-5(	568.	4843.
81.2	- 36	Φ	28	31.	-332.	3513.		ဝ	-5	529.	4 700.
92.5	-36	0	_	74.	-726.	34		°	9-	~	4126.
03.7	-39	9	-20		-1161-	1093.		•	-68	83.	3006.
15.0	-45	3	-68		-1471.	-267.		·	-5	53.	1112.
7	-45		-81		2	-2274.		•	94-	65.	- 703.
37.5	04-	3	-64		-1624.	-3406.		•0	4-	486.	63
48.7	-48	2	-85	•	-1780.	-2893.		•	7-	• 00	-2252.

	POINT	7							
VKTS =	140.9	Ž	OMEG#R =	603.8	3 ALFS,C	j,( ± 5.5	5.5 CLR/S,R		$CMY/S_{y}R = 0.1694$
V/0R =	0.394	RH.		0.2188				\ =0.01295	ii
	LOWER	ROT OR	BLAUE	NGRMAL R	BENDING .38	MOMENT -68	LR EDGEWISE Bending . 18	LR PITCH	(TCH
V		4	,	ŧ.	)	; }	•		
0	60	641.	109	,2•	3851.	-243.	-2702.	7-	140.
•		82	9	<b>N</b>	-	8	-	· "-	
7.5	6	~	631	33	4594.	164.	-6324.	<b>5</b>	-440.
6.2	1132		746	0	4845.	17.	-6965	7	-176.
5.0	6		746		4643.	138.	-1049.		35.
3.7	9		585	.8.	3898.	194.	-7864.		17.
2.5	S	5793.	432	. 4.	2870.	-41.	-9450.		41.
1.2	ιΛ	620.	368	17.	2054.	-466-	-10103.	<b>→</b>	.25.
0.0	4	665.	319	ō.	1535.	-932.	-9254.		186.
8.7	7	579.	218	•	786.	-1207.	-8485.	2	206.
7.5	1	967.	27	9•	-465.	-1197.	-8748.	-	164.
6.2	4-	-4782.	N		.1755.	-963.	-8447.	~	151.
5.0	9-	617.	39		.2522.	-751.	-6528.	~	.44.
3.7	9-	354.	42		.2603.	-660.	-4667.		36.
142.5	75	34	-367	•	-2133.	-579.	-4413.		52.
1.2	<b>サ</b> -	•	27	5.	.1434.	-430.	-4839.	2	216.
120.0	Ē,	~	18	٠.	-4664-	-229.	-4505.		.06
8.7	-2	2483.	11	2•	-259.	21.	-3603.	7-	206.
7.5	-2	-	7	.7.	234.	320.	-3289.	7	197.
6.2	7-	-4	S	.9.	583.	561.	-4034	-	-130.
5.0	1	S	3	д.	739.	588.	-5065	7	186.
3.7	1	Ø	27	•	822.	452.	-5107.		-8-
5.5			99	.7.	950.	328.	-400I.	7	141.
1.2		7.	71	1.	8	184.	-3093.	,	-92.
0.0		6	16	.4.	1145.	-43.	-3241.	-	-106.
8.7	7	-4	971	.8.	1037.	-157.	-3258.	7	184.
5	1	-398-	81	1.	862.	-86-	-1882.	•	-18.
56.2	1	•	25	.69	749.	-10.	-588-	<b>\$</b>	452.
45.0	7	3	71	8.	862.	-175.	-481-	€-	379.
۲.	7	98	183	.91	1442.	-227.	-1883-	7-	262.
22.5	'n	-	321	.6	7440	-302.	-2457.	<b>5</b> -	・カナナ
11.2	20	7	7	.5.	3349.	-399.	-2152.	£-	168.

= 0.1812 =-0.0135	-1995-1 -1995-1 -1995-1 -410-6 1047-5 -687-4 -128-2 -258-8 -100-9	
CAX/S,R =	210.5 -2159.0 -2159.0 -2159.0 -210.5 -2210.5 -82.9 84.0 58.0	
=0.12530 =0.01325	BENJING MUMENT  .3R  .0S .3R  213.5 .2521.8  043.1 .546.4 -27.9 .74.9 .88.3 .282.4 .137.2 .186.0 -58.5 -261.7 .22.3 -42.0 -24.6 -29.2 37.0 -11.5	STRESS STRESS SIN -878.6 -665.4 -358.4 1137.7 -482.7 -79.3 -282.9 -194.7 -48.9
CLR/3,K CDR/S, K	COS COS 808.2 213.5 -1043.1 -27.9 -88.3 -137.2 -58.5 -24.6 37.0	UPPER SHAFT CUS 2405.4 -4013.6 -668.8 407.0 24.2 15.1 39.2 -268.0 59.4 111.4
= 5.5 3.034110	BLADE NURMA SIN 268.2 967.0 52.3 648.1 425.8 489.4 -17.6 71.1 58.9	290.7 290.7 156.4 -12.7 42.8 -47.5 -0.9 -6.8 21.4 20.2
ALFS,C CP/S =	UPPER RCTCF CUS CUS 2970.9 -1406.2 -71.7 -193.7 -332.0 -4.1 -201.8 -125.5	UPPER RUTUR CLS SI -335.4 S90 13.3 156 -13.3 -12 3.9 42 26.5 -47 65.7 -0 -15.9 -6 42.7 21 20.3 20
UMEG*R = 601.7 RHU130 = 0.2184	6902.0 -1327.5 -1327.5 -1191.7 885.9 -729.5 -84.4 186.8 332.6	KUTUK EDGEWISE NG MUMENT .IR S SIN .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0 .0 0.0
PUINT 8 141.2 UM 3.396 RH	1451.5 -126.4 -126.4 -129.9 -72.2 -341.6 -249.5 376.7 -237.1 -58.8	DPPER RUING CUS
RUN 24 VKTS = V/CR =	HAP MENTE 0 1 2 2 4 4 5 5 7 10	208 H ARRAN 10 10 10 10 10 10 10 10 10 10 10 10 10

f

<pre>&lt; = 0.1812 &lt; =-0.0135</pre>	6R SIN 77.9 77.9 77.9 77.9 77.9 77.9 77.9 77.
CMY/S+R CMX/S+R	122.8 160.4 160.4 17.2 95.2 95.4 19.4 11.4
=0.12530 =0.01325	ALMENT SIN SIN 344.9 -2709.6 -242.1 -35.6 -2 -35.6 -2 -3.9
CLR/5, K CUR/5, R	BENDING -3 CUS -3 1823.2 -122.7 1495.4 135.3 -134.9 -77.8 81.4 23.0 -12.6
5.5	R BLADE NURMAL  R SIN  -4588.9  -4588.9  -120.5  741.8  -131.1  473.8  -8.0  -8.0  -8.0  -8.0  -8.0  -8.0  -13.1  473.8  76.1  22.3  75.6  114.8  78.7  35.6  49.9  72.2  -26.1  -9.5  19.0
ALFS,C CP/S =	CGS -2R CGS -2R CGS -28 -249 -4901.3 -1901.3 -
UMEG#K = 601.7 RHU100 = 0.2184	244.6 -1032.6
PCINT 8 141.2 UA 0.396 RH	2973.2 -2684.3 -2684.3 -188.0 -768.9 -354.4 -257.7 -257.7 -12.1 -1
PUN 24 VKTS = V/CR =	HARMONIC 10 9 8 4 4 7 5 5 5 6 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 6 7 5 6 7

f

/s,R = 0.1812 /s,R =-0.0135	UPPER ROTUR SHAFT STRESS		9	\$	0	53	-1872.	<b>(1)</b>	34	82	2443.	59	S.	6859.	.1109	4237.	3432.	3949.	5514.	7089.	7217.	6225.	5359.	4557.	3739.	3634.	98	8	•		S	0		-1184.
=0.12530 CNY/	UR PITCH LINK LUAD		15	7	-172.	-75.	105.	176.	- 65	-52•	- 18.	-160.	-218.	-142.	-200•	-694-	-558.	-395•	-277.	-270-	-303.	-397.	-441.	-434.	-577.	-732.	-644	-547.	-648		S		0	-362.
CLR/S, R CDR/S, H	JR EDGEWISE SENDING . 1R		•	•0	•	• •	•	•0	•	•	•	•	ż	•0	ċ	ċ	•0	•	•	•	•0	•	•	·	•	•	•	•	•	•	•	•	•	•
S.C = 5.5 S = 0.004110	MOMENT L		92	-1026.	"		30	-201.	1196.	863.	-506-	351.	1682.	1653.	-123.	-2796.	-4973.	-5321.	-3949.	-2335.	-1712.	-1994.	-2146.	-1603.	-546.	1071.	2890.	3573.	2922.	2012.	772.	-885.		-950-
AL F CP/	BENDING •3R	) }	-153.	-63•	667.	1714.	2468.	2880.	3394.	4108.	4620.	4622.	4067.	14	5	21	0	90	36	53	-2097.	206	159	12	-941.	-860•	-069-	-516-	-436.	-435.		-254.	-6-	27.
OMEG*R = 601.7 RHU100 = 0.2184	BLADE NORMAL		$\sim$	608	~	2	5379.	ø	0	~	~	~	3	6490.	-	30	~	5	_	-408-	-1676.	-1527.	-817.	-187.	187.	157.	_	-101-	347.	639.	3	139	8	528
PCINT 8 141.2 OME 0.396 RHU	UPPER ROTOR				-	_	6028.	7720.	7580.	•0106	11812.	11761.	3684.	6545.	6562.	6946	6424.	4057.	•	-4488	-5776.	-4945	0	ø	0	•	47	51	8	-	66	72	830	S
RUN 24 VKTS = V/OR =		S	0	1.2	2.5	3.7	5.0	5.2	7.5	8.7	0.0	01.2	12.5	23.7	35.0	46.2	157.5	68.7	180.0	91.2	02	13.7	25.0	36.2	47.5	58.7	70.0	81.2	92.5	03.7	15.0	26.2	37.5	8.7

KUN 24	PCINT	<b>∞</b>				;		•	
/KTS = //OR =	141.2 0.396	DMEG#R RHU100	*R = 601.7 00 = 0.2184	7 ALFS,C 4 CP/S =	c = 5.5 = 0.004110	CLR/S,R CDR/S,R	=0.12530 =0.01325	CMX/S,R = 0.1812 CMX/S,R =-0.0135	
	LOWER R	ROTOR BL	BLADE NORMAL	BENDING M	MOMENT	LR EDGEWISE Bending .lr	LE PITCH	0	
150		•	:	;					
00	166	•	7057.	4627.	-75.	-4599	-100	•9	
88	16	95	7147.	5099.		52	-310	•0	
77.	120	23	7916.	5663	337.	-7850-	-397	7.	
99	39	4	9273.	6132.	333.	-8298	- 88	. 60	
55	1267	20	9369.	6077.	356.	-8413	130	• 0	
43.	103(	0	8015.	5406.	344.	-9274.	109	•	
232.50	93	96.	6745.	4492.	123.	-10437.	125	5.	
21.	93.	87.	6256.	3817.	-369.	-10219.	71	•	
10	87	6.J.	5964.	3390.	-836.	-8879.	707	1.	
98.	49	68.	4975.	2640.	-991.	-8581.	797	2.	
87.	24.	20.	2805.	1280.	-919.	-9158	262	2.	
76.	-1651-	91.	143.	-126.	-724.	-8132.	179	•6	
65.	-32	21.	-1586.	-898-	-456.	-5643	991	• 9	
53.	-31.	22.	-1920.	-976-	-333.	-4443.	22	•9	
42.	-25	50.	-1537.	-632.	-348.	-4935.	257	7.	
31.	-18	20.	-970-	-145.	-240.	-4910.	200	•0	
20.	-11-	24.	-365.	227.	-40•	-3722.	30	• •	
08.	-12	62.	-37.	447.	141.	-2806.	76-	•	
97.	-2177	77.	-214.	611.	421.	-2959.	-48	. 80	
•	-25	61.	-561.	610.	639.	-3565.	-45	2.	
5	-20	44.	-636-	376.	536.	-3628.	-124	•	
~	-18	13.	-546.	201.	361.	-2647.	-7.	1.	
~	-18	90.	-514.	290.	245.	-1268.		1.	
_	6-	18.	-226.	439.	-94-	-144.	-31	1.	
ö	17	73.	348.	438.	-457.	-1044.	101	7.	
æ	4-	47.	373.	301.	-416.	-737.	716	• •	
-	-19	23	-340.	104.	-237.	467.	36	• •	
56.	-15	48.	-670-	-07	-249.	884.	-298	8.	
45.	ň	45.	56.	381.	-242.	-385.	-310	••	
33.	67	15.	1520.	1377.	-221.	-1921.	-341	1.	
22.	ು	43	3648.	2747.	-373.	-2469.			
311.25	16	45	5940.	3929.	-399.	-2874.	-284	•	

X = 0.1834 X =-0.0004	3	NIS.	•		-1882•	954.	284.	634.	-558.	268.	67.	0 -244.2	-213.	-81.															
CMY/S,R CMX/S,R		COS		-1621-	÷			•	•	•	•	-11.	•	•															
=0.09029 =0.01622	BENDING MUMENT	N I			766.1	117.1	128.8	6*667-	177.6	-181.7	-31.0	1.14-	80 • 55	11.4	ROTCR	STRESS	SIN			144.	29.	27.	031.	96	•	252.		23.8	•
CL R/5, K COR / 5, R		<b>X7.</b>	503	-468.1	-1945.8	-492.7	38.2	117.5	-56.1	-68.0	56.5	1.0	23.4	15.8	UPPER				022	-3049.6	515	389.3	-270.9	•	-0-3	35.	7.	32.0	6
7.9	R BLADE NCRMAL				1591.8	7	192.8	-422.5	393.7	-358.6	-15.5	105.3	-33.8	4.1-	RUTUR	NK LOAD				~	N	-	•	~	0	o	33.0	T-0-	-32.1
ALFS.C	UPPER ROTOR	*5.	212	185	121	•	vo	172.3	~	- 60		_	-	-19.1	UPPER	PITCH LINK	SOO		-421.8	4.04-	-10.0	-105.3	-16.1	-57.8	33.6	68.0	39.8	4.8	1.2
UMEG#K = 600.4 RHJ100 = 0.2175			Z 10		3773.6	-206-8	300.8	-759.2	703.8	-485.5	-100.B	323.9	169.0	4.6-	IR EDGEMI	NG MUMENT . IR	SIN			0.0	0•0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
PUINT 9 142.4 UME 0.400 RHJ	,	* 1R	503	-1031.5	. 4	•	2007. H	-42.9	-133.6	-211.7	234.5	1.00.0	7.88.7	-70.4	UPPER RGIO	M SNI CMER	503		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0 0	0.0	0.0
FUN 24 VKTS = V/CR =			CTMCMOAU	)	٠,	• ^	.ı ~	• 4	י י		· •	- a	י ס	10	2:	12		HARMONIC	Ç	_	~	: ••	• 4	· w	· •c	. ^	- <b>a</b> x	• •	10

Contract of the Contract of th

= 0.1804 =-0.0004	į	Z 7		514.4	230.3	9.69	4.04-	83.5	9.64-	-19.5	<b>5. 5</b>	-11.0	4.7															
CMY/S,R = C	. 6R	د <u>ن</u> د	-405.0	635.8	-492.4	116.7	20.8	23.4	38.7	-20.8	11.8	27.5	-4-3															
=0.09029 =0.01622	MOMENT	Ž S		87.1	807.1	8•1	6*86	-182.1	142.8	-30.8	16.1	-1.0	5.4															
CLR/S,R CUR/S,R	60	SOO	509.8	2689.3	1701.8	-14.2	25.8	-37.2	-84.2	76.3	19.3	-5- ს	-2-3															
616000°0	BL & CF ROQMAL	2 7		-662.9		-40.5		366.2				102.9	61.9						98.5	95.6	26.9	-26.1	-28.5	18.7	26.9	<b>5.9-</b>	55.6	6*51
ALFS,C CP/S =	LOWER ROTOR	503	1008.7		2256.8			'						LUWER KU	PITCH LINK	COS		-133.1	-177.3	35.3	-7.0	-46.3	-14.4	43.0	10.8	11.2	-I.6	-36.2
DMEG*R = 600.4 RHO100 = 0.2175		NIS	•	-1098.3	1430•3	-166.6	6.661	-722.2	421.2	273.0	-64.1	15.1	1.6	STUR EDGEWISE	MOMENT .	NIS			-718.7	-2717.5	138.1	-76.5	34.0	-67.4	-619.9		-1	3 -11.8
POINT 9 142.4 C 0.400 F		S 0 3	-1387.5	4179.	-3359.(	-234	-229.1	-88-	-481.	211.	-132.	-334.	-142.	L DWER RO	-	SUO		-5068	1522.	615.	457.	54.1	84.		0	-99.	•	•0-
RUN 24 VKTS = V/OR =		HARMONIC	6		2	<b>~</b>	4	ĸ.	•	_	<b>c</b> c	6	01	21:	3		HARMUNIC	c	-	2	<b>.</b>	4	ĸ	•	7	œ	Φ	1.0

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0.400	¥.	RH0100	<b>= 0.2175</b>	S CP/S	s = 0.000919	1919 CDR/S,R	=0.01622	CMX/S.R	+0000*0-= 1
		! <b>!</b>							
	ROTOR	BLADE	E NORMAL	<b>6</b>	MOMENT	UR EDGEWISE	UR PITCH		UPPER ROTOR
	4		4	•	Ś	•			
9-	887.	-2	485.	-2777.	-3394.	•	-50	.00	-1524.
-56	33	-2	132.	-2726.		•	-3	384.	-1271.
4-	89	1-	580.	-2305-	-2774.	•0	-38	97.	51.
14-	30	Ī	•	-1563.	-1972.	•	-31	318.	1261.
7	6			-1045.	-2434.	•0		-33.	1220.
•	33	-	132.	-798.	-2381.	•	22	28.	767.
7-	_	-	533.	-318.	-1457.	•	7	117.	1603.
<b>–</b>	7	~	194.	447.	-1976.	•	31-	85.	3607.
4	183.	W	809.	1049.	-3679.	•	-23	35.	5107.
S	362.	4	864.	1252.	-3817.	•	11-	.119.	6040
e	580.	4	208.	1112.	-2425.	ं	-12	126.	7715.
7	2837.	m	3346.	869.	-1999.	•0	961-	96.	9241.
4	567.	m	864.	944.	-3106.	•	-253	53.	8415.
9	6067.	Ñ	030.	1449.	-4119.	•	-31	18.	5883
Ś	5867.	ķ	470.	1868.	-4003.	•	-28	-283.	4198.
4	4601.	4	954.	1674.	-3009.	o	-19	92.	3956.
7	516.	E)	199.	986.	-1502.	•	-54	46.	4130.
	187.	Ż	437.	378.	106.	•	-37	73.	<b>4196</b>
١	-112.	Ä	669.	238.	842.	•	64-	52.	3935.
·	-47.	~	972.	398.	398.	•	-59	591.	3037.
	665.	7	466.	495.	-28.	•	-160	•09	1629.
	299.	7	391.	452.	323.	•0	51-	. 96	273.
Ī	648.		917.	296.	901.	•	-73	33.	-452.
1	962.	<b>-</b>	255.	-06-	1577.	•	-645	42.	-435
-37	710.		261.	-660	2332.	•	-119-	11.	Ō
Š	_	1	15.	-1201-	2087.	•	)8-	800.	-16.
-54	482.	1-	29.	-1718.	716.	o	-978	78.	
019-	1 08.	7	•	-2283.	-531.	•	-743	43.	-418
-68	883.	-2	404.	-2736.	-1775.	•	-417	17.	-1582.
-619	194.	-2	683.	-2933。	-3468.	•	-54	549.	-2336.
	561.		441.	-2919.	-4156.	•	-8	842.	-1896.
-1	'n		0	-2816.	-3507.	•0	-71	71.	-1374.

RUN 24 VKTS = V/GR =	PGINT 142.4 0.400	9 CMEG#R RHULOO	# H	600.4	ALFS,C	S,C = 7.9 S = 0.000919	7.9	CLR/S, R CDR/S, R	=0.09029 =0.01622	$CMY/S_9R = 0.1804$ $CMX/S_9R = -0.0004$
			!		i			•		
	LOWER R	OTOR	BLADE N	NURMAL R	BENDING 38	MOMENT	LR EDGE	EDGEMISE DING 118	LR PITCH	TCH 1 OAD
••	•	•	į	•				•		ì
9	16	30.	1341	•	790-	-546		-6964-	1	-371.
	15	10	136		987.	28		46	7-	-419-
S	26	49	1 70	2.0	1290	-406-		-5618.		987-1
N	37	6	243		1365	-478		-5268	7	-222.
0	20	45	201		798.	-493		-4739	) [	-63
~	-143	æ	-17	*	-324.	-429.		-6540	,	-48•
Ň	-34	.07.	-1974	•	-1475.	-559.		-9014.	•	-27.
7	-365	.55.	-2794		.2276.	-1017.		-9230.		•0
Ó	24-	.09	-317	•	-2806-	-1493.		-7346.		48.
	-62	.89.	-407	•	.3435.	-1697.		-6623.		56.
Ň	06-	11.	-567		-4350.	-1688.		-7580.		31.
Ň	-1398	.68	-727	•	-5156-	-1555.		-7478.		93.
ó	-114	.05	-792(	•	-5367.	-1314.		-5047.	-	119.
~	£C1-	118.	-732	•	-4716.	-1084.		-2720.	,	-26.
Ň	-82	17.	-602		-3667.	-886-		-2948.	1	-49.
7	79-	.16.	-456	- 0	.2612.	-578.		-4652.	-	120.
ó	-45	•	-317	•	-1564.	-184.		-5150.		59.
۲,	-21	٠	-177		-433.	150.		-4319.	1-	-185.
Č	6-	61.	-34(	•	659.	444		-4556.	1-	-199.
7	.7	54.	77	•	1492.	689		-6771.	1-	-129.
ó	16	~	1594		2032.	739.		-8789.	-15	53.
-	35	4	248	•	2378.	650		-8515.	1	-13.
č	31	2	294.	7.	2486.	•019		-6875.	7	140.
Š	11	0	239	7.	2237.	561.		-6228.	1	-58.
ó	11	.86	163	3.	1738.	383.		-6750.	-2	267.
Ļ	7	3	125	9•	1216.	187.		-6103.	1-	-184.
Š	01-	ø	53	7.	4	•09		-3190.	1-	-188.
Š	-19	3	-36	•	332.	-123.		-472.	-3	376.
Ó	ţ	Ø	-378	<b>5</b> •	-	-410.		-618-	<b>7</b> -	*604
~	Ð	S	33(	<b>0</b> •	180.	-655.		-2256.	-3	348.
322.50	5	.85.	142	2•	7	-737.		-2121.	-3	384.
7	51	8	1041	l.	.649	-676-		-480-	-3	91.

										!			
		. 1R	αx	<b>.</b>	UPPER RUTUR		BLADE NURMAL		BENDING MCMENT  • 3K	- Z		• \$6	
		003	SIN	<b>-</b> 9-	cos		NIS	203	NIS	z	SOO		NIS
HAKKUNIC O	-105	8 0			1227.2			-466.5			-1593.1		
-	-476	3.1	2884.	-	-3080.7		30.7	-1882.6	589	۳.	-438.2	ı	1939.2
2	-8¢	-833.6	-349.	,2	-614.3		75.7	-506-0	35	•2	-1317.2		17.0
т.	11	164.9	367.6	9	26.3		246.1	<b>+.9-</b>	153.7	.7	-433.2		103.3
4	7.1	172.9	-723.4	4	286.4		349.6	172.4	-154.5	• 5	1-14-1		9.58
<b>~</b>	-41	13.4	493.0	<u>ن</u>	-291.7		215.4	-125.3	104	0•	354.4	•	394.9
9	. 7	26.4	-487.	80,	105.3	1	41.5	0.6	-187.1	.1	104.8		90.5
7	36	324.8	34.		. 166.8		70.3	57.8	S	5.0	-177.6	•	12.4
80	11-	-116.1	320.7	.7	-80.2		77.5	21.6	1.04-		81.0	7-	25.8
6	-417		-86.	ñ	-130.8	1	04.4	6-5-	97	•3	248.4	1	55.7
10	9	7-1	-75.	ó	-15.3	•	10.2	4.6	23	<b>.</b>	84.4	•	53.0
	UPPER		ROTOR EDGEW	-	UPPER	UPPER KUTOR	ÜR	UPPER					
	BENC	_	CHENT	* 1 *	PITCH	ž	LOAD	SHAFT	SIKESS	v.			
		cos su	NIS	•	002		NIS	CUS		) Z			
HAP MON IC													
o o		0.0			-416.4			2030.7					
		0.0	o	0.	-65.1	'n	56.1	-2848.2	2653.	• 5			
2		0.0	0.0	0	-10.4		54.2	-390.0	-959.4	4.			
3		0.0	•	0	-103.5		17.0	329.2	56.9	6.			
4		0.0	ċ	o,	4.0-		18.0	-631.3	863.4	4.			
<b>~</b>		0.0	•	o,	-33.3		57.5	118.1	-306	٦.			
9		0.0	•	o	6.6		67.2	-71.6	47	ω.			
1		0.0	ċ	o o	28.4		105.3	-80.4	-307.8	8			
80		0.0	•	o o	23.5		40.6	384.0	161-	٠3			
6		0.0	•	0	-5.2		-2.3	36.9	20'	89			
<u> </u>													

0.1801	مد	NI S		477.6		10	~	•	-53.3	-0-1	1.1		-13.7																
CMY/S,R =	• 6k	COS	-408-1	673.7	-456.3	133.1	10.1	38.0	22.8	-29.5	13.2	21.7	6.4																
	MOMENT R	NIS		-43.5	1028.9	7.8	83.5	<b>+*691</b> -	155.5	-32.0	-8.7	-10.1	14.2																
	IAL BENDING . 3R	cos	-517.1	2765.5	-1558.1	-1.1	52.8	-87.0	2.1	37.9	13.6	4.6	-14.4																
000•0	BLADE NURMAL	NIS		-833.8	1607.7	-17.0	150.7	-305.7	337.3	-63.4	33.1	154.5	68.3	OLI	٠ د د د د د د د د د د د د د د د د د د د	C L C A U C 1 L C A U	2 7			115.5	85.3	24.6	-3.1	-22.3	-1.0	9.1	3.2	30.8	20.9
<b>4</b> 0	LOWER ROTOR .2R	SOO	-1023.8	3617.3										OMES D		PIICH LINK LDA	202		-133.9	-172.7	45.6							25.4	-5-3
= 607. = 0.217		NIS	•	-1310.1	872.8	157.	183.7	-645.1	510.2	128.0	-15.2	290.7	126.9	portion physical ce		MUMEN! . IK				-933.1	-2800.6	-53•3	-49.1	6.7				-71.6	
PGINT 10 142.5 DMEG#R 0.396 RHJ100	• 1R	0.05	-1909.2	*	-3079.3		-140.6	-274.8	-243.6	304.8	-142.8	-258.2	-59.8	CIND CHACL	STOK KUROU	E SULCIVER	202	1	-5153.4	1564.5		396.5	14.1	69.5	39.1	7.867	6.64-	-17.0	-26.1
P(IN 24 VKTS = V/OR =		J LNUN G WH	0	_	2	~	4	S	•	~	œ,		61	21	١7			HAR YONIC	C		۲.	~	4	ıc.	\$	~	æ	6	61

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S <sub>2</sub> K = 0.1801 S <sub>2</sub> K = 0.0003	<b>*</b> +	ストリ	1 5 1	1177	CCIT	n	1480.	2045.	1276.	1305.	3117.	4922.	5676.	6830.	8646.	8820.	6625.	4367	3655	3738.	3714.	3536.	3078.	1994.	486.	-589.	-703.	-376.	-546.	-138.	-63.	~	-1709.	-1949.	38
=0.09034 CMY/?	UR PITCH	LUAU	5.5	***************************************	ָ רו	_	9	-165.	162.	201.	ന	-204.	-103.	-112.	-190	-212.	-290-	-340-	-237.	-196.	-299.	-378-	-493.	-108.	-824.	-775.	-673.	-620.	-757.	-963.	-830	-486.	-466-	7	-787-
CLR/S, R CDR/S, R	UR EDGEWISE	•	C	<b>.</b>	•	•	• •	•	• •	•	•	0	0	•	• •	0	•	•	•	•	•	•	•	•	•	•	•	•	•	•0	•	•0	0	•0	•
5.c = 7.9 5 = 0.000884		• • • •	010	• 0010	0	-3170.	-2282.	-2378.	-2475.	-	-1415.	-5819•	-3761.	-2946	-2131.	~	-3923.	-4298.	-3534.	-2208.	-738.	363.	493.	129.	218.	663.	1238.	2083.	2362.	1400.	147.	-1026.	-2712.	85	45
607.1 ALFS.C	BE	• 5K	3776	-6133-	-7607-	-2416.	-1766.	-1105.	-801	-521.	109.	790.	1130.	1119.	908	804.	1121.	1628.	1713.	1186.	492.	161.	241.	361.	354.	328.	162.	-332.	-930.	7	-1989.	-2530.	-2774.	277	-2741.
UMEG*R = 60 RHU100 = 0.2		• 2K	0 7 6	<b>7</b> (	777	165	90	-110	2	52	æ	0	S	S	S	5	4527.	~	-	7	6	œ	-	~	~	0	65	832.	-203.	-886-	-1397.	0		24	11
PGINT 10 142.5 UME 0.396 RHU	UPPER KOTOR	• 1K	Č	•6880-	-	-4911.	-4405.		30	-		2849.		4275.		•	5473.	5801.	4911.	32.15.	970.	-614.	-610.	140.	321.	-250.	9	-2927.	'n	ø		-9649-	0	~	-6580•
RUN 24 VKTS = V/OR =			100	<b>:</b> -	∴	᠅	æ	•	•		8	ò	•	å	~	δ.		157.	8	180.	-:	~	ě	Š	å	<b>;</b>	8	ċ	-	å	8	ĸ.	\$	-	<b>œ</b>

/S,K = 0.1801 /S,K = 0.0003																																	
CMY/S	A O	• 99	386.	17.	16.	-139.	54.	56.	26.	62.	.16	33.	19.	.06	•99	17.	33.	81.	50.	76.	81.	51.	51.	109.	24.	.91	39.	67.	86.	22.	04.	379.	88.
=0.09034 =0.01615	LR PITCH LINK LOAD	Ę.	61	-417	7	1	1	1	ľ		-			-		1	•		1	921-	-181	1-	1	7	24.	7-	-2	-191-	-2	-45	4-	-3	-3
CLR/S,R CDK/S,R	LR EDGEWISE BENDING .IR	-616-	8	-4427.	-5458	-5564.	-6237.	-7844.	-9018	-8539.	-7323.	-7030.	-7194.	-6154.	-4234.	-3365.	-4059.	-4911.	-4918°	-4858•	-5963-	-7849.	-8703.	-1978.	-6792.	-6493.	-6288.	-4514.	-1674.	-352.	-1253.	-1962.	-1099.
7.9	L R B E																																
ħ	CAENT •6R	-630.	6	-394.	-485.	-538.	-428.	-471.	-857.	-1342.	-1641-	-1703.	-1605.	-1427.	-1218.	-466-	-703.	-308.	88.	378.	601.	743.	702.	590	572.	502.	278.	102.	-31.	-329.	-636.	-708.	-119-
ALFS,C CP/S =	BENDING MLMENT •3R	713.	837.	39	1337.	4	-20.	1154.	1111.	5.		_			-5063.	4153.	2981.	1834.	-908-	235.	1233.	1958.	2385.	2556.	2400•	1985.	1498.	1008.	561.	266.	æ	330.	571.
607.1 0.2175	ORMAL	•	•		•	*	3.	,	'	,																		4	3.	•	·	<b>4.</b>	:
5#R = 1000 = 1	BLADE N •2k	1150	1375.	1483.	2044.	~	693.	-155	27	-3159.	3	52	3	78	-7715.	•	50	3	2	-916-	724	1424.	2295	3014	2801.	193	1457	366	23	-361	529	724	824
10 OMEG*R RHO100	ROTCR .		3.4	7	. ^	861.	_	10			~		~	_	9	8	$\sim$	3		. ^	-	Ø	4	S	6	14	œ	$\infty$	91	4		6	37
POINT 142.5 3.396	LOWER	<b>~</b>	<b>~</b>	ã	ř	284	Í	-3	-3	4-1	-5	1.03	~	-11-	01-	6-	1-	-5.	Ř	1-		7	Ñ	ลั	73	` <del>`</del>	Á	•	) <del>1</del> –	Ĭ		•	ä
RUN 24 VKTS = V/OR =	V	0.00	88.7	77.5	66.2	,	43.7	32.5	21.2	10.0	98.7	87.5	76.2	65.0	53.7	45.5	131.2	20.02	08.7	7.5	6.2	5.0	3.7	2.5	1.2	0.0	8.7	.5	56.2	45.0	-	22.5	11.2

ſ

= 0.1025 =-0.0174	70°	SIN		-1331.9	-461.6	483.4	880.3	-612.2	430.6	2.8	-105.3	•	-3.5															
CMY/3, K	•	SUS	9-6067-		-593.5	496.3	720.0	325.9	153.9	-216.0	6.46-	-143.4	-4.7															
=0.08466 =0.00762	MUMENT	SIN		1135.4	-735.7	6.07	-232.7	206.5	-239.1	9.04-	-4.1	-12.1	17.1	RUTUR	STRESS	SIN			-2462.8	-111.9	159.7	805.9	-310.4	<b>4.</b> 8	-217.9	-113.8	-12.6	-58.5
CLK/3, K CUR/5, R	NE BENDING MUMENT	cos	-2333.H	4.628	-415.2	-42.1	1.9	-136.9	-33.7	52.9	-18.5	24.3	17.2	UPPER		cu,		2424.1		-535.1	544.1	-54.9	152.8	26.1	-303.5	18.4	83.7	10.9
2.8	8 BLADE NURMAL	NIS		2141.7	-1227.1	-43.4	-569.6	371.9	6.944-	28.6	58.7	97.0	-1.7	ROTOR	NK LUAD	žIS			215.3	118.8	-10.2	-7.4	9.011-	29.3	22.9	37.6	33.9	-6.8
ALFS,C CP/S =	UPPER RCTOR	cos	0.580	) <b>4</b>			-122.8	-379.4	21.9	141.8	6.4-	33.6	21.7	UPPER ROTOR	PITCH LINK LUAD	SOO		-564.0	49.1	-100.4	-17.1	-84.5	84.3	-3.8	60.1	4.4	9.01	-17.2
UMEG*K = 603.8 RHUlû∪ = 0.2137	ا م	NIS		-247-0	-725.8	-403.4	19.7	-78-4	-10.9	103.8	-40.4	71.5	39.7	RCIOR EDGEMISE	~	SIN			0.0	0.0	0.0	0.0	0•0	⊙•0	0.0	0.0	0.0	0.0
PUINT 11 160.6 UM 0.449 RH		• 500	0 00707	6.2006+- 6.71-	8.8	-321.2	37.2	-413.1	-189.9	4-47-4	5.2	0.04-	-58° U	UPPER RCI	DNI CN38	SOO		0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
RUN 24 VKTS = V/CR =			HARMCNIC	<b>~</b>	• ~	- ~	•	٠ ٧٠	\$	~	· cc	0	1.0	220	0		HARMCNIC	0		~	· m	• •	v	•	~	œ	6	10

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<u>a</u>	LUWER RCTUR	R BLADE NORMAL		BENDING MUMENT	3	
NIS VI	C03	NIS.	C C C C	NIS	500	NIS
: •	}	:	) )		) •	;
	465.7		503.8		-271.6	
-2123.3 -5100.5		-2952.3	-762.6	-1579.6	132.0	257.6
531.	-2681.4	677.0	-2119.1	207.2	-693.0	-93.3
-487	-253.2	-231.8	-101-9	-108.0	82.8	108.0
793.	12.7	475.8	-7.2	182.4	13.8	-139.8
101.	-16.8	86.3	-27.3	6.49	3.3	-14.0
430	1.2	290.7	1.1-	130.5	13.0	-41.1
261.	149.3	-21.9	40.0	-54.7	-28.8	-16.1
-21.	-17.8	-2.6	16.7	-19.2	11.2	6.1
	-228.1	-20.2	25.3	-17.3	6.64	43.3
105.	11.8	62.0	<b>1.6-</b>	-12.0	23.7	-20.1
-	LOWER					
BENDING MOMENT . IR	PITCH LINK	_				
NIS	SOO	NIS				
	•					
1306.	-212-3	-53.7				
-920.	154.6	15.9				
<b>*</b> 00 <b>*</b>	34.7	106.4				
1.0 35.9	-21.8	-7.4				
54.	30.2	26.5				
-111.	15.8	35.3				
-480	0.2	9.4-				
-35	-28.3	-5.7				
-40•	-107.4	-6.5				
1.9	-7.2	6.9-				

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9 RHUIDO = 0.2137 CP/S = 8 K RJTOR BLADE NURMAL BENDING MOM	9 RHC	11		. = 0.003551	51 COR/5,R	<b>=0.0076</b> 2	CMX/S,R =-0.0174
PSI  - 1R  - 2R  - 1R  - 2R  - 50428  - 1671  - 2082  - 11.25  - 50173  - 50173  - 5020  - 2334  - 50173  - 50152  - 50173  - 1925  - 2142  - 50173  - 50152  - 6915  - 1936  - 1935  - 1936  - 1937  - 1938							
PSI  0.18	R ROTOR	Ž		MOMENT	E	UR PITCH	RUTU
P.S.I.       -50428.       -1671.       -2082.         11.25       -50173.       -2020.       -2334.         22.50       -50173.       -1925.       -2142.         33.75       -50152.       -981.       -1636.         35.75       -5020.       -234.       -1656.         56.25       -5020.       -172.       -1465.         56.25       -5020.       -172.       -1465.       -1366.         57.50       -49689.       1421.       -956.       -956.         78.75       -49629.       1421.       -956.       -956.         78.75       -49629.       1421.       -956.       -956.         78.75       -49622.       -1789.       -219.       -1789.       -2491.         78.75       -49622.       -1786.       -1789.       -2430.       -669.         78.75       -49824.       -1788.       -2430.       -669.       -4446.       -4981.       -7880.       -6491.       -7880.       -2491.       -7880.       -6491.       -7880.       -6491.       -7880.       -6491.       -7880.       -6491.       -7880.       -6491.       -7880.       -6491.       -7880.       -7880.       -7880.       -			• 3R	• <b>6</b> K	BENDING . IR	LINK LUAD	SHAFT STRESS
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22.50		-2020-	-2334.	-549.	•0	2	-24
33.75       -50152       -981       -1636       -3         56.25       -50177       272       -1465       -4         56.25       -50220       14       -1356       -4         78.75       -49689       1421       -1356       -3         78.75       -49689       1421       -956       -4         78.75       -49367       1246       -461       -3         12.50       -48929       1899       -461       -3         12.50       -48927       1246       -461       -3         12.50       -49824       105       -1549       -2         23.75       -49824       -219       -1789       -2         46.25       -49824       -219       -1789       -2         58.75       -49824       -218       -2483       -2         68.75       -49176       -218       -4446       -4446       -4446         75.00       -49176       -5596       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446       -4446		-1925.	-2142.	-	• •	5	-255
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56.25       -50177       272       -1465       -4         57.50       -5020       415       -956       -3         78.75       -49689       415       -956       -3         90.00       -49066       1421       -956       -3         90.00       -49066       1899       -461       -3         12.5       -48929       1899       -461       -2         12.5       -48929       1899       -461       -2         12.5       -49622       -4895       -1549       -2         23.75       -49824       -219       -1789       -2         46.25       -49824       -219       -1789       -2         46.25       -49824       -219       -1789       -2         56.00       -4915       -2186       -2483       -2         68.75       -4916       -5297       -4466       -4         75.00       -4918       -5297       -4296       -4         75.00       -5018       -5596       -4273       -5         75.00       -5035       -3560       -3569       -3569         75.00       -49397       -3549       -3549       -4<	-50082	81.	-1393	4	•	~	28
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57.50       -49315.       102.       -1785.       -6         68.75       -44776.       -708.       -2430.       -6         80.00       -48751.       -2788.       -3483.       -5         91.25       -49012.       -4816.       -4446.       -4         92.50       -49319.       -5596.       -4922.       -4         13.75       -49679.       -5297.       -4769.       -5         55.00       -5018.       -4273.       -5         56.25       -50395.       -3851.       -3851.       -4         77.50       -50397.       -3851.       -3851.       -3         76.00       -49397.       -3819.       -3549.       -3         76.00       -49457.       -3830.       -3568.       -3         76.00       -49487.       -1882.       -2763.       1         76.00       -48474.       -1682.       -2289.       -289.         76.20       -48474.       -1882.       -2289.       -289.         76.20       -47677.       -365.       -1596.       -259.	*	-219.	-1788.	4	•	-507-	3900.
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80.00       -48751.       -2788.       -3483.       -5         91.25       -49012.       -4816.       -4446.       -4         92.50       -49319.       -5596.       -4922.       -4         13.75       -49679.       -5297.       -4769.       -5         25.00       -50118.       -4586.       -4273.       -5         36.25       -50395.       -3851.       -3851.       -4         58.75       -49397.       -3819.       -3549.       -3         70.00       -49157.       -3830.       -3538.       -3         70.00       -49452.       -3143.       -2763.       1         92.50       -48474.       -1682.       -2289.       -2         15.00       -47671.       -894.       -1819.       -1         26.25       -47521.       -365.       -1596.       -2	4377	- 108.	-2430.	•	•	•006-	3928.
91.25	48751	-2788.	-3483.	R.	•	-953.	5303.
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25.00 -50118458642735 36.25 -50395385138514 47.50 -50076356036493 58.75 -4915738193538 4915738303268 12.50 -4905523402289 15.00 -4787789418191	0	-5297.	-4769.	S	•	-471.	7140.
36.25       -50395.       -3851.       -43649.       -49397.       -3560.       -3649.       -3       -3       -49397.       -3819.       -3538.       -3	m	-4586.	-4273.	S	•0	-199-	6776.
47.50       -50076.       -3560.       -3649.       -3         58.75       -49397.       -3819.       -3538.       -         70.00       -49157.       -3830.       -3268.       -         81.25       -49282.       -3143.       -2763.       1         92.50       -49055.       -2340.       -2289.       -         15.00       -47874.       -1682.       -2029.       -         26.25       -47521.       -365.       -1596.       -2	50395	-3851.	-3851.	4	•0	-128.	6273.
58.75	50076	-3560.	-3649.		<b>.</b>	-716.	S
70.00	49397	-3819.	35	-811.	•	•069-	4
81.25	49157	-3830.	32	717.	•	-649-	S
92.50	$\sim$	-3143.	-2763.	1034.	•	-677.	531
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48.75 -49475121	146	21	173		•	-120.	-455.

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	LONER	ROTUK	BLADE	NURMAL	BENDING	MOMENT	LR EDGEWISE	LR PITCH	
S		4	•			•	T. ONITON	רווא רחשו	3
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98.7	7	∞	20	.60	640.	-1376.	-5797.	108	* ************************************
87.5		vo.	1	74.	-235.	-1351.	-5425.	75.	
• 7	-2	2555.	6-	22.	-1020-	-1013.	-5189.	697	•
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٠,	-25	~	- 6	82.	53.	336.	-5003.	-151	•
Ţ.	<b>7</b> -	മ	91-	57.	-650-	150.	-3374.	-224	•
• 2	C-	78	56	68.	-1188.	-87.	-1103.	-313	3.
C	<b>7</b> -	-		93.	-1686.	-490.	141.	<u>-4-</u>	3.
٠,	<b>5</b> -	16	-30	57.	-2172.	-784.	541.	136	•
• 5	9	11	-36	58.	-2445.	-741.	1105.	-93	
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33.7	7-	S	-21	• 66	20	-556.	-408	-309	•
322.50		593.	-2	82.	4	-440.	-2397.	-493	•
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PUN 24 VKTS = V/CR =	PCINT 160.6 0.447	12 UMEG*R RHU100	ų H	606.2 0.2137	ALFS,C CP/S =	; = 2.8 = 0.003623	2.8 3623	CLR/S,R CDR/S,R	=0.08466 =0.00751	CMY/S,R	= 0.1019 =-0.0187
		a i		a D	UPPER RCIUR		BLADE NORMAL	BENDING MUMENT	MUMENT	•	89
		cos	SIN		soo	SIN		รกว	NIS ,	cos	SIN
HARMUNIC											
C	- 1455	54.3			-1397.1		ľ	-2210.5		-2865.1	
	7	•			481.6	2517.8		566.9	1451.4	1572.2	-1183.6
7	7-	•				-1064.d		-423.7	-603.4	-464.2	-584.1
~	7				1.69-	-22.2		-36.2	23.6	439.3	378.6
4	-2	225.9	411.1		-220.8	-629.5		9.65-	-271.5	917.0	878.3
\$	7		•		-321.6	471.5		-100.9	242.1	215.8	-726.3
\$	E 1	320.8	•		-91.3	-445.4		-94.6	-231.2	263.9	375.4
~	<i>5</i> 1	1910	_		151.3	-24.5		17.6	-55.8	-215.0	7.99
œ	-2		392.7		4.9	71.8		-19.1	0.5	-130.3	-91.4
6		10.9			50.2	8.66		14.5	-18.9	-187.2	-136.4
01	-2	32.	2		25.4	-5.6		14.8	0.0-	-33.5	-11.3
22	UPPER		≥ EJGEM		UPPER ROTOR	ROTOR			KUTUR		
4	BEN	BENDING MO	NG MOMENT . 1R		PITCH LINK LOAD	VK LOAD			STRESS		
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-		•	•		61.5	216.7	i	-4235.1	-430.7		
2		•			-91.6	131.4		-570.8	-730.4		
٣			•		-16.2	-11.1		474.2	-281.6		
4			•		-83.3	-1.3		68.2	877.3		
2			•		81.7	-135.0		99.5	-346.3		
9		•	•		2.5	27.7		35.3	7.4-		
1		0.0	0.0		73.4	3.7		-309.5	-138.6		
€0		•	•		20.6	30.8		30.2	•		
6		•	•		13.8	28.8		93.6	-50.9		
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!

= 0.1019 =-0.0187	<b>3</b>	SIN		322.1	-97.5	125.6	-120.4	-17.8	1.04-	6*41-	S	40.6	3.2															
CMY/S,R CMX/S,R		• SO 3	-286.7	158.3	-698.8	65.0	39.3	11.4	23.9	-12.2	6.6	36.7	6.0															
=0.08466 =0.00751	MUMENT	NIS		-1258.1	153.7	-98.7	187.2	68.2	6.051	-50.7	-13.0	6-1-	-7.4															
CLR/S,R CDR/S,R	AL BENDING MUMENT	cos cos	376.3	-422.9		-61.7	1.44-	-25.6	-45.9	55.6	17.3	33.2	-13.6															
2.8 0.003623	BLADE NURMAL	N I S		2509.4	612.7	-225.1	6.174	110.4	337.8	8.61	1-9-	-63.5	53.5	RUTOR	K LOAD	NIS			-56.7	95.0	104.0	-11.9	36.5	45.6	-15.7	-19.4	-34•0	-1.6
ALFS.C CP/S =	LUWER ROTOR		240.0	- 696.7	798.3	201.2	-83.0	-9.1	-68.5	145.1	-27.7	-222.2	-20.9	LOWER RO	PITCH LINK	COS		-92.8	-204.6	144.2	25.3	-24.6				-25.9		
FR = 606.2 30 = 0.2137		NIS		4426.7	433.5	-476.9	724.9	124.6	442.9	301.3	-35.6	-520.2	2.09	EDGEWISE	YENT . I.R	SIN			1256.9	1115.1	428.0	28.6	45.3	-127.2	-452.0	-19.6	16.0	-46.0
POINT 12 160.6 UMEG*R 0.447 RH0100	9	C0S	196 1	-1392-1 -4		·	7	•	•	9	-75.3	• 4	-123.5	LOWER ROTOR EDGEWIS	BENUING MU	000		-4047-1	7.	4	. 7	.2	80		ຕ	9.6	•	-5.2
PUN 24 PUN 24 VKTS = 14			HARMUNIC	o <b>-</b> -	2	, m	4	2	•	~	αr	Φ	CI	225	5		HAR 40NIC	Ç١		<b>~</b> :	~	4	5	\$	~	gr.	¢	6.1

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RUN 24		12 OME	-	909	ALF	ا ک <b>ۇ</b> د	~	CLK/>, K	.0846	CAY	S.K = 0.101
α	744.0	A H	± 0010H)	0.2137	CP/	3 1 1 S	23	CUK/5, R	=0.00751	CAX/	15.K =-0.0187
	UPPER :	ROTOR	BLADE	NURMAL	BENDING	MCMENT	UR ED	EUGEW ISE	UK PITCH	т-	UPPEK RUTÜK
		. I.	•	2R	• 3R	• 6R	BENDING	Ι.	LINK LUAD	A C	STRE
S											
00.0	-14	351.	7	.18	-2321.	-487.		• •	-53	36.	0
1.2	-14	2		32.	242	-531.		၁	54-	35.	5
2.5	-152	သ	17	59.	-2002-	-1286.		• •	-66	. 19	~
3.7	-15.	Ø	5	75.	~	-3302.		•	-5.	501.	-
0	~	~	Ś	25.	-1155.	-4697.		• •	7-	41.	-5105.
6.2	-148	0	ã	.09	-1150.	-4211.		•	71	29.	-5158
7.5	-15	4	ΣŪ	0	-945.	-3514.		• •	-12	23.	-707-
. 7	-	.10	_	4	-865-	-3920.		•	£ξ-	335.	1247.
0.0	~	~	~	4	-66-	-4306.		• •	04-	.50	2632.
01.2	-4	4	25.	-	-40.	-3625.		•0	50	21.	4019.
2.5	-13	53	9	26.	-597.	-2576.		ဝ	-50	21.	5855.
23.7	-148	835.	₹0	34.	-1264.	-2351.		•	-385	82.	.0669
35.0	-14:	366.	~	55.	-1452.	-3483.		ວ່	-38	<b>31</b> •	6460.
46.2	-13	415.	~	34.	-1229.	-5419.		•	-53	36.	5099.
157.5	-146	2649	<b>Э</b>	17.	-1316.	-6583.		ċ	-18	50.	4380.
68.7	-179	952.	$\sim$	48.	-2095-	-5860.		•	96-	58.	4812.
180.0	-11	NI.	5	64.	-3244.	-4137.		•	96-	54.	5859.
91.5	-1315	Ω	S	56.	-4204-	-3247.		·	-65	54.	6642.
72.5	-15	750.	-	78.	-4590.	-3689.		·	-415	15.	6657.
13.7	-14	•	æ	.10	-4396.	-4563.		ာ	964-	.96	6114.
25.0	-145	564.	14-	18.	-3949.	-5070		•	-676.	76.	5395.
36.2	-14	94	•	. 16	-3632.			•0	-76	50.	*9674
41.5	-15	0	•	33.	-3589.	-3010-		ċ	-75	50.	3543.
58.7	-154	9	2	71.	-3633.	-717.		ċ	-611	17.	3159
70.0	-160	.660	_	.64	-3453.	616.		• •	-64	41.	3448.
81.2	-160	.160	5	37.	-3039.	656.		• •	-72	21.	3482.
95.5	- 14	~	28	15.	-2662.	124.		• •	08-	.90	2564.
03.7	-133	358.	21	89.	-2412.	S		•	08-	. 80	1081.
15.0	-146	2	3	48.	-2164.	4		• •	-78	31.	-253.
26.2	-149	56	7	.66	-1922.	-2580.		•	-16	. 99	970
337.50		549.	07-	80.	-1830-	134		•	-15	50.	-1202.
48.7	-14	•	16	20•	-1661-	-489.		•	19-	72.	32

	~	12				,		77700 0 - 0	9 0737
V / 0 %   1	0.447	SH C	OMEC#K = RHOICO =	0.2137	CP/S =	3 = 0.003623	2.8 CLR/3,R 3623 COR/S,R	K =0.00751	CMX/S,R =-0.0187
	LOWER	ROTUR		NURMAL 28	BENDING	MOMENT	LR EDGEWISE RENDING . 18	LK PITCH	H. CA
U			•		•	<u> </u>	•		
000	• 1	_	36.	36.	2519.	-265.	-4126.	1-	.26.
•	1	5236.	408	•	3025.	112.	-5475.	-3	322.
77.5		95	45	S	3451.	240.	-7218.	-3	338.
66.2	-	2	52	97.	3674.	169.	-8261.	•	.27.
55.0	•	•	55	.80	3535.	116.	-1900.	7	114.
43.7	-1	Ó	43,	21.	3005.	-50.	-1504.		57.
32.5	<b>J</b> 1	-	35	70.	2157.	-486.	-8155.	7	.31•
21.2	•	4915.	31	52.	1316.	-954.	-8339	7	216.
10.0	***	3036.	22.	30.	705.	-1257.	-7005.		138.
98.7	-7	.9611	Ŏ,	<b>40</b> •	32.	-1411.	-5755.	-	.23.
87.5	ī	1187.	-3.	33.	-886-	-1359.	-5504.	7	.39.
76.2	Ĭ	4062.	7	5.	-1638.	-1046.	-4932	2	233.
65.0	ĭ	4925.	~	2.	.1778.	-691.	-3603.	<b>T</b>	138.
53.7	1	-3784.	7	7.	-1423.	-460.	-2786.	1	194.
145.5	1	3166.	_	• •	-823.	-201•	-2998•	2	
31.2	ĭ	2929.	-13	30.	-156.	139.	-3625.		-5.
120.0	Ĩ	1551.	9-	53.	429.	344.	-4280	2	281.
08.7	•	-536-	Ř	47.	950.	424.	-4844.		326.
5	•	-240•	జే	55.	1408.	579.	-5196.		-352.
.2	Ī	1229.	ğ	26.	1512.	691.	-5500.		-442.
C	ī	.1611	7	93.	1052.	565.	-5785.		-334.
	í	.8061	-5,	.0.	304.	382.	-5313.		-161.
.5	ï	.1068	-15	97.	-351.	256.	-3516.	7-	-242.
.2	7	•781·	-25	93.	-873.	-65-	-1336.	-5	269.
0	71	.000	-24	+7	-	- 504.	-175.		25.
7.	ĭ	+446.	-25	ъ.	-1911.	-120.	333.		.34•
.5	ĭ	6390.	Ġ	- 84	-2249.	-673.	1308.	7	-148.
56.2	ĭ	o	-41	17	-2323.	-699-	2248.	7-	-268•
45.0	7	63	-35	12	$\sim$	-680	1567.	7	-178.
333.75	ï	.2395.	-21	<b>5</b> •	-1144.	-612.	-422•	£-	340.
22.5		80	7	73.	292.	-574.	-2167.	<u> </u>	504.
11.2	•	S	25,	45.	1670.	-536.	-3211.	-2	:82.

98 60.	SIN 08.4 75.4 76.8 12.3 98.8 37.7	
0.1998 -0.010-	2014001 @	
CMY/S,R =	. CUS -947.8 1465.5 -836.9 -27.7 -266.8 409.5 104.9 -37.0 158.9 -83.9	
=0.10721 =0.01670	MCMENT R SIN 167.2 -381.6 90.2 -98.8 17.7 -128.8 -75.2 26.9 -7.0	SIRESS SIRESS SIN -1541.6 -467.4 -390.4 341.5 -559.6 -407.0 149.8 -47.1
CLR/S,R CDR/S,R	. BENDING MUMENT .38 SIN -71.0 735.3 167.2 -146.0 -381.6 29.1 90.2 118.4 -96.8 118.4 -96.8 -97.1 17.7 5.9 -128.8 24.3 -75.2 -0.3 26.9 -17.9 -7.0	UPPER SHAFT COS 1523.0 -1642.4 -554.3 320.6 -24.1 77.7 -40.6 -303.7 68.9 10.6
8.3 0.001613	BLADE NGRMAL SIN 600.4 611.7 130.3 203.7 81.7 81.7 50.8 -47.7	108 LOAD SIN 242.6 34.0 21.9 -98.8 99.8 61.0
ALFS,C = CP/S =	UPPER RUTUR 1670.6 837.3 -119.1 -300.5 -120.4 -120.4 -36.3	UPPER RUT COS -246.0 -44.4 7.0 -74.1 -74.1 -27.2 -27.2 -27.7 -27.7 -27.7 -27.7 -27.7 -27.7 -27.7 -27.7 -27.7
3*R = 593.8 100 = 6.2277	SIN 1356.6 -914.9 190.9 -452.0 312.3 -449.4 309.9 -63.5	OK EDGEWISE MOMENT . 1R SIN 836.6 746.0 8.3 38.5 -79.9 -79.9 -79.9 -79.9 -79.9 -10.4
PUINT 5 105.3 UMEG*R 0.299 RHUIOO	. LOS -146.3 -147.4 -147.4 -147.4 -147.4 -147.4 -147.4 -147.4 -147.4 -147.4 -123.5 -123.5	UPPER RUTOR BENDING 401 COS -5086.8 1866.4 -665.2 -6.7 -90.3 74.1 2.5 -40.7 -72.5
PUN 25 PUN 25 VKTS = 10	HAFMONIC 0 1 2 4 4 5 7 10	HARYONIC 2 2 2 2 1 0 0 1 1 0 0 1 0 0 1 0 0 1 0 0 1 0 0 1 0

A DOLLAR CONTRACT

RUN 25 VKTS = V/OR =	POINT 105.3 3.299	5 OMEG*R RH0100	G#R 100 =	593.8 0.2277	ALFS,C CP/S =	* 8.3 0.001613	3 CLR/S, R 3 CDR/S, R	,R =0.10721 ,R =0.01670	I CHY/S,R O CMX/S,R	8 8 8 0 -	= 0.1998 =-0.0103
				707	LOWER ROTOR	BLADE	NORMAL BENDI	BENDING MUMENT		•	
		•1R	2 2		. 2R	2	300	• 3R	302	89	2
HARMONIC	•		570		S S	5 7 7			Ś	•	:
0	204	$\sim$			1724.7		1337.5		-155.	S	
-	-484	~	-2487.2		' ~	1418.2	-55.8	,	138	6.	277.4
~	011-	19.5	63		~	541.9	$\circ$	332	-296.7	. 7	63.2
m	-1	•	-196.9		~	-112.2	26.1	-51	20.	.2	-3.7
•	2.	9	537.3			252.1	117.3	145	-12.	4	-85.7
\$	-25	4	105.5			1+1-1	-56.0	87	58.	<b>-</b> !	-14.9
•	ï	Ø	645.5			356.4	20.9	185	ฑ้	۳,	-66.6
~	2:	~	66			-32.2	1.61	-21	-23	4.	-4.3
80	8	2	-228.7		-87.5	-52.6	-2.1		12.	0	18.9
	7	8	52.3		-0-3	-1.2	-3.9	-21	ý	80	-1.6
10	**#	~	107.	10	40.4	8.7	6.5	-5	1.	5.	-8.6
22	LOWER	ROJ	R EDGEWISE		LOWER R	ROTOR					
	BEN	BENDING M	MOMENT		PITCH LINK	K LOAO					
	_	203	SIN		SOO	N I S					
0	-554	42.0			æ						
~	27.	11.7	299.6		5.	155.0					
7	S	75.6	-865	•	•	50.2					
ж	11	24.4	108.		7	6.44-					
4	ī	15.9	33.		5	-10.5					
ĸ		18.1	80.			-7.1					
9	Ī	4.46	85.	01	2.	23.9					
7	•	73.5	1019.6	•	•	-15.0					
œ	i	-19.6	9.3	3	-4	16.1					
<b>ው</b>	-	10.7	7. C		•	5.61					
10		0.3	7.07	_	•	10.1					

FUN 25 VKTS = V/CR =	105.3 105.3 105.3	UMEG RHU1(	UMEG*K = RHU100 =	593.8 0.2277	ALF CP/	S = 0.	4.3 CL	CLR/S, K CDR/S, R	=0.10721 =0.01670	C.4Y/5, R C.4X/5, R	R = 0.1998 R =-0.0103	
	UPPER	ROTUR	BLADE N	NURMAL	BENDING MOMENT	MOMENT 6R	UR EDGEWIS	WISE PAR	UR PITCH	^	UPPER KUIGK SHAFI SIRESS	
V		•	•	<b>:</b>								
00.0		347.	S	7.	624.	45.		S	-36	.6	-581.	
1.2		4-			8	-7-	6-	922	7	7.	4	
2.5		~	. 0	.2.		O	€-	40		9	619	
•		85	242	.25.	360.	172	-2	9	2	5.	32	
5.0		3		0.	333.	*	7	608.	<b>7</b> -	. 6.	25	
6.2		1	Ø,	.92	156.	-1629.	-2	:064.	30	.61	36	
7.5	1	106	0	11.	28.	-2170.	€-	1251.	90	1.	16	
8.7	7	07	~	.5.	46.	-2210.	E-	1581.	8-	.0.	7	
0.0		4	~	17.	307.	-2311.	£-	1172.	-31	5.	7	
1.2	2	•		15.	507.	-2860.	£-	1726.	-22	• 0:	214	
2.5	2	5	0	.0.	207.	-2722.	<b>3</b> -	.025	5-	.1.	19	
23.7		29		15.	-235.	-1441.	91	539.	6	.21	$\circ$	
35.0	1-	32	σ	•0•	-277.	-401-	91	.197	•	.2.	50	
46.2		0	3	1.	-206-	-2407.	9-	220.	11-	0.	2040.	
51.5	7	_	231	9.	-344.	-4084	-1	,369.	<del>- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1</del>	.4.	613.	
68.7		~	σ	•0•	-497.	-4063.	80-	1532.	-12	.0.	209	
80.0	1-	Δ	94	.7.	-724.	-3408	30	1238.	-11	3.	493	
91.2	-2	9	32	•	-1175.	9	9-	.686	-21	3.	4087.	
2.5	-3	3434.	-35	•	-1517.	20	9-	272.	-19	. *	3899.	
13.7	<b>7</b> -	5	-87	•	-1501.	-1341.	9-	.119	-29	.2.	569	
25.0	-2	90	$\sim$	•	-1248.	4	9-	.926	44-	Э.	•	
36.2	-1-	œ	49	.4.	-824•	Š	9-	053.	L 4 -	.4.	200	
47.5	-1-	80	81	7.	-397.	-31.	7-	933.	-50	.60	$\sim$	
58.7	1-	27	0	15.	-194.	943.	3-	093.	-54	.64	0	
70.0	Í	O	S	.6	-19.	1450.	<b>5</b> -	938.	-40	.2.	53	
81.2	7-	53	-	.7.	288.	2676.	-5	738.	-31	.7.	8	
95.5	-1	1361.	S	.4.	3	46	<b>4</b> -		-54	5.	01	
03.7	ł	Ø	œ	.7.	~	99	<b>7</b> -	.401.	99-	.90	20	
15.0	•	90	2	.6.	433.	1731.	5-	324.		.61	9	
26.2		92	3	. *.	4	16	5-	136.			~	
37.5		113.	270	.5	2	97.	4-	4786.	-39	.90	1517.	
48.7	<b>નં</b>	41	Q.	75.	868.	-517.	£-	i	-50		3	

L	POINT	5	1		,	9		-
V/08 =	105.3	RHOI 00	0 = 0.2277	.8 ALF3,C	o, c = 6.5 5 = 0.001613	CDR/S,R	=0.01670 CP	CAX/S,R =-0.0103
	LOWER	ROTOR BLA	BLADE NORMAL	BENDING .3R	MUMENT • 6R	LR EDGEWISE BENDING . LR	LR PITCH	
S		t	ı	<u>;</u>	•	•		
00.00	4	49	ဘာ	2089.	-327.	-4365	-209.	
88.7	4	90	3141.	2106.	0	20	-158.	
77.5	4	8	8	2332.	-129.	31	-272.	
66.2	•	_	ഹ	2750.	-225.	12	-281.	
55.0	Ó	5	ထ	2934.	-272.	-6748.	-72.	
43.7	S	75	~	2653.	-151.	-8723.	57.	
32.5	m	5	3142.	2148.	-103.	-8743.	34.	
21.2	4	S	-	1799.	-290-	-7353.	51.	
10.0	4	40	2883.	1700.	-550.	-1116.	133.	
98.7	er.	75	2817.	1595.	-126.	-8538	.102	
87.5	2	13	2183.	1203.	-753.	-9225.	218.	
6.2	-	51	1201.	.919	-638.	-7630.	151.	
65.0		1	373.	238.	-459.	-5596•	91.	
53.7	1	630		236.	-290.	-5624.	130.	
142.5	Ī	68	₹	380.	-130.	-6997.	174.	
31.2		19		544.	-1-	-9869-	175.	
120.0		40	.669	866.	82.	-5293.	191.	
08.7		10	16	1273.	182.	-4447.	177.	
.5		899.	1302.		302.	-5594	132.	
5.2	-	25	43	1603.	370.	-6699-	170.	
5.0	7	0 53	49	1508.	415.	-5854•	232.	
3.7		51.	0	1225.	473.	-4104.	194.	
2.5	1	416	461.	918.	432.	-3733.	100	
1.2		Ω	422.	851.	222.	-4451.	-46.	
0.0		7	824.	983.	-62.	-4040-	-219.	
8.7	-	25	1223.	1062.	-265-	-5014.	-222•	
7.5		1193.	3	959.	-375.	-825•	-101-	
56.2		99	887.	682.	-316-	-1694.	-166.	
45.0		49	377.	7		-5833.	-308-	
•		956.	575.	5	2	54	-767-	
22.5	7	2	1546.	Ø			-526.	
11.2	7	996	9	1847.	-358.	-2181-	-282.	

• K = 0.1385	.6R SI 5 -3437 6 438 6 438 0 556		
CMY/S. K CMX/S. R	CUS -1076. -66. -1776. -691.	137.7 10.6 142.6 147.1 39.3	
R =0.06654 R =0.01263	BENDING MUMENT • 3R COS • 3R 163.8 039.3 - 1394.6 548.1 61.1 57.8 61.1 57.8 246.9 - 147.7	-53.0 -27.9 -27.9 -25.6 -7.6 16.3 KUTUR STRESS SIN	-17.6 -411.1 -80.1 378.5 -266.4 -21.2 -245.5 146.5
0 CLR/5, R 2 CDR/5, R	1 → 1	49.3 8.7 8.7 14.5 3.7 UPPER COS	1074.0 -5660.9 -694.7 398.8 -283.2 -407.9 -74.2 -256.5 18.6
C = 8.0 = 0.000632		21.1 -92.4 -42.6 21.1 -24.7 9.4 8070R NK LOAD SIN	253 1 1 8 8 4 1 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
.9 ALFS,C	UPPER RUTUR • 2R CUS 1558-1 -1742-3 - -686-9 153-8 513-1	95.5 -112.3 -97.5 -10.7 UPPER RU PITCH LINK	-236.5 -90.8 -22.8 -66.1 -72.1 -32.4 -66.3 -44.1
CMEG*R = 593.9 RHG100 = 0.2272	-1596.7 -217.1 -542.1	<u>Ģ</u> <del>∑</del>	493.1 509.7 -83.9 -116.2 -388.4 47.5
PUINT 6 106.2 CN 0.302 RF	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	111.0 -142.8 32.2 -244.4 -230.9 -47.5 UPPEK RUI BENGING	-5368.0 2027.3 1162.6 -15.0 24.5 -1.1 498.7 -0.7
RUN 25 VKTS = V/CR =	HARMONIC 0 1 2 3 3	232	HARMONIC 0 1 2 4 4 7 7 9 9

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RUN 25 VKTS =	P 01 NT 106.2	6 UME(	# C	593.9		"	8.0	CLR/S,R		CMY/S,R =		
V/0R =	0.302	RHU100	= 001	0.2272	CP/S =		0.000632	CDK/S,R		CMX/Syk =		
		<u>a</u>	~	<b>.</b>	LOWER ROTOR		BLADE NORMAL	NE BENDING MUMENT	MUMENT	, 30	¥	
	J	cos	NIS	-	cus	<u>:</u>	NIS	SOO	NIS	S 503	NIS	
HAPMONIC	-7073	93.9			-4716.4			-3114.9		-166.1		
· ~		109.3	1902	1	366.1	1557	57.2		1372.6		501.9	
۰ ۵	1	-414.6	960.7		-215.9	ı	648.0	-201.7	380.7	-60.2	31.5	
m		31.2	80.8	ဆ	120.6		37.2	1.06	27.8	9.89	6.94-	
4	-157	57.5	348.3	۳,	18.5	7	22.5	27.6	8.601	15.2	6.89-	
· w	7-	-112.3	-517	3	-179.6	1	53.5	-62.4	-123.2	19.8	62.6	
• • •	-2	-287.1	420.2	-2	-37.1		9.06	-46.2	132.5	20.5	-46.3	
~	7	160.5	92.0	0	88.3		31.6	34.3	46.1	-15.2	-7-1	
က	1	-25.4	-76.	9	-23.2		-9.2	5.3	14.5	1.1	4.5	
o	9-	1.49	146.2	7	35.1		57.5	6.6	-7.2	10.6	-17.6	
10	-	24.4	63,	9.	27.9		24.6	-12.0	23.9	2.8	-11.5	
:												
233	LOWER	R ROTUR	R EDGEW	EMISE	LOWER ROTOR	ROT .	OR					
1	BEN	BENDING MOMENT	OMENT	•	PITCH LINK LUAD	¥NT.	LOAU					
		0.05	SIN	7	COS		SIN					
HARMONIC												
C	-4568	٠,			-162.1							
-	4		-1296.6	9.	-117.1	7	124.7					
7		51.5	<b>-449.4</b>	4.	24.0		27.8					
٣	·	-8.3	-20.9	6.	-17.9		-6.2					
4	•	25.8	-12	4.	-1.8		9.5					
2		10-7	22.9	6.	6.61-	1	27					
9		-1.9	-13	۲.	24.6		33.0					
7	-1	-777-2	1016.9	6.	36.8	'	27					
89	ŧ	-15.5	6-	7.6	-11.1		15.2					
6		5.5	-50	6.	5.9		7.3					
10		-6.3	-1.	9•	32.6		21.3					

Contraction of the Contraction

RUN 25 VKTS =	POINT 106.2	6 OMEG*		593.9		"	8 • 0	CLR/S.R	=0.06654	CMY/S,R	'S,R =	0.1385
œ	0.302	RHU1 00	<b>#</b> 00	0.2272	CP/S =		00632	CDR/S,R	=0.01263	CMX/	'S,R #	0.0028
	UPPER	TOR	BLADE	NURMAL	BENDING	MOME	~ ·	SIM		H	UPPER	
		¥.	.2K	<b>~</b>	• 3R	• 6R	BEND	ENDING . IK	LINK	LUAD	SHAFI	
ISd												
0	-3	737.	-43	8.	1461.	-3506-		-1645.	Ϊ,	549.		-5870.
1.2	-3	65.	0	- 0	~	358		-2392.	<u>;</u> -	7		-5517.
2.5	4-	58.	_	7	215	-3060		-2974.	1	-21.		-4472
3.7	- 5	. **	Ň	1	220	192		259				
50	-5	37.	~		206	-1635.		-2395.		46.		-2804.
56.25	-34	27.	-100		~	-2411.		-3500.		87.		-2772.
7.5	-2	05.	-182	'	-1464.	-3142.		-5087.		-6-		-2218.
8.7	-1,	3	64		-1054.	-3629.		-5743.	•	-65.		-429.
0.0	•	9	116	•	-760.	-4055.		-5631.		56.		1688.
01.2	•	9	149	2.	-169-	-3819.		-5979.	.=•	125.		3367.
12.5	1	337.	114		-804-	-2923.		-7004-		28.		4885.
23.7	ī	~	191	•	-870.	-2514.		-7567-		12.		6024.
35.0		39.	116,	2.	-623.	-3104.		-7032.	-	131.		.,519
46.2	<b>-</b>	446.	207	•	-167.	-3948		-6335.		116.		5543.
157.5	7	242.	267	• 6	138.	-4257.		-6471.	•	- 55.		4940.
8.7	7	2205.	280		270.	-3865.		-6945.		15.		4966.
180.0	7	759.	279	•	435.	-2943.		-6676.		130.		5833.
91.2	<b>-</b>	.604	278		.109	-1712.		-5780.	•	-99-		.6050
02.5	-	447.	283	•	731.	-363.		-5458	7	455.		5884.
13.7	4	810.	309	•	987.	923.		-6317.	1	585.		4902.
25.0	2.	308.	352.		1383.	1964.		-7341.	•	201.		4847.
36.2	2	938.	405	•	1758.	2633.		-1249.	ï	542.		4811.
47.5	<b>C</b>	537.	454	•	2056.	3018.		-6553.	ĭ	637.		3704.
58.7	Ä	473.	415	9.	2	3456.		-6691.	ī'	-556.		2356.
70.0	2	572.	431	•	2	4005		-7424.	Ĭ	419.		1586.
81.2	4	564.	361	• 9	1673.	4146.		-7252.	ī	4		192.
92.5		552.	285	5.	•686	3696.		-6056	Ĭ,	S		-561.
03.7	1-1	1	1 78	9.	219.	3023.		-5090	ĭ	.069		-1959.
15.0	-2,	_	121	•	-351.	1804.		-4805-	•	595.		-2694.
26.2		9	450	• 0	0	-485.		-4426.	1	390.		-2970.
37.5		934.	09	5.	-783.	-2722.		-3336	1	374.		-3718.
48.7	-2		24	5.	108	-3513.		-2027.	1	559.		•

RUN 25 VKTS =	PUINT 106.2	6 DMEG#R PHOLOGO	# C	593.9		ALFS,C =	8.000.00.00.00.00.00.00.00.00.00.00.00.0	CLR/S,R	=0.06654	CMY/S,R	= 0.1385	
:	ON ER	ROTCR 6	ADE	•	BENG	MCME	~	LR EDGEWISE				
	•	<b>1</b> × 1	.2R	~	.3R	.6R	BEN	-	LINK L	LOAD		
PSI												
0.00	-95	.16	-6610	۰ ۰	4567.	-1199.		-4078	1	316.		
88.7	46-	9	-661	2	4595.	-1237.		-3092	1	325.		
77.5	-87	19	-623	•	425	-1266.		-1948.	Ī	2		
66.2	-14	75	-5555	,	3907.	33		-2888-	-3	3		
55.0	71-	0	-519	B. I	3946.	~		83	7	151.		
. 7	-84	27	-566		-4193.	0		•	7	-175.		
32.5	- 89	57.	-620		4263.	-976-		-3533.	T	278.		
21.2	-16	17	-587	1	4093.	-1001-		-3234.	1	222.		
10.0	-63	30.	-504		3773.	-1262.		-485ª	•	-84.		
98.7	<b>4</b> 9-	24.	-465		3516.	-1298.		-6100-		48.		
87.5	-74	41.	-498		3596.	-1178.		-5285.		.16		
76.2	E8-	58.	-555		3842.	-982.		-3918		-35.		
65.0	-85	69	-580		3795.	-815.		-4280.	1	120.		
53.7	- 78	55.	-550(		3430.	-720.		-5934.	•	-20.		
42.5	-65	83.	-4114		2973.	-671.		-6388•		18.		
31.2	-55	50.	-393		2462.	-610.		-5077.		-54.		
20.02	-52	70.	-338		2328.	-470.		-4306.		-24.		
08.7	-54	39	-330(		1845.	-276.		-5590.		<b>.</b> 6		
.5	-53	84	-332		1756.	-141-		-7105.	•	-80.		
.2	-53	.19	-3115		-1598.	-06-		-6536.	•	115.		
0	-48	.61	-288		1478.	-65-		-48a4-	•	-77.		
. 1	-45	٠	-2116	,	1443.	-184.		-4874	•	-80•		
5	-45	ð	-266	•	1472.	-313.		-6440-	•	-09-		
.2	<b>55</b> -	90.	-271	1	1623.	-380.		-6747.	,	-73.		
0	-5362	62.	-3016	•	1828.	-434.		-4959.	ř	218.		
	-50		-3360	•	2041.	-522.		-3532.	7	276.		
Š	99-	.69	-389	•	2476.	-538.		-4114-	1	Φ		
56.2	-81	05.	-486(	•	.3131.	_		-5054.	ì	245.		
45.0	18-	$\circ$	- 5629	,	3626.	-641.		-4238.	1	368.		
33.7	-85	-	-574	'	3836.	-854.		-2373.	ľ	339.		
322.50	-87	54.	-5812.	'	.4004	-992.		-1854.	1	311.		
11.2	3	75	-624	•	4285.	-1094.		-3163.	•	551.		

CMY/S,R = 0.1973 CMX/S,R =-0.0051	-230.9 -230.9 -234.1 -234.1 -1529.0 -2463.6 -234.1 -167.4 -167.4 -167.4 -11.1 -332.1 -196.3 97.3 -196.3 97.3 -196.3 -172.8 -59.2 -172.8 -152.0 -63.3 -11.5
=0.10581   =0.01620	BENDING MOMENT  .3K. COS .3R. SIN  774.4 .955.3 -476.0 785.9 -668.2 -32.7 -29.2 94.3 -129.8 -24.7 31.6 47.0 -128.2 -6.9 -11.8 40.9 -27.2 -6.9 -11.8 40.9 29.2 CUS SIN  738.8 40.9 -539.1 209.2 -37.1 276.0 -539.1 276.0 -542.7 -21.9 -241.2 -4.1 -18.7
CLK/3, K CUR/3, R	
ALFS,C = 8.3 CP/S = 0.002266	PER RUTCH BLADE NURMAL  COS SIN  2843.5 740.1 -1020.9 -1034.7 -63.8 49.0 246.0 -225.7 -159.5 141.2 160.1 -258.6 59.2 -118.2 -99.2 174.7 -14.8 -70.7 10.0 UPPER RUTUR  UPPER RUTUR  COS SIN -227.9 -127.9 -127.9 -162.2 273.7 -144.6 -59.9 -100.5 -117.8 -59.9 -100.5 -24.9 -100.5 -2.3 -26.1 -0.7 -25.6
PUINT 7 104.7 UMEG*R = 590.0 0.300 RHUIOU = 0.2269	UPPER SIN C CUS CUS CUS CUS CUS CUS CUS CUS CUS C
RUN 25 VKTS = V/OR =	HARMONIC 11 236 H ARMONIC 12 8 9 1 5 8 9 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

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RUN 25	PUINT	7		0 005			α II		8.27.012	9	05.81	# 8'5/AE	0.1970	
	0.300	RHU100	1 II	0.2269		CP/S =	0.002266		CDR/5, R	=0.01620	1620	CMX/S,R =-	=-0.0051	
		Š		-	LOWER ROTOR		BLADE NORMAL		BENDING MOMENT	MOME	⊨ Z	V		
	ر	¥1.	2	-	<i>3</i> 00	¥7•	2		76. Cos	2 I	2	<b>50.5</b>	Z Z	
HARMONIC	<b>)</b>	3	÷		3	<b>)</b>			3	;	•	)		
0	25	52.1			468	٤,			475.6			-260.4		
~	-1735.	7.	349.	7	-982.8		1.1.49	1	-550.1	762	4.	81.3	483.3	
2	-1139	0	453.	ro c	-833		409.8	1	-724.9	228	9•	-323.4	34.0	
~	<b>~1</b>	7.	216.	7	80	,	-175.0		28.7	-51	•1	28.5	0.5	
4	206	7.	819.1		309.5		372.6		139.8	173	•5	-69.5	-140.9	
2	-138	٠,	69.0	ن	-40		52.3		7.7-	42	1.	3.3	8.6-	
•	61	4.	682.9	6	285.1		290.9		101.2	175	0.	-30.5	<b>+•09-</b>	
7	23	5.0	47.	٠. د	115		-27.9		48.8	0.1	••	-28.1	0.3	
s,	-10	5.7	6.16-	5	6.69-		20.6		12.5	13	.7	14.5	4.2	
6	10	6.5	201.	7	55	5.5	24.0		-27.4	-40.7	.7	-12.6	-17.1	
10	•	3.2	81.	.7	17	80	26.8		-3.9	6	4.	-4.2	-9.5	
23	LOWER	RCI	FUGE	W I SE	07	LOWER RO	RUTOR							
7	BENC		ENT	_	P 1 TC	PITCH LINK	LCAD							
	<b>J</b>	cos	SIN	-	COS	S	NIS							
HARACHIC														
0	-515	2.2			-39	•2								
	2430	*	317.	ν	-182.5	٠,	161.2							
2	196	· -	886.	ဆ	-18		34.4							
€	M		125.	מ	-17		-53.1							
4	7-	• 5	-22.	۲.	-2.6		-0.5							
2	9	_	163.1	~	21	21.2	-14.5							
9	-95	.2	-27.0	o,	57		14.2							
7	77	. 2	11111.2	ې	7	. 1	-5.0							
<b>c</b> c	09-	æ.	1-61-	<b>-</b>	-14.5	٠,	20.2							
6	<b>*</b> -	1.5		oʻ	0	÷3	-23.3							
10	•	S	34.	4	0	9.	<b>8</b> •1							

t

RUN 25	PLINT	~				•		•	
VKTS = V/CR =	104.7	CMEG*R RHU100	.4R = 590.0 .00 = 0.2269	) ALFS,C 9 (P/S =	)( = 8.3 = 0.002266	CUR/5, K	=0.10581 CM =0.01620 CM	CMY/S,R = 0.1970 CMX/S,R =-0.0051	
	UPPER	TOK		NDING	MOMENT	7	UR PITCH	UPPEK KOTOR	
	•	. I.R	• 2K	• 3K	¥ 0	BENDING .IK	LINK LUAD		
SI									
0		557.	2790.	852.	-1357.	Ø	-368.	ထ	
1.2	ì	5	1942.	239.	-1606.	-647.	• <b>1 5 7 7</b>	7	
2.5	Î	168.	1618.	-104.	-2150.	-1163.	-280.	85	
3.4	•	0	1901	0	-2281.	83	17.	_	
5.0	•	•	2260.	(ل)	-1781.	~	-11-	-643.	
2.9	4		2464.	555.	ന	21	-114.	3	
7.5	7	184.	2863.	685.	-1269.	-3344.	4I.	-375.	
8.7	Ň	_	3425.	897.	16	-5172.	22.	٠	
0	2	(C)	3671.	1142.	-561.	83	-210.	2	
01.2	ň	~	3838.	1317.	-682.	-6126.	-155.	3901.	
12.5	÷	145.	4044.	1085.	-970-	-1377.	-2.	4554	
23.7	7	~	3372.	543.	-563.	-4006-	-57.	5407.	
35.0	,	0	2105.	317.	-504.	59	-45.	5872.	
46.2	<b>J</b>	$\sim$	2047.	366.	-2355.	-8361.	1.	5004.	
57.5	7	ဘ	2904.	136.	-4585.	-8394•	-84•	3497.	
68.7	Ĩ <b>1</b>	*	2588.	-260.	-4770.	-9234.	114.	3009.	
80.0	ĩ	•	1289.	-524.	-3811.	-8720.	491.	4171.	
91.2	-1-	ın	614.	-807.	-3406.	-6627.	351.	5354.	
202.50	1-	~	441.	-966-	-2802.	-4881-	-119.	4726.	
13.7	-21	m	387.	-724.	-1573.	-4776.	-320.	3411.	
25.0	ĩ	O	1161.	-106.	-781.	-5650.	-406.	3485.	
36.2	7	167.	2482.	572.	-38•	-5713.	-555.	Q.	
47.5	-	O	3239.	1205.	ø	-4538	-610-	-	
58.7	1		3586.	1647.	3400.	-4041.	-626•	ň	
70.07	ý	$\sim$	4134.	1978.	4369.	-5525.	-588	1758.	
81.2	m	$\neg$	4640.	2399.	13	-6333.	-434.	•	
92.5	Ř		4841.	2622.	2	9	-504	1973.	
03.7	ň	*	4776.	2386.	28	3	-119.	-	
15.0	Ň	980.	4386.	2051.	36		-695.		
26.2	2.	0	3927.	1854.		-4863.	-355.	-1410.	
37.5	.2	~	3744.	9		-3618.	-260.	-1520.	
48.7	ã		3506.	29	2	83	-316.	22	

RUN 25 VKTS = V/OR =	POINT 104.7 0.300	7 OMEG*R RH0100	# 00 H H	590.0 0.2269		ALFS,C = 8.3 CP/S = 0.002266		CLR/S,R CDR/S,R	=0.10581 =0.01620	CMY/S,R = 0.1970 CMX/S,R =-0.0051	
	LOWER	ROT OR B	BLADE	NORMAL	BENDING	BENDING MOMENT	LR EDGE	EW I SE	LR PITCH	<b>.</b>	
				2R	.3R	• 6R	BENDING	_	LINK LOAD	ON	
PSI		l									
0.00	. •	219.		5.	-75.	-678.	7	-4155.	-233	33.	
88.7	7	.04.	<u>-</u>	75.	-60.	-601.	1	5176.	-20	35.	
77.5	7	.102.	7	44.	166.	-454.	71	-4805.	-29	93.	
66.2	J	954.	25	.99	558.	-417.	71	-4878.	-29	97.	
55.0	21	145.	123	33.	732.	-454.	7	-6581.	-14	.7.	
43.7	16	1624.	~	65.	605.	-405.	ì	-8219.	<b>5</b> -	.5.	
32.5	•	448.	99	.69	424.	-357.	ī	-1741.	•	-3.	
21.2	J	343.	4	31.	332.	-511,	7	-6430.	4	43.	
10.0	24	•90	36	73.	407.	-800	7	-6773.	•	54.	
1	25	2913.	162	620.	626.	-965.	7	-8103.	14	42.	
87.5	77	.161	148	484.	674.	-887.	1	-7948.	23	38.	
76.2	4	.161	7	57.	393.	-999-	Ĭ	-6159.	14	41.	
65.0	7	146.	77	214.	163.	-424.	7-	-4064-	1	17.	
53.7	7	œ	<b>1</b>	31.	346.	-189.	ï	5579.	01	36.	
42.5	7	177.	ň	•	804.	<b>1</b> .	ī	-7030-	91	57.	
31.2	16	69.	114	•	1278.	87.	17	7014.	10	55.	
20.02	21	.07.	205		1702.	152.	1	5629.	18	34.	
08.7	24	2440.	233		2011.	301.	1	-5412.	25	258.	
•5	7	.12	218	•	2113.	450.	ĭ	-6905-	10	.60	
	51	.92	205	94.	2044.	512.	-	-1490.	•	62.	
0		.041	185	75.	1860.	543.	7	5047.	77	.61	
. 7	. 7	111.	129	99.	1478.	533.	7	-4726.	20	04.	
Š	ĭ	.22.	519	19.	873.	398.	7-	-4931.	1	14.	
.2	611-	.06	:T-	38.	320.	170.	4)	-5161.	-101-	.10	
0	-12	4	-409	.60	116.	-109.	ĩ	.3797.	-508	.60	
	9	81.	-5(	208°	103.	-433.	1	1727.	-265	.25	
.5	-10	_	761-	94.	-147.	-628.	-	-1110.	-180	30 <b>•</b>	
56.2	-28	355.	701-	27.	-715.	-551.	, <del>,</del> ,	-2162.	-164	64.	
45.0	14-	Ó	-20	71	~	-401	7	2718.	-29	•00	
333.75	-34	Š	7	89	-1357.	-401-	7	-1691-	-32	26.	
25.5		966	-156	97.	95	-518.	•	-883.	-28	83.	
11.2	9		-67	77.	-373•	-625.	-2	0	-21	.61	

CMY/S,R = 0.2138 CMX/S,R =-0.0055	89.	7	-25.6	-1187.	578.1 -1259.	31.	7 249.	0 -126.	285.	-60•	48	113.	101.															
R =0.11600 R =0.01780	NG MOMENT •38			∞ -	-673.2	58.4	-78.3	-3.1	-117.7	-50.4	25.0	9.6-	23.5		STRESS	SI			-775.1	-442.8	-160.7	206.7	-553.9	86.4	-655.0	156.9	~	-7.2
CLR/S, R CDR/S, R	BENDI	2	1115.1	∞ −	-	0	105.5	•	52.4	67.0	4.0	3	18.0	UPPER	SHAFT	COS		1866.1	-1388.4	-438.3	231.3	-375.8	-45.6	48.9	-0.8	35.2	-50.0	-13.7
S,C = 8.4 S = 0.001886	OR BLADE NORMAL 2R			1696.0	-1021.6	7.16	-109.3	35.1	-212.6	6.89	-80.0	26.6	5	5	¥	NIS			281.0	_	3	3	-150.6	S	3	•	3	6.1-
ALFS, CP/S	UPPER ROTOR	3	3375.1	881.2	-513.3	-38.3	260.2	-259.8	163.9	40.4	-87.7	155.9	-28.6	UPPER	PITCH LIP	COS		-274.2	-148.6	98.4	-136.9	28.3	8.0	-2.9	0	_	32.9	~
OMEG*R = 591.9 RHO100 = 0.2265	U . SIN	2 7 0		872.	-1408.9	153.3	-251.6	228.2	-383.8	279.7	-124.6	9	50.	EDGE	~	NIS			•				-109.8	_	•	•	•	•
PCINT 8 104.8 OM 0.299 RH	٠		2216.0	968.4	-676.0	6.64-	371.6	-484.0	139.5	-24.7	-234.8	337.2	-121-1	UPPER ROTUR	BEND ING	COS		-5088.1	3	8	148.0	~	127.0	-43.0	891.0	-67.0	-17.5	-8-0
RUN 25 VKTS = V/OR =		HARMONIC	O	-	2	3	4	€	•	~	œ	6	10	24	10		HAR MON IC	0		7	6	*	\$	•	7	<b>c</b> c	6	10

= 0.2138 =-0.0055		NIS		60.1	-21.8	-84.0	12.5	-53.7	17.4	4.0	-14.0	-5.9															
CMY/SgR =	•6R	<b>COS</b>	-211.9	-142.3	31.0	-57.0	49.5	-41.5	-30.6	8.2	-24.8	-10.1															
=0.11600 =0.01780	3	NIS		277.7	-83.7	708.4	22.5	138.7	-44.3	5.2	-12.4	4.6															
CLR/S,R CDR/S,R	BENDING . 3R	<b>COS</b>	893.3		41.2	131.2	-86.3	129.5	1.69	0.5	-34.0	0.2															
* 8.4 0.001886	BLADE NURMAL	SIN			-152.9	223.7	4.4.4	210.3	.128.8	18.6	7	3.2	TOR	LOAD	NIS			145.1	31.2	-26.8	7.2	-18.5	-8.8	-29.0	59.9	-31.0	-14.4
ALFS, C CP/S =	LOWER ROTOR .2R	cos		-180-6		270.0			117.7 -	-42.1	112.2	32.1	LOWER ROTOR	PITCH LINK	cos		-51.4	-157.9	19.5	-28.0	-2.7	0.1	54.4	14.4	-0-2	25.1	16.7
= 591.9 = 0.2265	ï	NIS		500.3 616.0	244.8	5.81	6.9	35.3	30.2	15.5	30.1	57.0	GEWI SE	IT .IR	ZIS			6.9	53.0	6.41	-30.3	9.69	-2.6	12.1	5.01	3.9	9•9.
8 OMEG#R RHO100	. IR		•	) ) (		0	80		80	۳,	4	6.5	RO	ING MOP	05		0.1	'	-209.6 -25			. 7		0	7	4	3
POINT 104.8 3.299		J	1142	-1089	95	24	-373	314	296	-117	23	4	LOWER	BEND ING	Ü		675-	224	-20		-2	34.	16-	438	-82	9-	-1-
PUN 25 VKTS = V/OR =		HARMONIC	0	<b>-</b> ^	ı m	*	ĸ	•	_	<b>6</b> 0	6	10	24	1		HARMONIC	0	_	7	m	4	2	\$	~	<b>c</b> c	6	<b>1</b>

S#R = 0.2138 S#R =-0.0055	UPPER RUTOR SHAFT STRESS		3	~	72	144.	~	452.	8	295.	39	90	36	54	13	3408.	1468.	83	37	98	18	2769.	714	3405.	3504	86	40	2697.	87	330	48	30	409	1196.
0.11603 CMY/ 0.01780 CMX/	UR PITCH		-421.	54	96	-206.	18.	146.	93.	-95.	-205.	-134.	-47.	-14.	-129.	-130	-118.	-67.	110.	267.	132.	-224.	-481.	-919-	-771.	-765.	-498-	-378.	-621.	3	-649-	-447.	-403.	
CLR/5,R = COR/5,R =	UR EDGEWISE BENDING . 18		-1639.	-1757.	-2425.	-2161.	-1185.	-1241.	-2891.	-4495.	-4725.	-4660.	-5955-	-7951.	-8613.	-7921.	-1925.	-9172.	-9683.	-8251.	-6405-	-6009-	-6614.	-6407.	-5004-	-4023	-4560.	-5417.	-5083.		N	•	-4482	-5909-
S.C = 8.4 S = 0.001886	MCMENT U	<u>.</u>	N	N	-149.	-1058.	-541.	-102.	-34.	130.	115.	-343.	-511.	75.	373.	-613.	-3020.	-3908•	n	-3174.	-2825.	-1885.	-1303.	-1148.	-06-	49	45	3375.	42	4	55	2		1
9 ALF 5 CP/	BENDING 38	; ;	65		61	1477.	85	1977.	1978.	2126.	2447.	2679.	2469.	1930.	56	1404.	1060.	557.	17.	-419.	-995-	-1123.	-892.	-513.	-41.	395.	2	0	10	1556.	1524.	1616.	76	1802-
= 591 = 0.22	BLADE NURMAL		958	566	537	986	4386.	546	785	171	211	914	16	48	60	57	0	16	38	21	4	S	•	7	56	84	33	16	_	3361.	Φ	_	œ	4086.
PDINT 8 104.8 OMEG*R 0.299 RHJ100	UPPER ROTOR B	•	9	9	13	56	3522.	O	-	Q	7	36	1	œ	0	S	3	S	Q.	4	M	18	52	9	-118.	0	Ō	60	42	1482.	49	6	580	
NUN 25 P	כ	ဟ	0	1.2	2.5	3.7	0	6.2	7.5	8.7	0.0	01.2	12.5	23.7	35.0	46.2	51.5	68.7	80.0	91.2	02.5	13.7	25.0	36.2	47.5	58.7	70.0	81.2	92.5	03.7	15.0	26.2	37.5	8

RUN 25	POINT	80							
V/CR =	0.299	Ž	CHEC+R =	0.2265	5 CP/S =	s = 0.001886	8.4 CLK/3,K 1886 CDR/S,K	=0.11000 =0.01780	CMX/S,R = 0.2138 CMX/S,R =-0.0055
	LOWER	ROTOK	BLADE	NURMAL	60	KOK	LR EDGEWISE	LR PITCH	Į.
U		<u>د</u>		•	•	5			
000	,-1	26	25	34.	1747.	-373.	-3801	-2	58.
88.7	. 1*1	4	26	S	1691	-330.	3	-2	19.
77.5	•••	80	79		1791.	-245.	-4111.	ÇÎ	232.
66.2	4	90	31	_	2259.	-261.	-3878.	-3	.318.
55.0	7	8	40	0	2631.	-353.	-5117.	-2	39.
43.7	-1	98	42	•	2535.	-293.	-6767.	ĭ	-40.
32.5	171		34	0	2160.	-121.	-7011.		-2.
21.2	***	90	25	æ	1859.	-141-	-6252.	1	72.
10.0	•	19	28	107.	1801.	-403.	-6454.		1.
98.7	-1	41	33		1868.	-644.	-1161-	<u> </u>	182.
87.5		38	58	ø	1684.	-674.	-8751.	~	243.
•2	~	1599.	11	.97.	1054.	-550.	-7870.	7	39.
65.0		-4	'n	S	344.	-392.	-6573.		63.
53.7	7	20	-2	.09	-6.	-253.	-6559.	<b>-</b>	108.
42.5	7	40	-	_	-47.	-171.	-7439.	7	123.
31.2	ī	92	9	0	-12.	-182.	-1411.		71.
20.0	•	35	~	~	89.	-199.	-6809-	7	113.
08.7	7	39	-	.25.	227.	-97.	-5188		77.
7.5	1	59	4-	4	225.	<b>48</b>	-5723.		84.
6.2	ī		9-	~	91.	123.	-6176.	•	-5.
5.0	7	22	-	.10.	20•	178.	-5074.		64.
3.7	1	52	5	0	15.	210.	-3694.	7	07.
2.5	7	14	5-	.02.	-64•	119.	-3869.		48.
1.2	ī	01	9		-127.	-14.	-4145.	1	14.
0.0	ī	34	1	3	34.	-46-	-4345.	-134	34.
8.7	•	87	-	S	354.	-181-	-2957.	-260	•0•
3		37	S	す	565.	-315-	-2448	-19	93.
56.2		86	_		554.	-273.	$\sim$	Ĭ	•66
45.0	•	63	7	S	443.	-134.	æ	-227	27.
•		411.	•	_	479.	-148.	$\sim$	-3	46.
22.5	. •	6	=	.18	870.	1	-2427.	-2	77.
11.2	•••	29		9	1451.	-356.	S	7-	34.

= 0.2565 =-0.0028	<u>م</u>	NIS		2294.3	-550.9	165.9	483.6	-374.4	128.7	-36.4	1.68-	11.0	20.2																
CMY/S, K =	•	cos	7 8 2 7	1424.8	-414.3	-371.5	-538.8	240.3	236.8	7.1	30.1	-12.0	8.95																
=0.13770 =0.02220	MUMENT	NI S		4580.6	-475.3	80.9	-83.1	78.2	-91.6	-71.7	-5.9	-5.8	-7.5		LUTOK	TRESS	NIS			882.6	-2.3	-148.9	6.96-	-553.7	131.0	-671.5	38.5	-50.7	-15.0
CL K / S, K CDK / S, R	. BENUING MCMENT	cus	2231 5	703-1	125.0	3.3	114.6	-73.0	-11.1	38.7	20.2	14.0	17.0				cos		2232.2	-540.3	-435.1	139.3							-78.7
ALFS,C = d.6 CP/S = 0.001653	CTOR BLADE NORMAL	NIS	•	7 7108-8			2 -123.1					-27	-12		UPPER ROTOR	LINK LUAD	COS SIN		4	58	4.67	-7	14	-	(F)	7	ις.	7	
97.7 AL	UPPER RCTUR	SUO	5136	6.46.10	233	39	326.	-251.	-73.	44.	-63-	99	-21.		UPP	PITCH	COS		-344.	-152.	-21.	-06-	7	57.1	43.	-116.7	27.	-35.	S,
UMEG#R = 59 RHJ100 = 0.2	æ	SIN		10451.8	0-616-	239.0	-350.7	533.6	-275.7	206.3	130.6	-76.6	•		OR EDGEWISE	Š	SIN			561.1	-930.7	ø	-		_	-659.0	~	~ 1	16.6
PLINT 9 104.3 UM 3.295 RH	•	cos	7 7277	1253.2	471.5	144.4	4.67.4	-373.4	·	-	-134.2	65.8	6.99-		UPPER ROTOR	BEND ING	COS		-5526.3	•	Š	•	•			1	•	1.5	•
RUN 25 VKTS = V/OR =			HARMONIC	> ~	. ~	· ~	4	ν.	9	7	œ	6	10	2	:44			HARMONIC	0	-	7	6	4	2	•	1	<b>6</b> 0	0	10

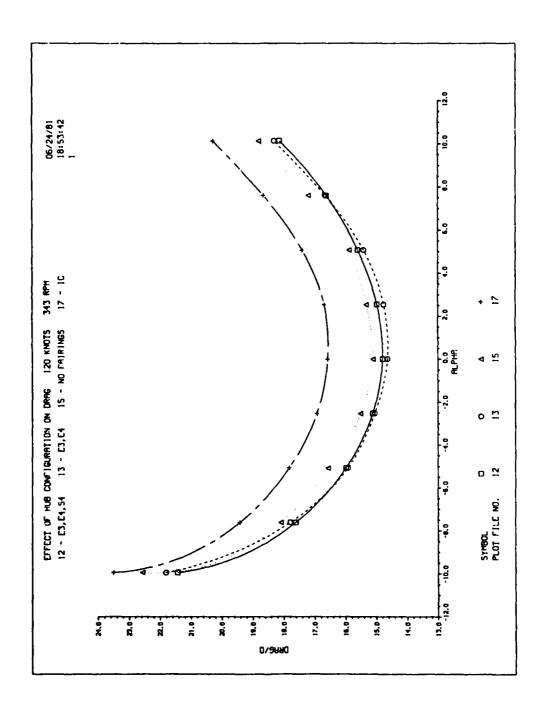
RUN 25 VKTS = V/OR =	POINT 104.3 0.295	9 UMEG*R RH0100	# 0 0 11 11	0	597.7	ALFS,C CP/S =	**	8.6	CLR/S,R CDR/S,R	±0. =0.	=0.13770 =0.02220	CMY/S,R =	=-0.0028	565 028
		•			LOM	LOWER ROTOR	8 BLADE	DE NORMAL	BENUIN	NON 3	ENT	•	Ç	
	ננ	•1R cos	NIS	z		cos	SIN	z	e. Suo	ξ S	NIS	cus	ž «	NIS
HARMONIC	,	,			,	0			0					
۰.	7487		0 2 3 0	G	7	30.6	2112	,	0.4691	-4413	- 2	1.041-	-27	3
- ~	902.4	7	0401-	۰.	•	702.9	507.5	ָּיַ עַ	483.3	70 <b>4</b> -	5.6	125.7	, ר	70.2
ı <b>~</b>	561		-122	· m			-107	.7	63.1	1	7.3	41.3	-2	0.8
4	36		118.9	6			58	4.	65.8	S	51.3	-24.0	- 3	1.9
S	-255		-434	.2	١	.217.1	-144	0.	-78.8	15	6.2	43.0	s	3.2
•	-164		634	۴,		77.5	365	.1	-3.3	87	0.6	6.2	9-	2.4
7	335		13	3.5		7.961	-113	.1	98.6	-13	7.0	-32.2		3.8
<b>6</b> 0	-123		-171	4.		-82.9	9-	•3	4.9	7	7.0	13.5	7	3.1
6	-263	3.4	112	€,		-48.8	98	•5	-1.0	<b>1</b> -	9.6	21.7	7	7.4
10	<b>)1</b>	0.2	26			11.0	13	•	-13.9		2.1	-2.2	•	9.3
2														
45	LOWER	RUTUR EDGEW	EDG.	EW ISE	•	LOWER ROTOR	40 TOR	<b>.</b>						
	BENO	BENDING MUMEN!	AFR.	→	2	11 H211	AK LUA	LUAD						
HARMONIC	<b>.</b>	<b>י</b>	7	5		3	5	<b>5</b>						
0	-5583	3.6				6.69-								
-	2242	0•	19	61.9	,	0.611	991	.1						
2	-1359	80	1088.0	•		75.6	19	19.4						
6	5 TT -	7	18	0		-25.4	30	4.						
4	-25	5.8	-42	45.9		0.8	-5							
5	19	7.5	-2	•2		-47.6	15	•2						
9	-25.8		95	9.		59.5	14	8.						
7	1156		-131	0.		-24.2	-27	<b>7.</b>						
æ	40	4.1	91 -	4.9		9.91-	10	6.01						
6	5-	9.5	14-	0		-9.3	9-	9.						
10	<b>4</b>	4.4	•	0		-1.3	9-							

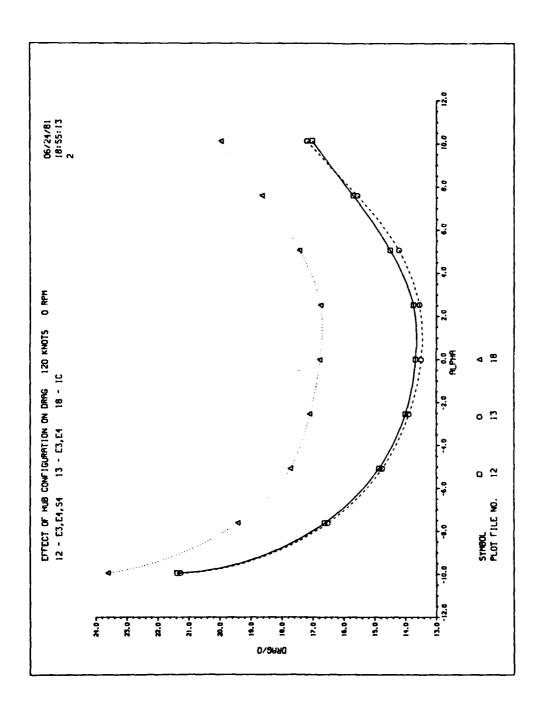
RUN 25	PCINT	<b>5</b>					•	1	
VKTS = V/CR =	104.3 0.295	A E	OMEG*R = 597.7 RHU100 = 0.2265	AL F CP/	$S_{9}C = 8.6$ S = 0.001653	53 CDK/S, R	=0.13170 =0.02220	CMX/S,R = 0.256 CMX/S,R =-0.03	65 28
	UPPER	ROTUR	BLADE	BEN	MCME	UR EDGEWISE	UR PITCH	UPPER RUT	<b>3</b>
	•	. 1.R	•2	•3R	• <b>6</b> R	BENDING . 1R	LINK LUAD	SHAFT STRE	SS
S									
0	9	389.	6134.	3117.	1373.	-3494	19	5. 109	
1.2	Ø		7297.	3638.	1639.	93	-355	5. 24	•6
2.5	01	~	8454.	4369.	2031.	-5345	766-	-	5.
3.7	10	خ.	9371.	5178.	2989.	21	-572	•	•
0			9945.	5617.	_	-	-362	•	
6.2	12.		10371.	5765.	_	-3646.	181	•	.2.
-	13.	13314.	10910.	6056.	3590.	-4325.	393	. 28	.5.
8.7	14.	302.	11655.	6559.	2865.	S	61	•	
0.0	15.	255.	12390.	94	2112.	-3255.	-278	•	4.
01.2	15		12628.	87	2183.	0	-230		·I.
12.5	14	ā	11960.	32	2964.	-4684.	ï		3.
23.7	12,	. •	10590.	67	3460.	-6024	8	•	3.
35.0	01	589.	9420.	5232.	2894.	-6149•	9-	•	5.
46.2	<b>₹</b>	485.	9011.	4802.	1225.	-6156.	-355	•	<b>.</b>
57.5	10	~	8598	4066.	-503-	-7634.	-451	•	۶.
68.7	~	719.	7148.	3001.	-1177.	-9705.	761-		8.
80.0	Ŧ	-	4938.	1745.	-1195.	-10277.	55		4.
91.2		•	2824.	470.	-1336.	-9371.	31-	(m)	6
02.5	7		953.	-641.	-1441-	-8902	-267		.720.
13.7	Æ-I	10	•	51	-1709.	-99566	-19	_	3.
25.0	14-	$\sim$	•	-2125.	-2586.	-9738.	-70		• •
36.2	-5	147.	•	-2431.	-3194.	-8058-	-165-	2	•
47.5	<u> </u>	$\sim$	•	-2521.	-2839.	-5858	716-	2	.8
58.7	9-	045.	•	-2510.	-2271.	-5238	-74(	91	58.
70.0	<u> </u>	~	•	-2342.	-1611.	-5577.	-36	. 15	37.
81.2	-5	~		-1991.	-271.	-4106.	-427	91	.7.
92.5	<b>3</b>	820.	•	-1539.	9	-2854.	-168		13.
03.7	-3	ù	-274.	-948-	1236.	-2240	-905	-	7.
15.0		00	.166	-176.	-	-3315	199-	•	<b>:</b>
26.2		165.	2379.	678.	æ	-4217.	-451	-	3.
37.5	7	00	3716.	r.	6	14	-569	7	4.
8.7	45	~	. 4764	2459.	747.	96	-75(	. 22	

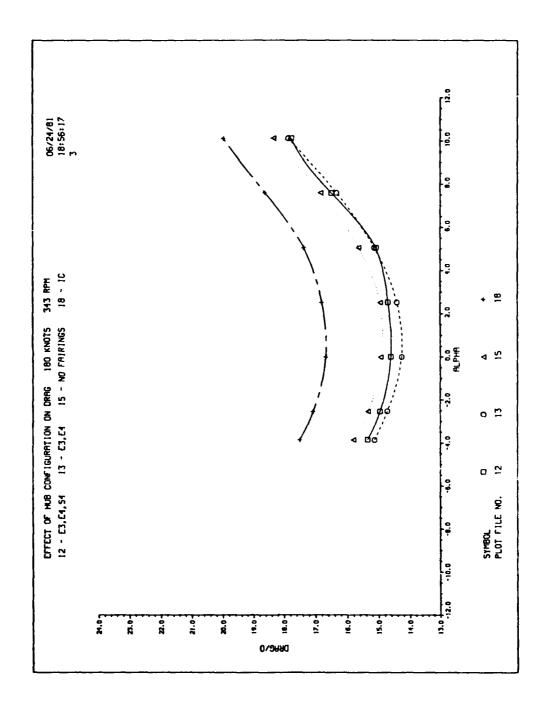
RUN 25 VKTS = V/OR =	POINT 104.3 0.295	9 UMEG#R : RHU100 :	= 597.7	.7 ALFS.C 65 CP/S =	00.001	8.6 CLR/S,R 653 CDR/S,R	=0.13770 =0.02220	CMY/S,R = 0.2565 CMX/S,R =-0.0028
	LOWER RO	ROTOR BLADE	E NORMAL	96	MOMENT	LR EDGEWISE	LR PITCH	
	17.		.2R	.3R	•6R	7.	LINK LOAD	0
PSI								
0000	086		591.	5066.	•06	398	-245	•
88.7	054	•	.609	5084.	147.	-5196.	-291	7.
77.5	125	9.	809.	5470.	138.	-5153	-385	2.
66.2	363	6. 3	923.	6027.	-32.	-3849	-370	•0
0	1437	•	9856.	6202.	-67.	-3600.	-210.	•
43.7	12025	•	167.	5852.	175.	-5157.	-61	
32.5	984	•	641.	5252.	358.	-6673.	-92	2.
21.2	9837	•	955.	4771.	244.	-6734.	-208	•6
10.0	0166	•	986.	4524.	<b>.</b>	-6390•	-177	7.
98.7	8287	•	423.	4088.	-176.	-7408.	36	• 9
87.5	7	9.	778.	3029.	-250.	-9454.	235	5.
76.2	508	•6	2548.	1553.	-247.	-10315.	197	•1
65.0		•9	416.	290.	-256.	-9150.	160	•0
53.7	_	7	184.	-616.	-363.	-7927-	95	2 *
45.5	~	- -	334.	-1421.	-520.	-8368-	103	3.
31.2	-578	33	418.	-2213•	-636.	-9088•	113	9.
20.0	2	64	46	-2854.	-687.	-7827.	26	2.
08.7	_	0 -5	~	-3224.	-684.	-5212•	56	•
7.5	ø	85	44	-3345	-637.	-3840•	7	7.
~	-858	•	21	-3295.	-567.	-4549•	-55	<b>5.</b>
0.0	_	- 15	21	-3047.	-505-	-4304.	-15	2•
3.7	-629	34	3	-2546.	-453.	-2794.	77	•
2.5	•	- 13	33	-1863.	-363.	-1455.	20	• 0
7.	~	52	33	-1062.	-220.	-2276.	7-	2•
0.0	~	11	02	-102.	-101-	-4300.	25	5.
8.7	9	0.	685.	945.	-18.	-4965.	-11	7.
r.	310	2. 2	-	1862.	112.	3	-130	••
56.2	8	6. 3	-	2554.	244.	2	-181	7.
45.0	0	8. 4	~	3096.	255.	S	-201	•
333.75	808	9. 5	56	_	205.	S	-255	· 0
22.5	918	9 • 0	~	38	181.	59	6	٠.
11.2	Δ.	7. 7	05	4941.	129.	-3927.	<b>~</b>	•0

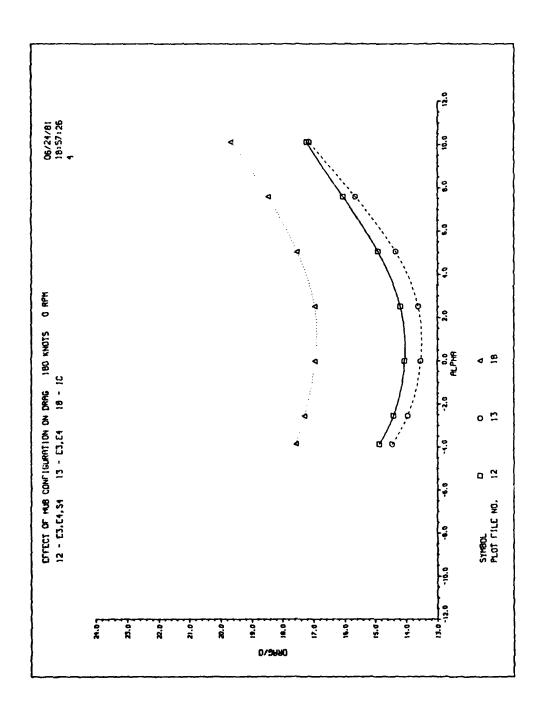
## SECTION D

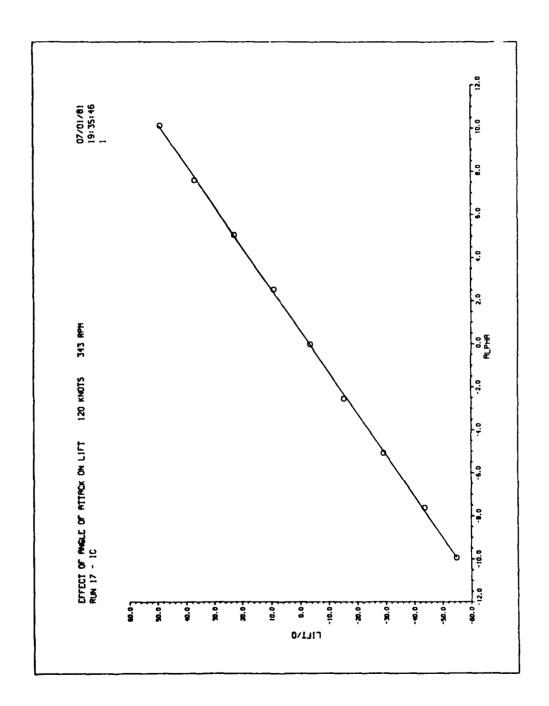
Plotted Performance and Loads Data

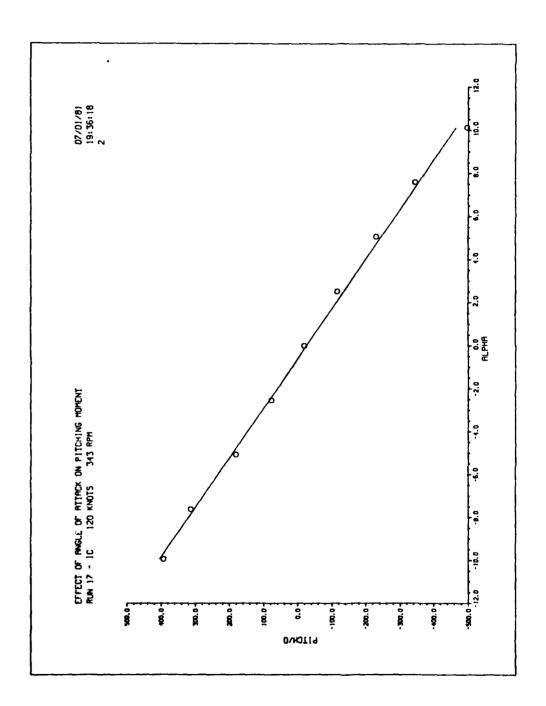


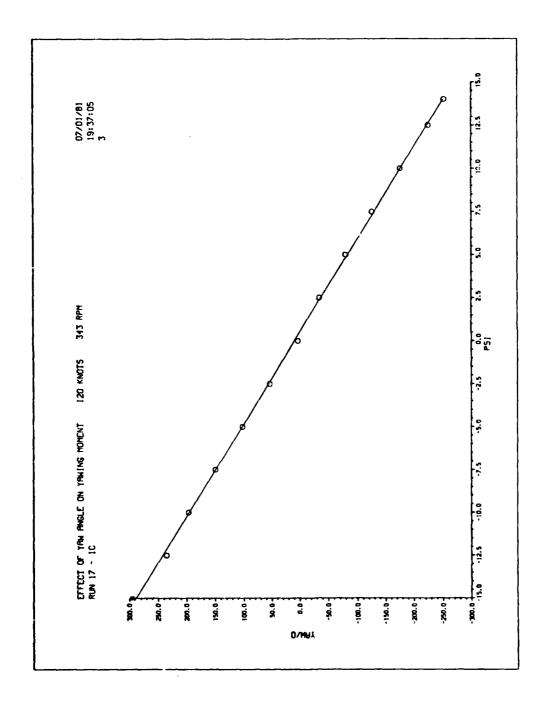


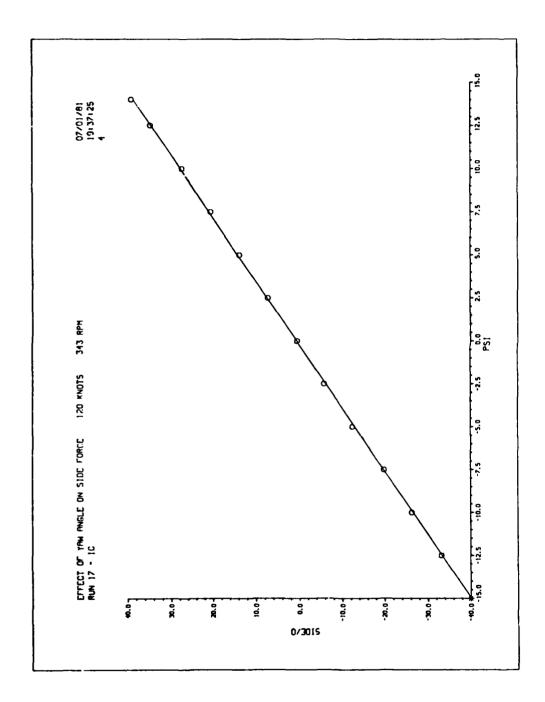


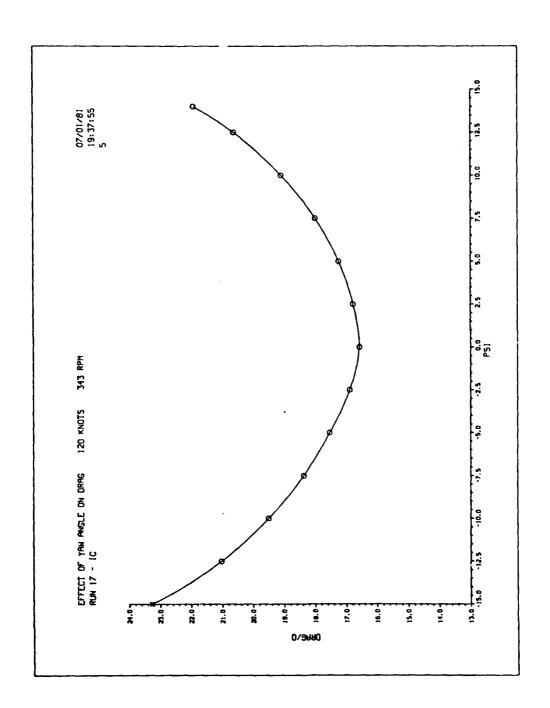


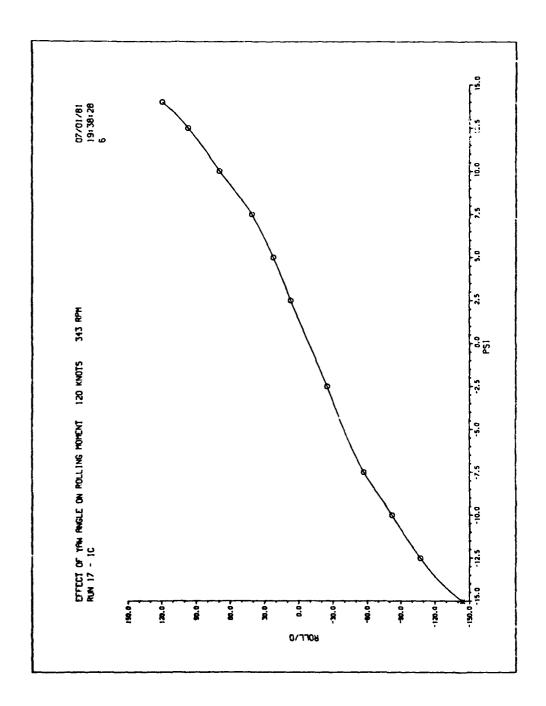


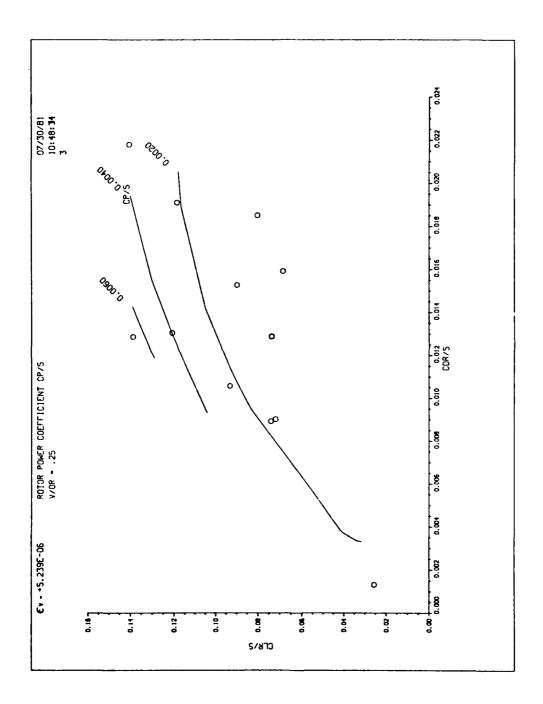


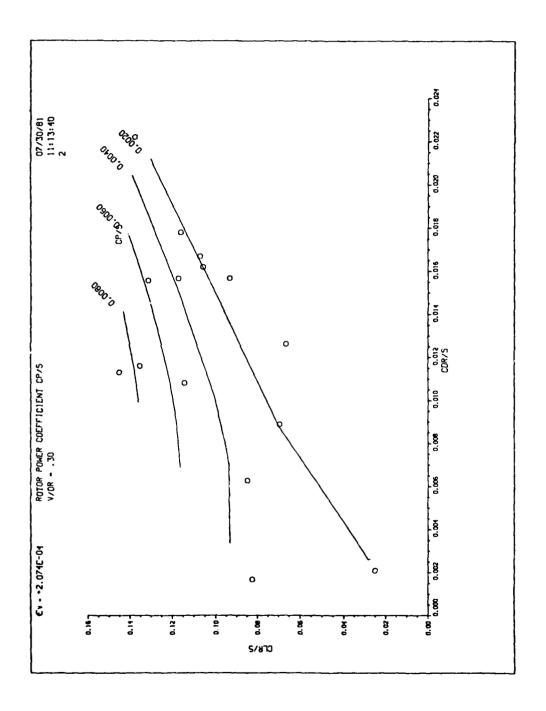


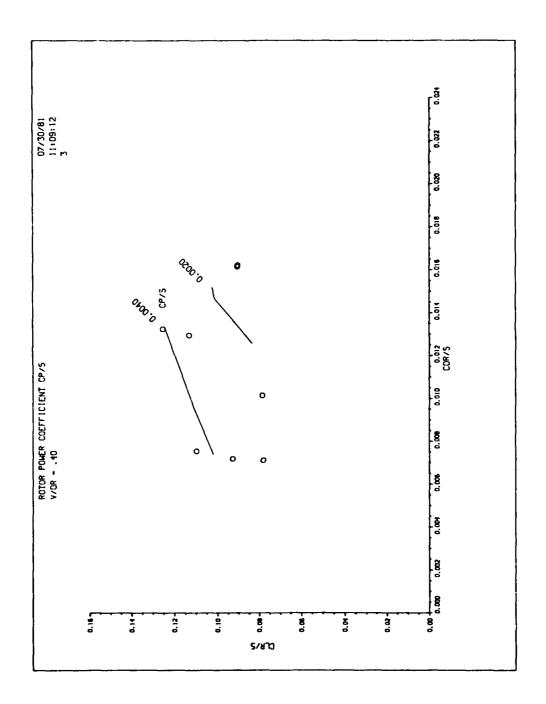


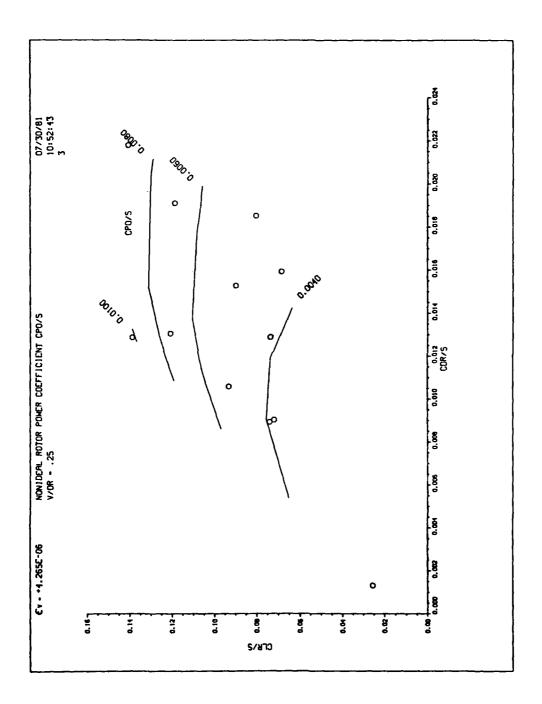


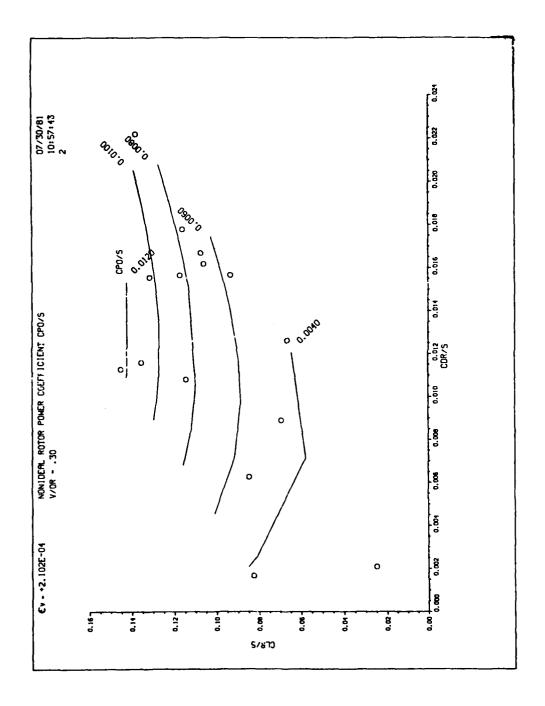


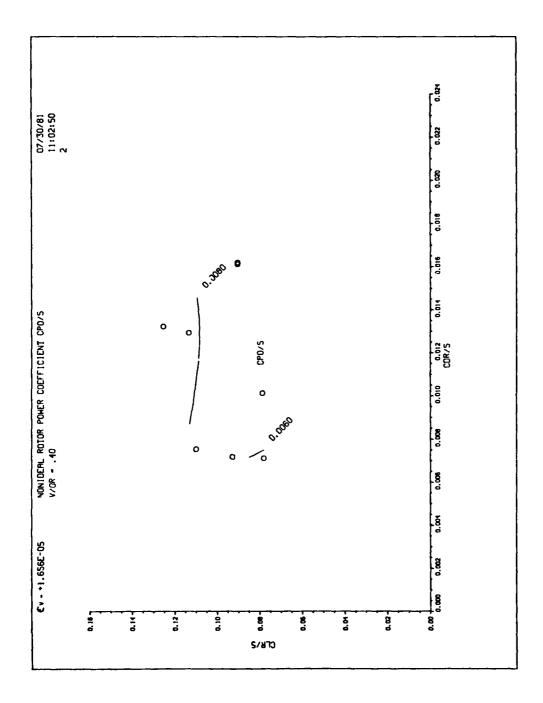


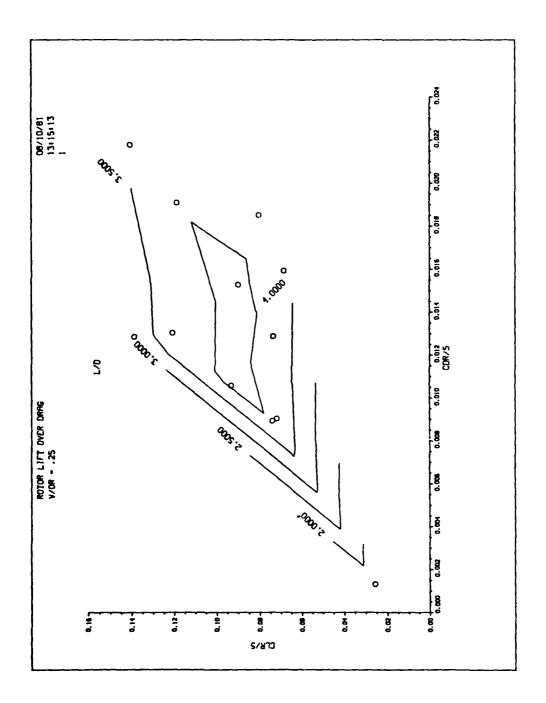


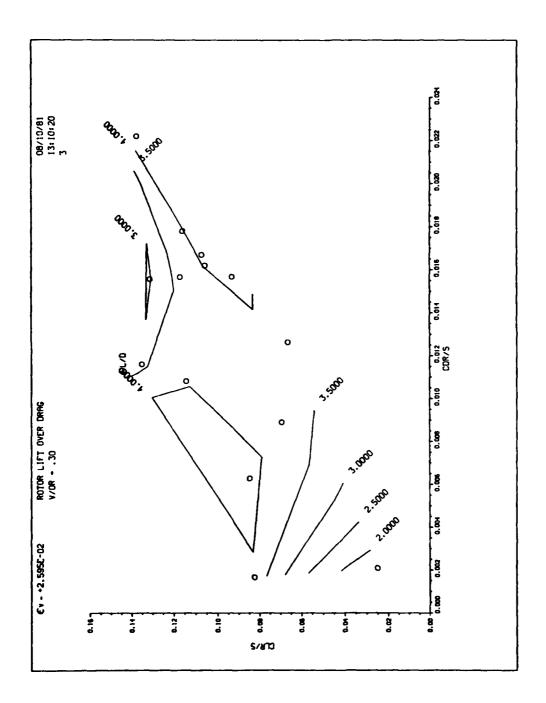


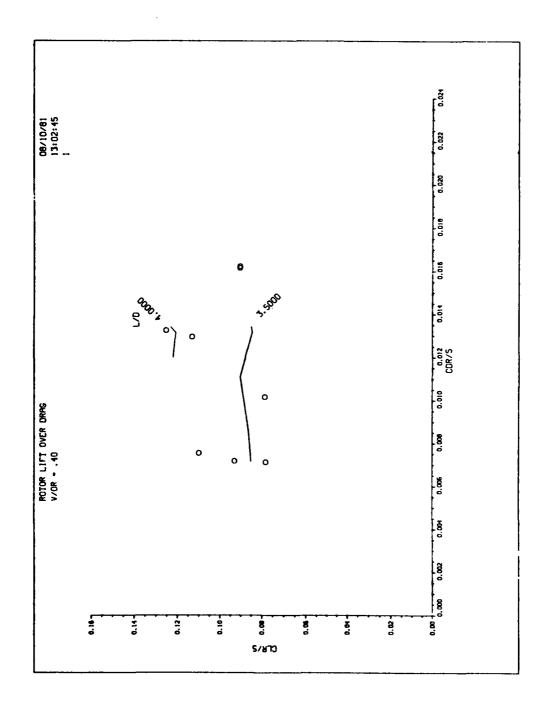


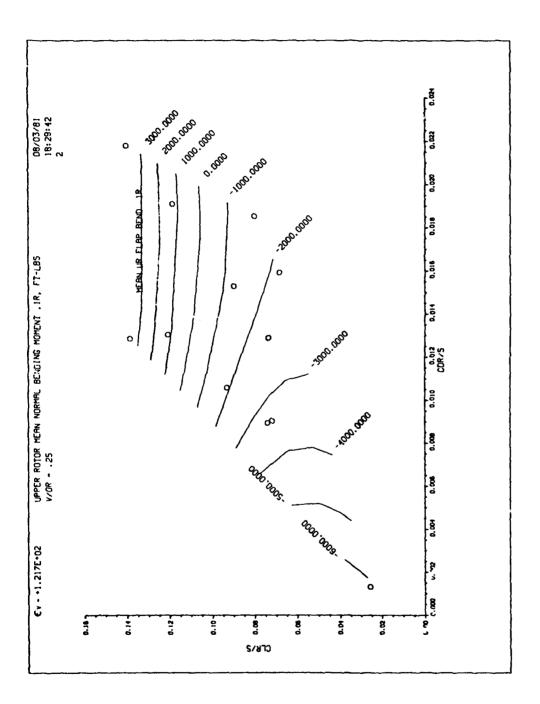


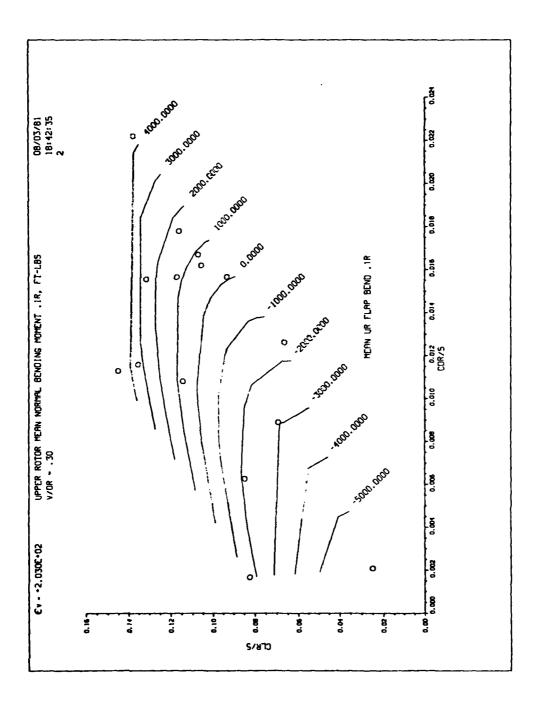


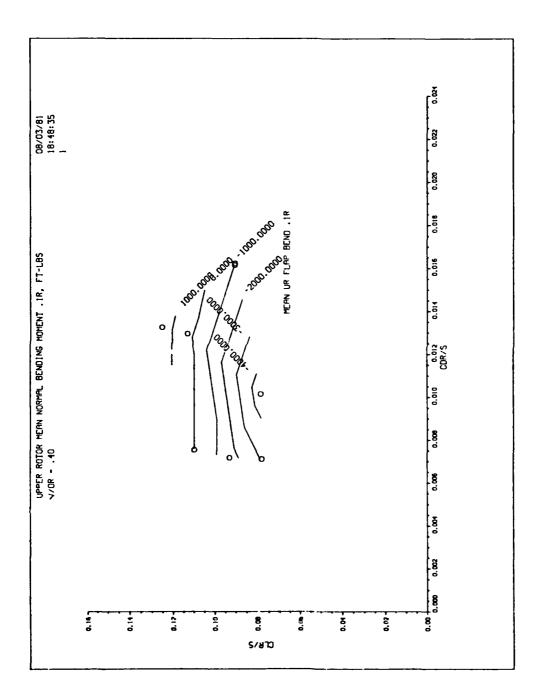


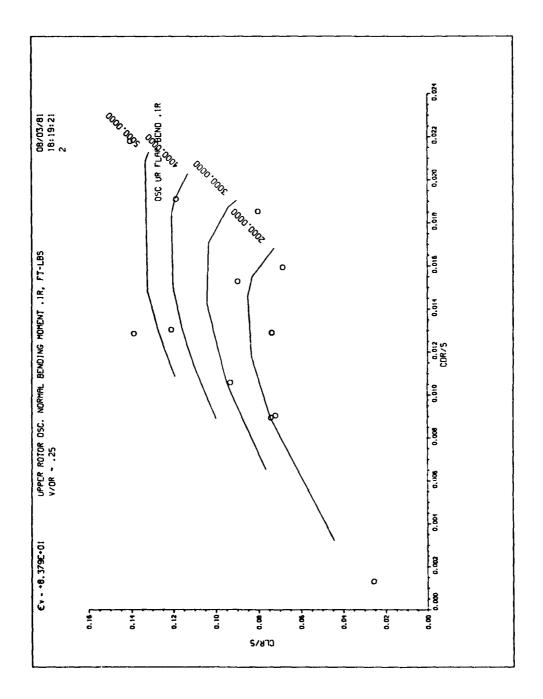


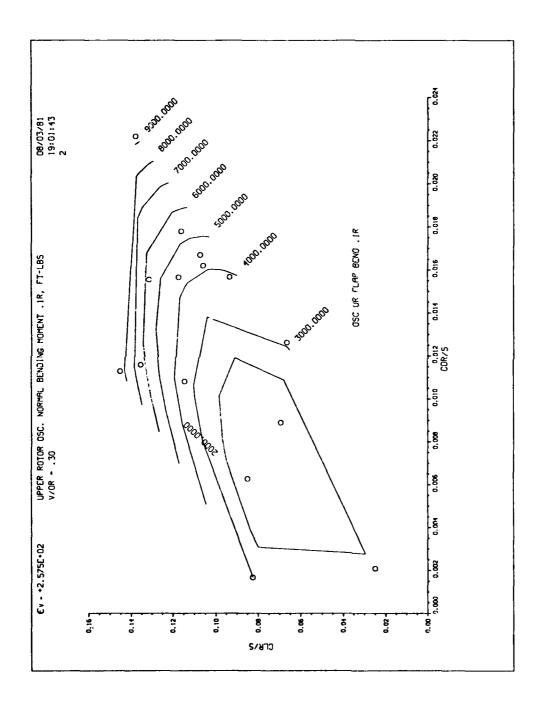


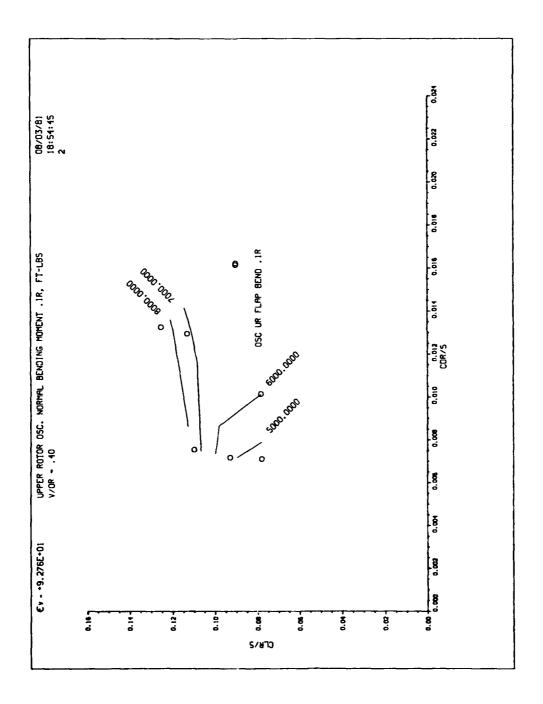


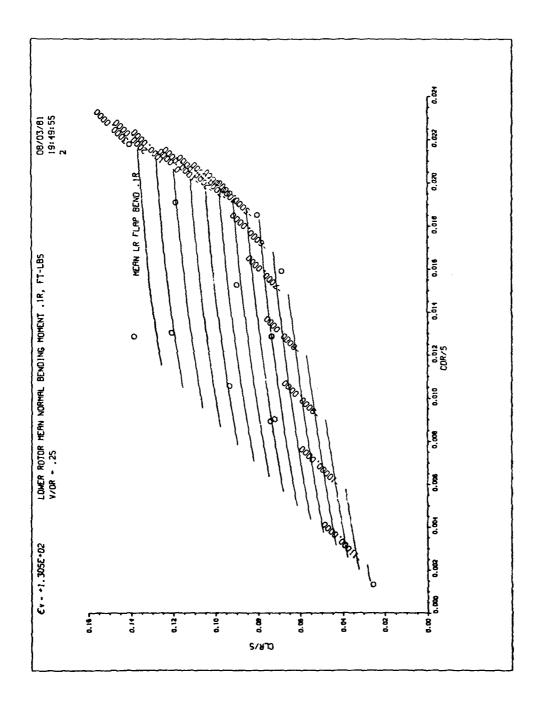


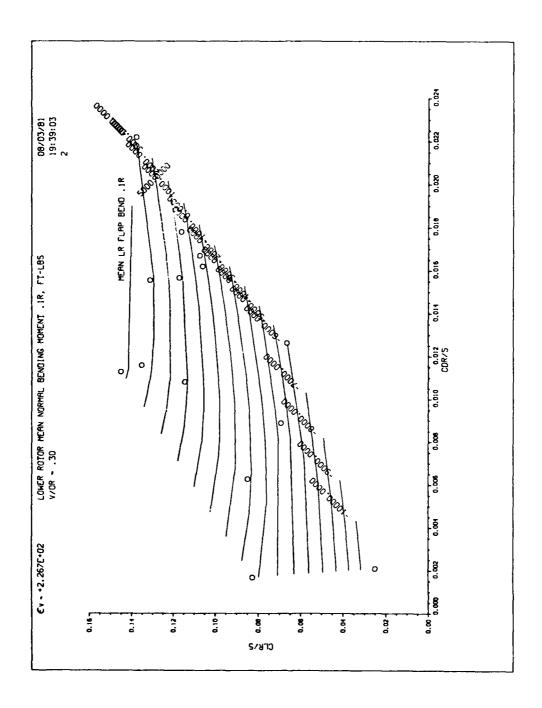


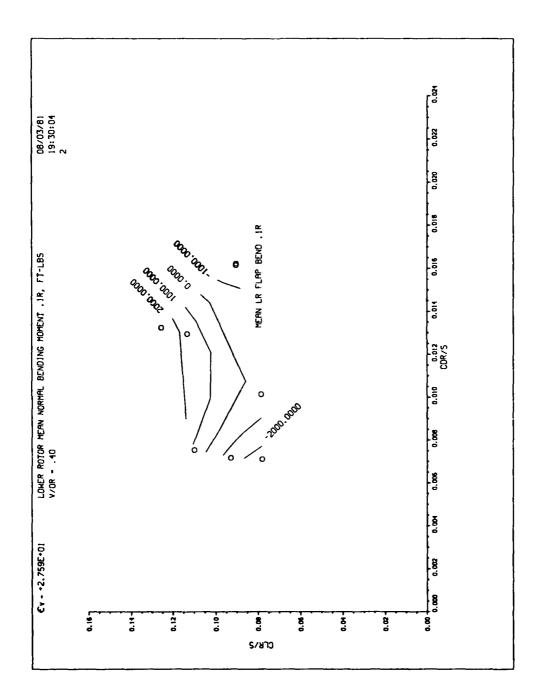


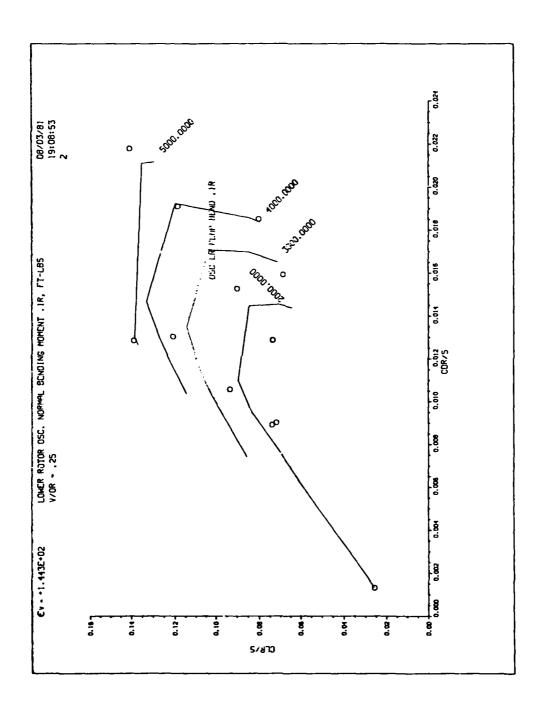


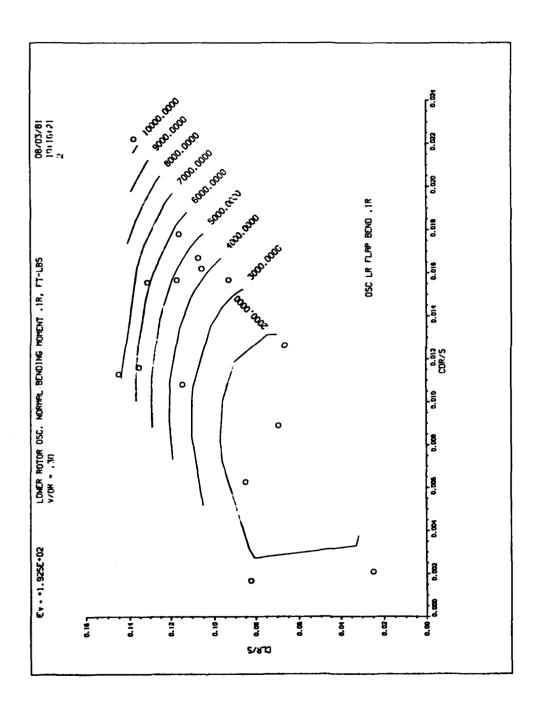


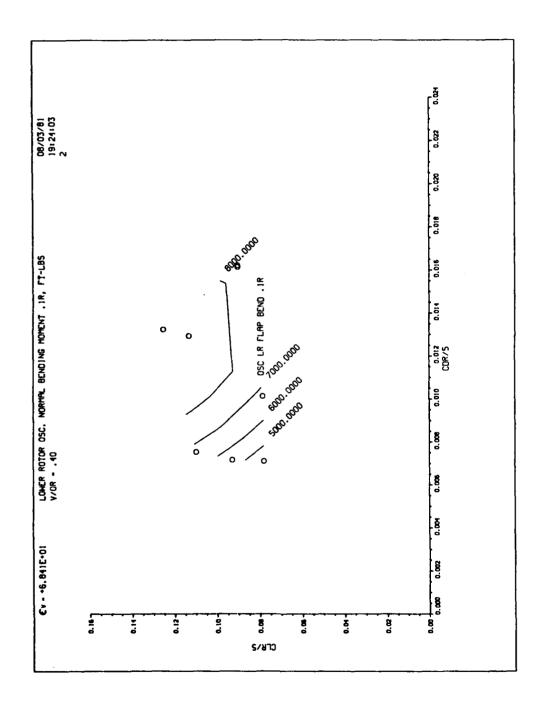


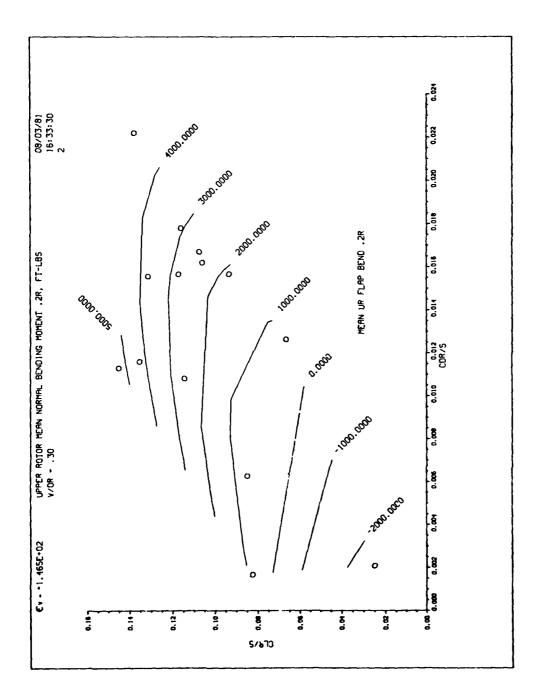


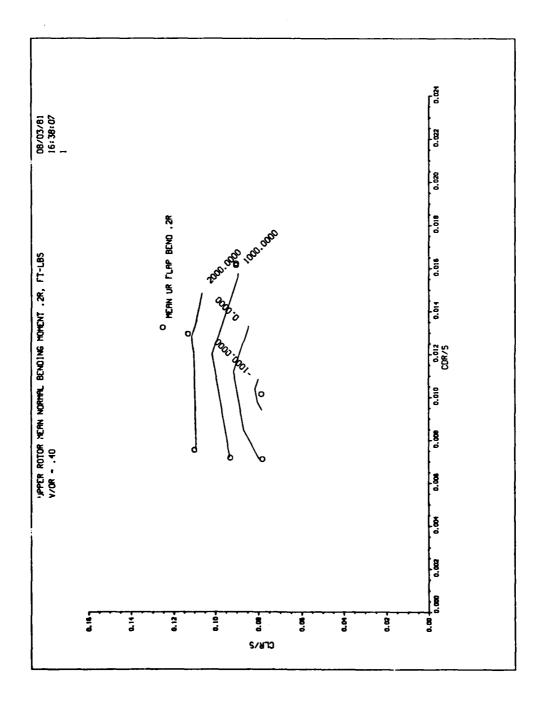


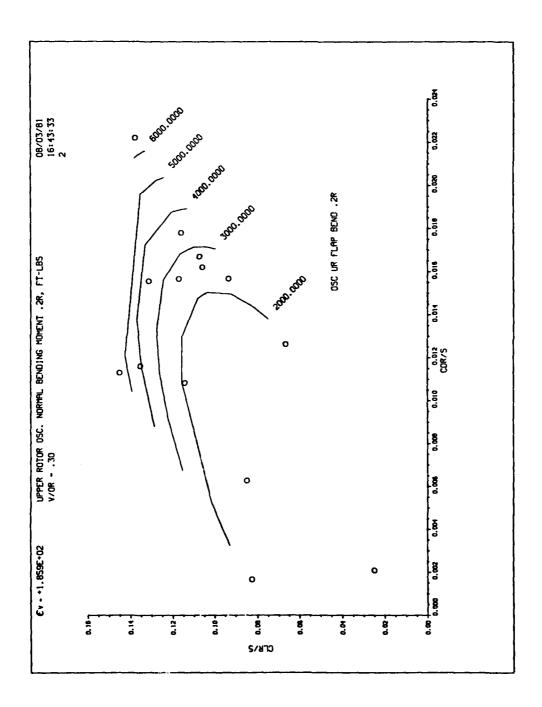


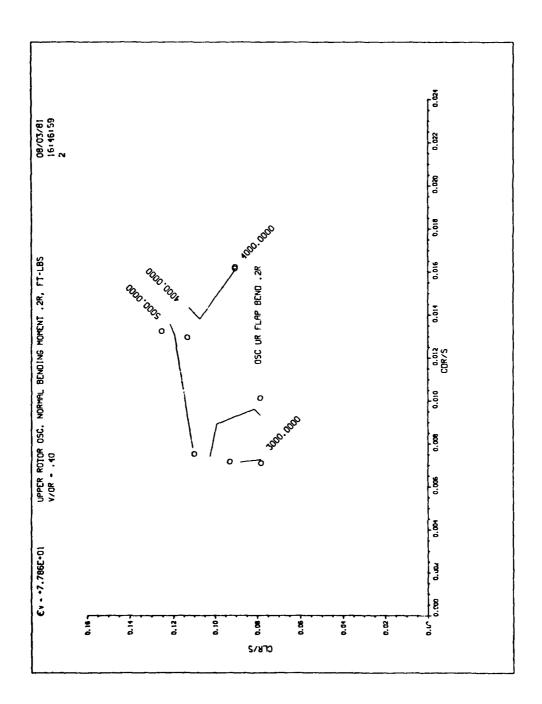


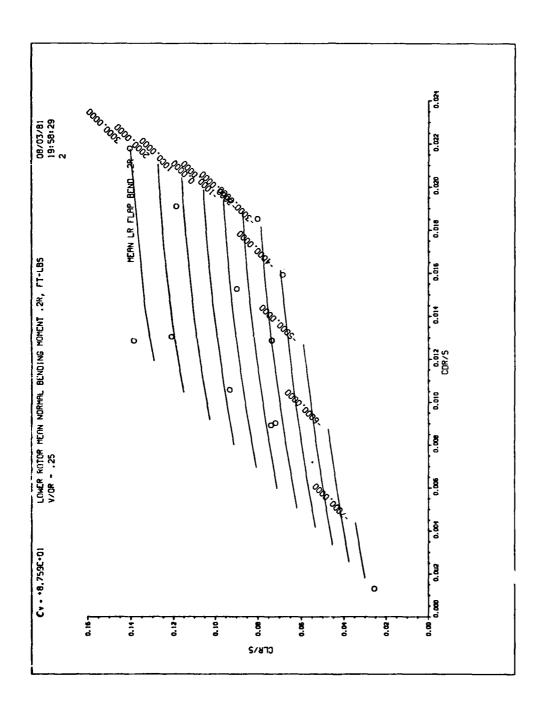


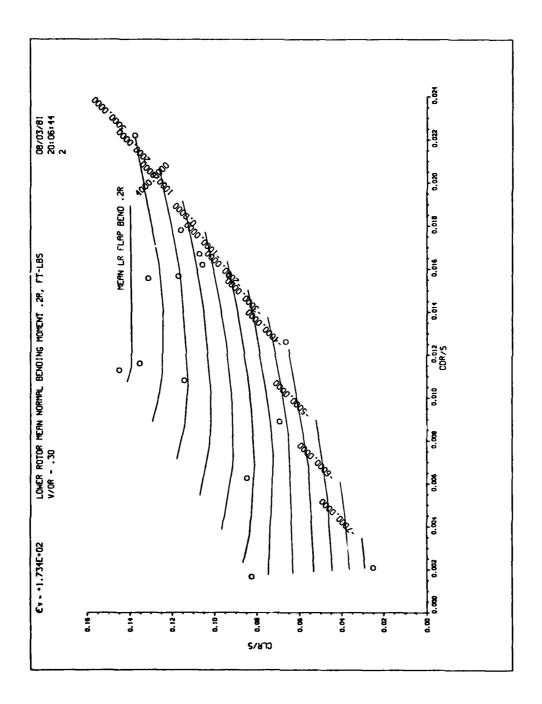


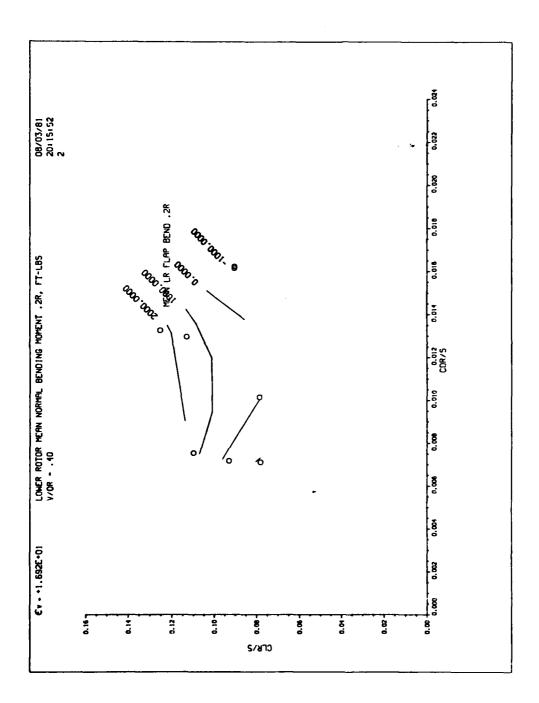


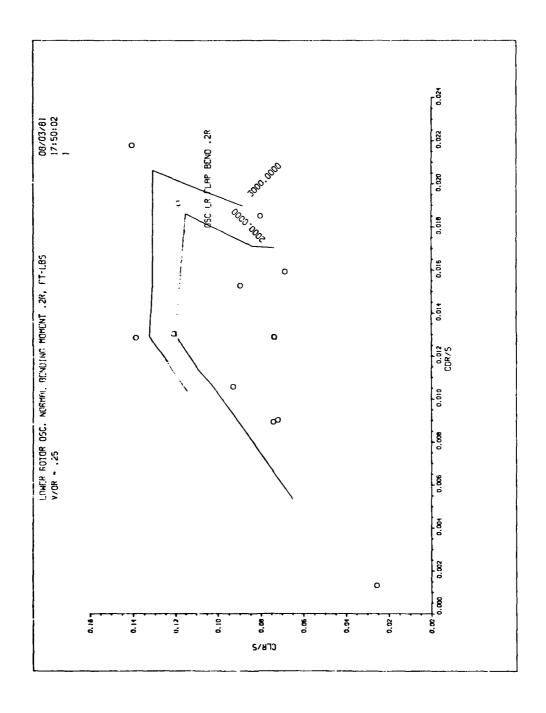


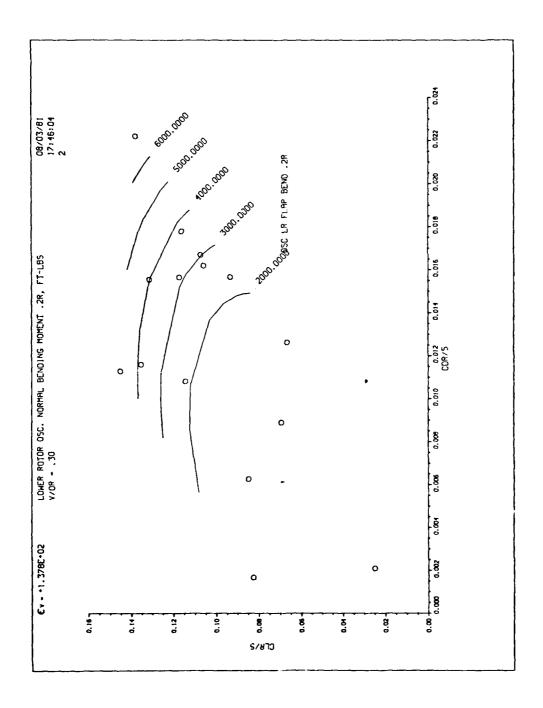


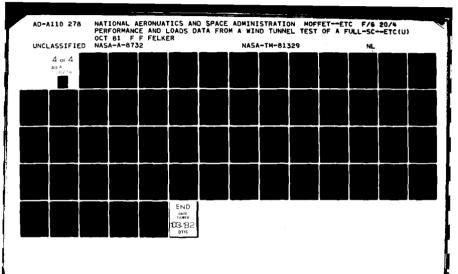


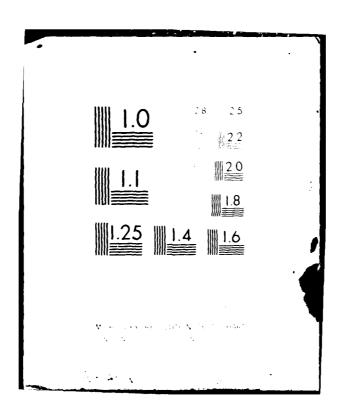


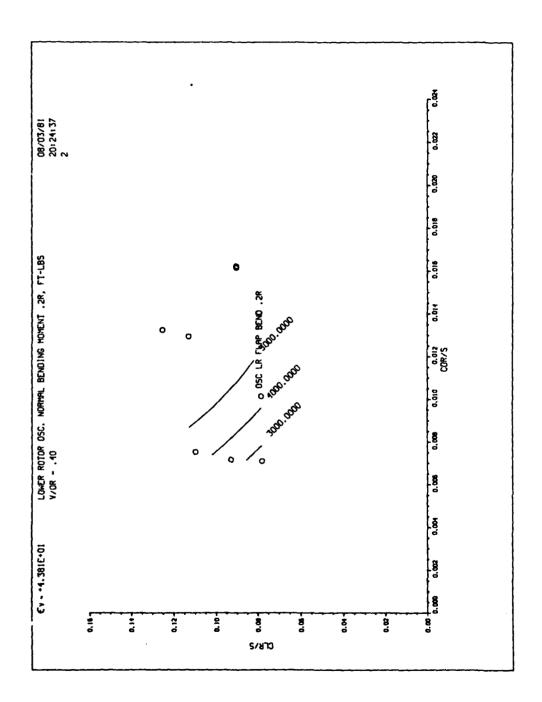


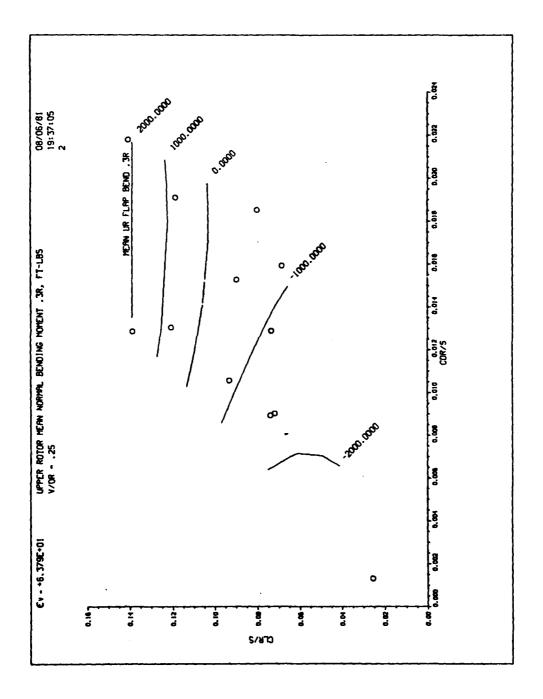




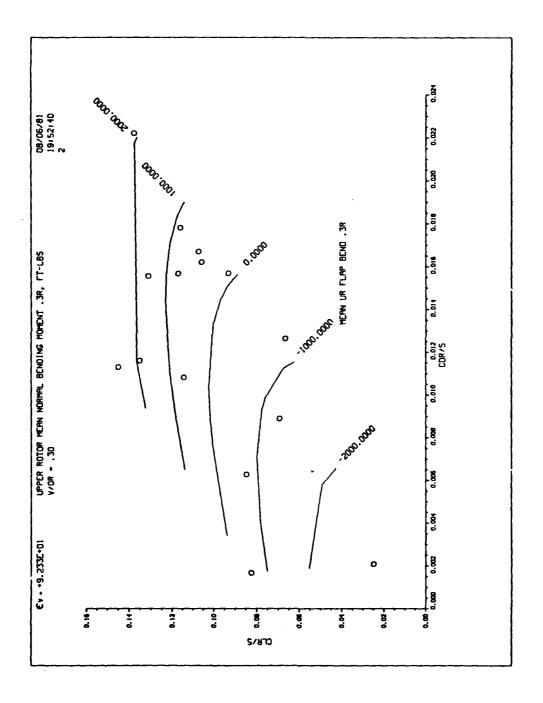


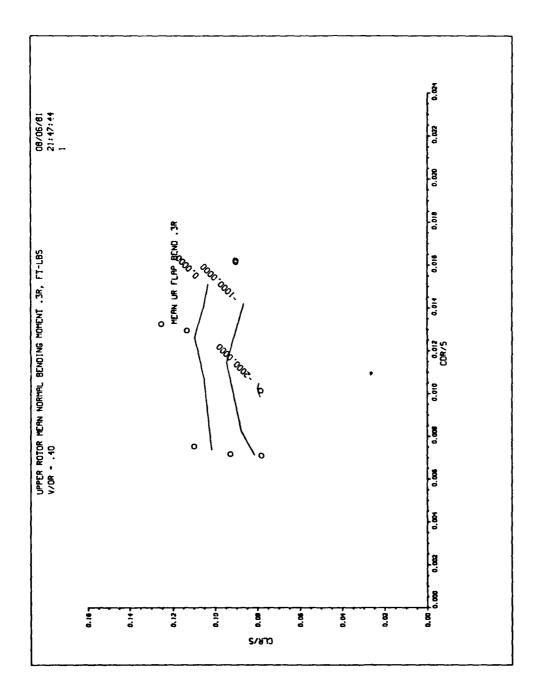


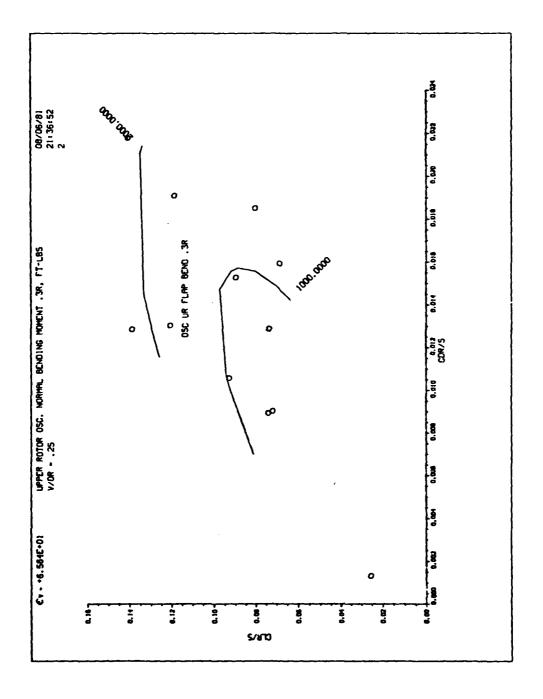


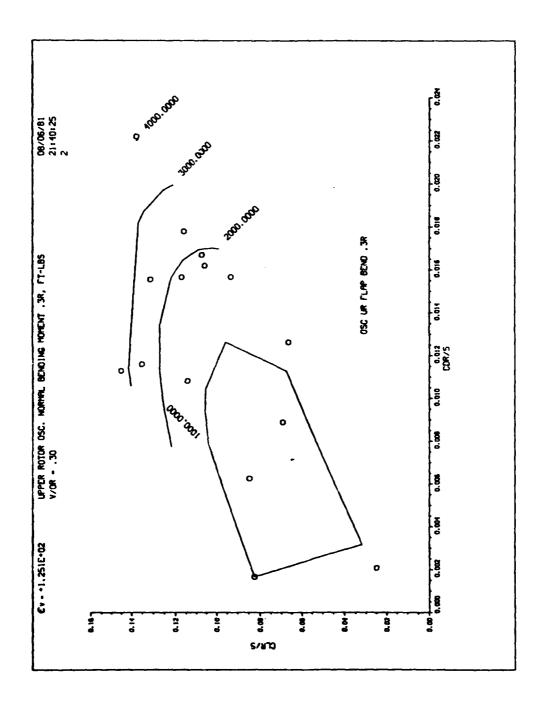


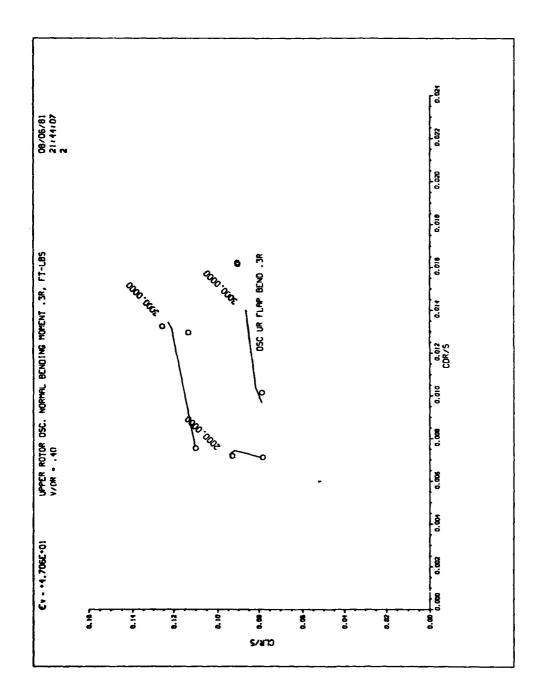
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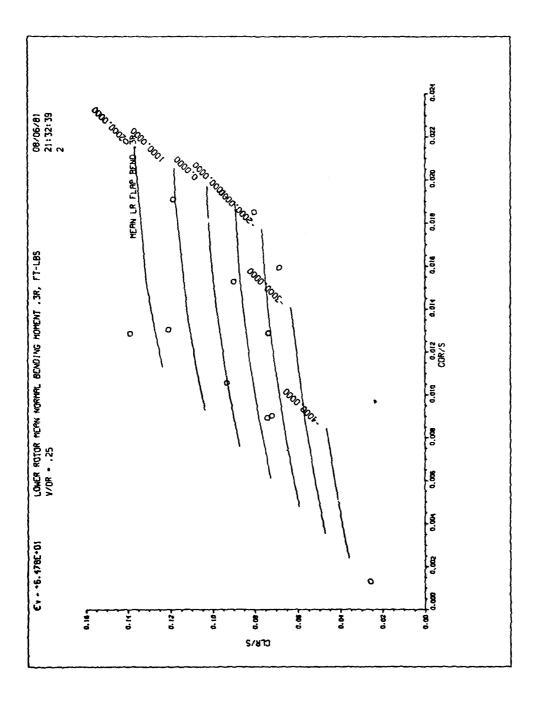


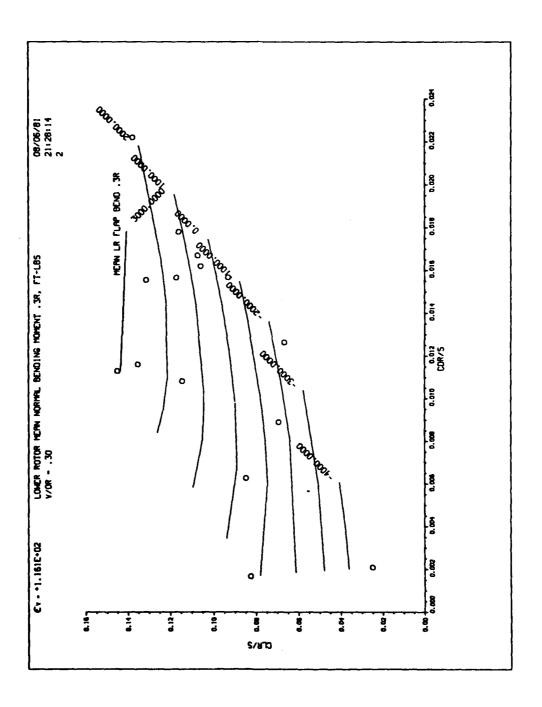


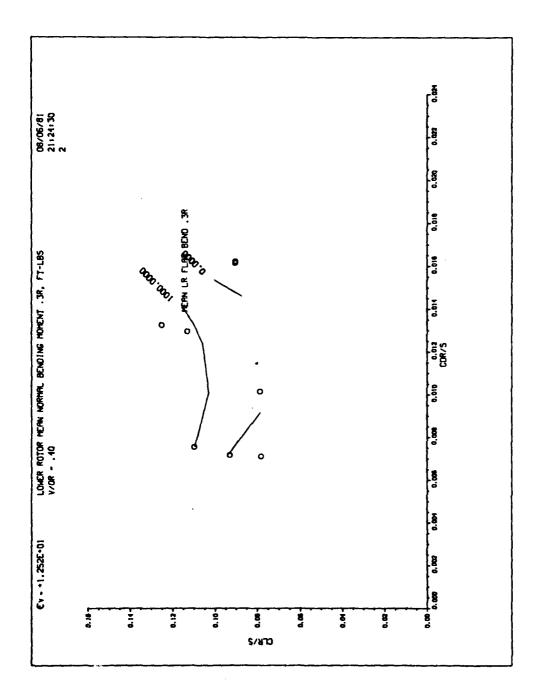


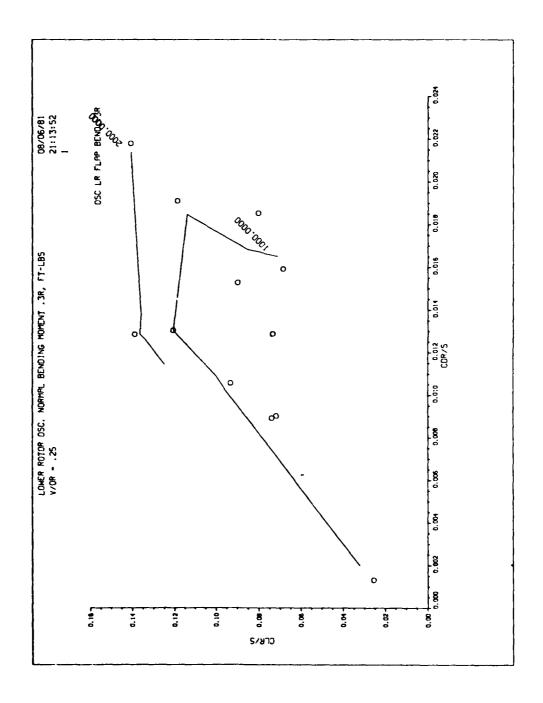


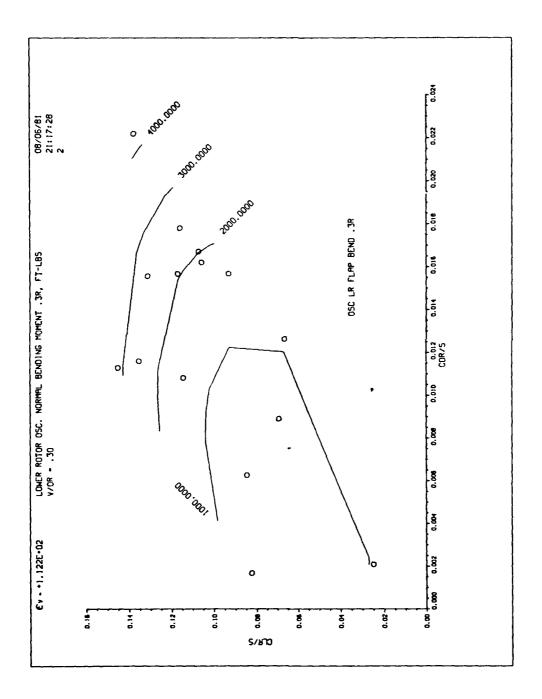


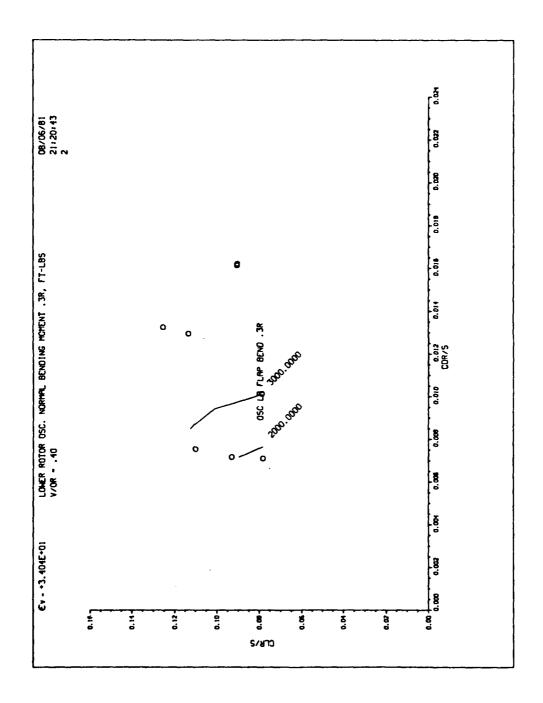


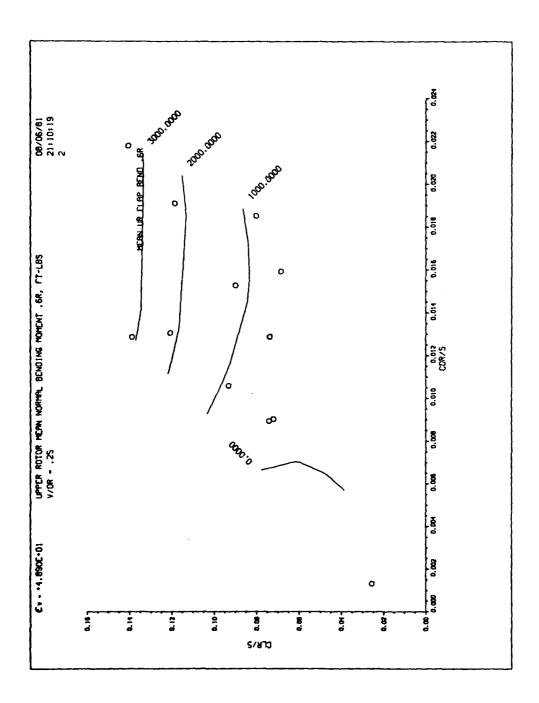




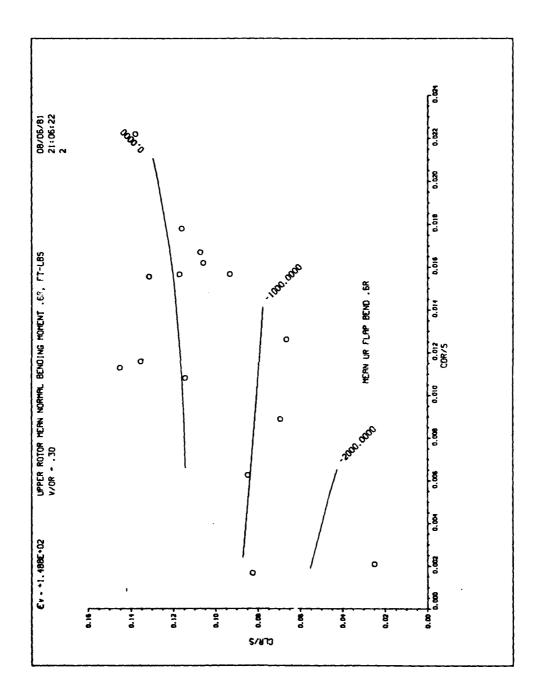


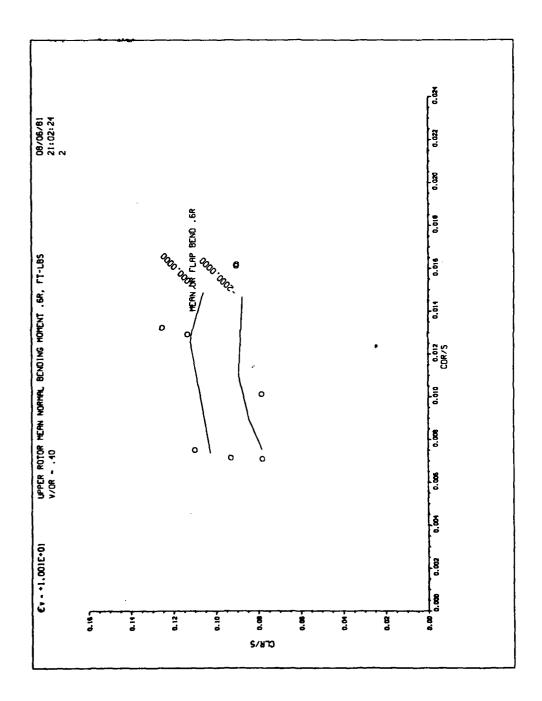




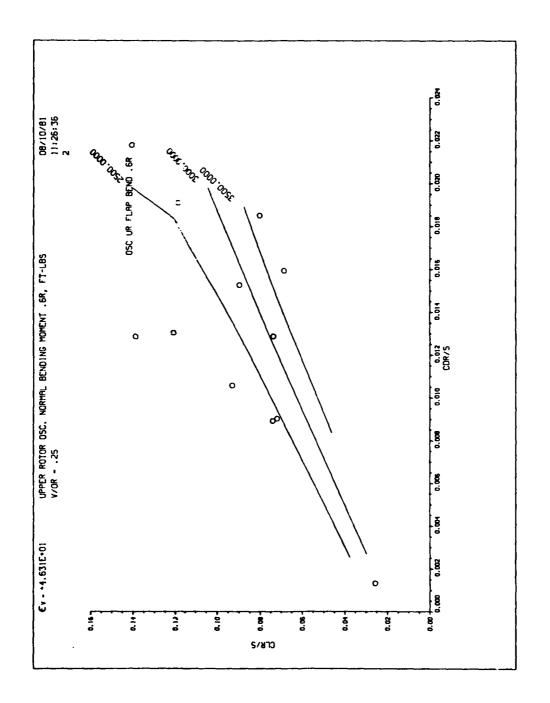


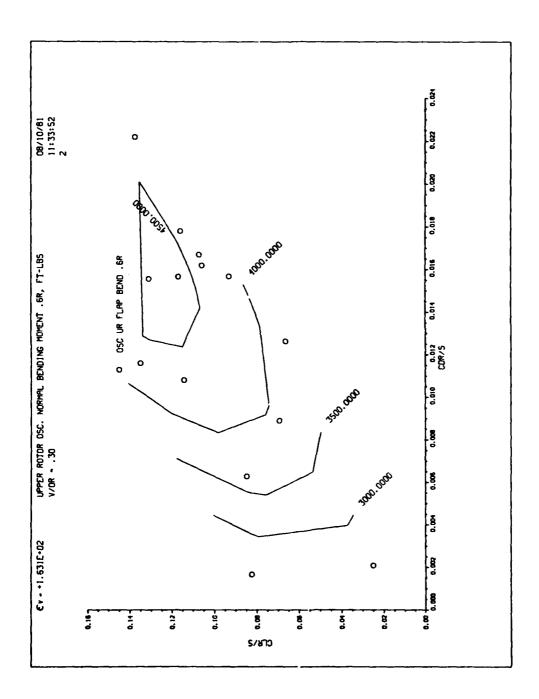
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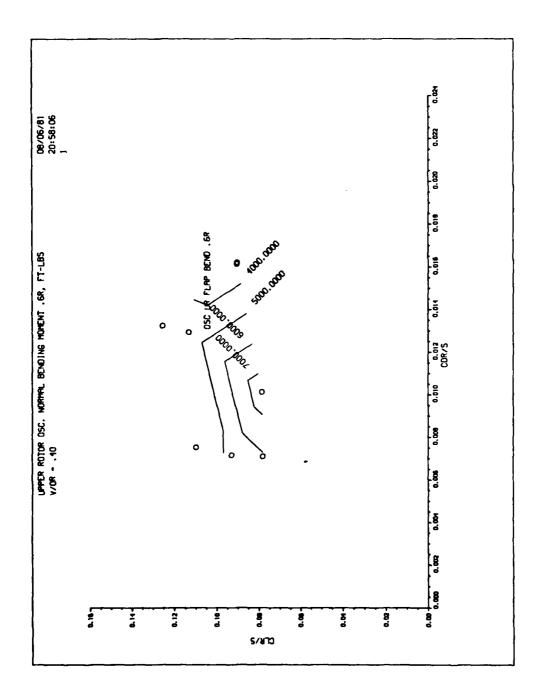


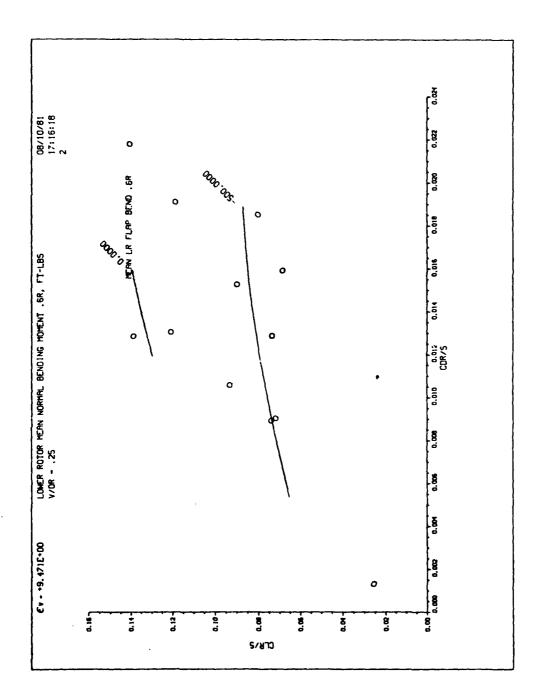


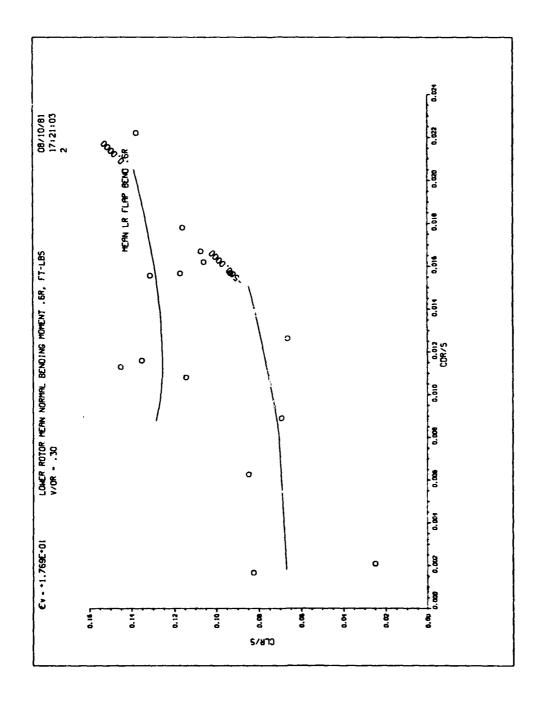
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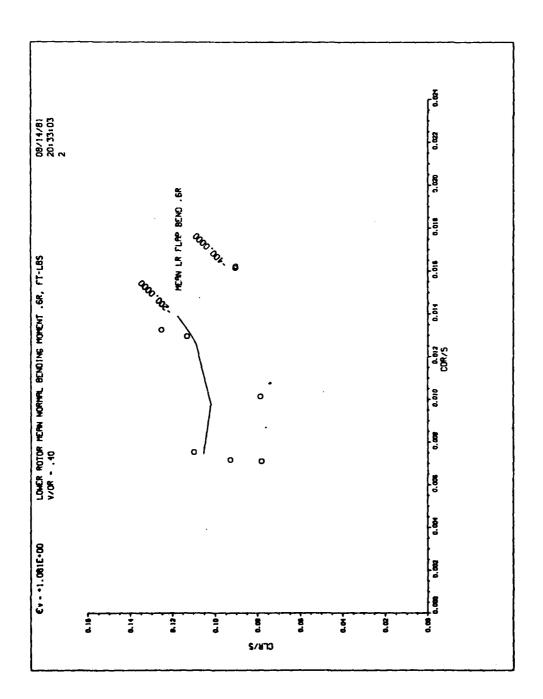


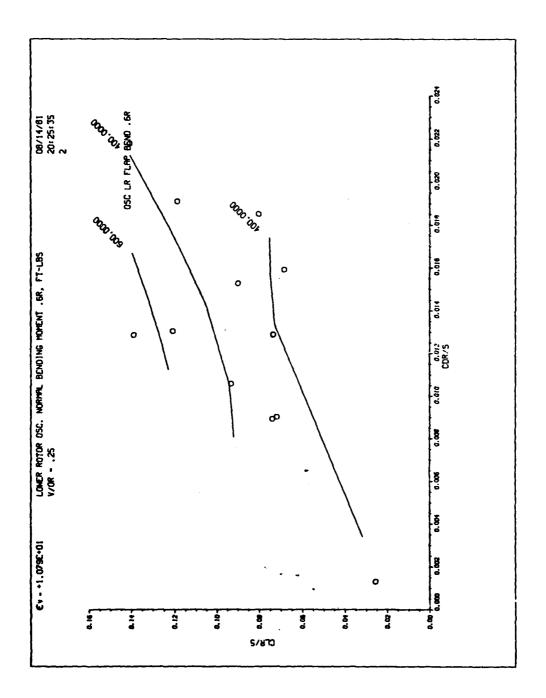


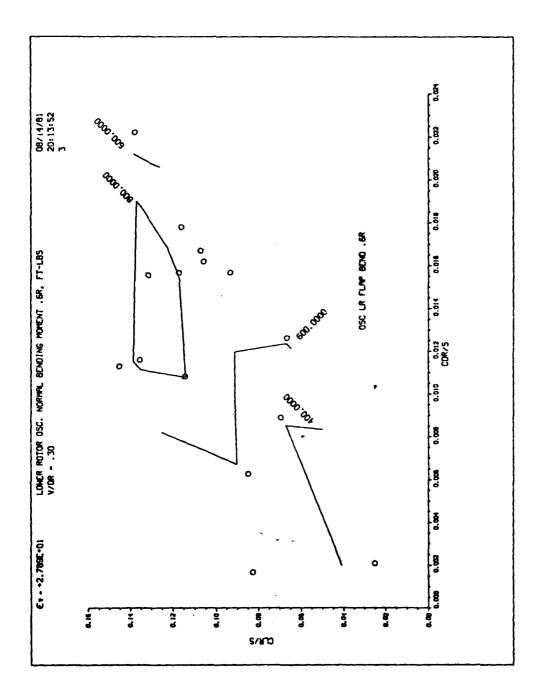


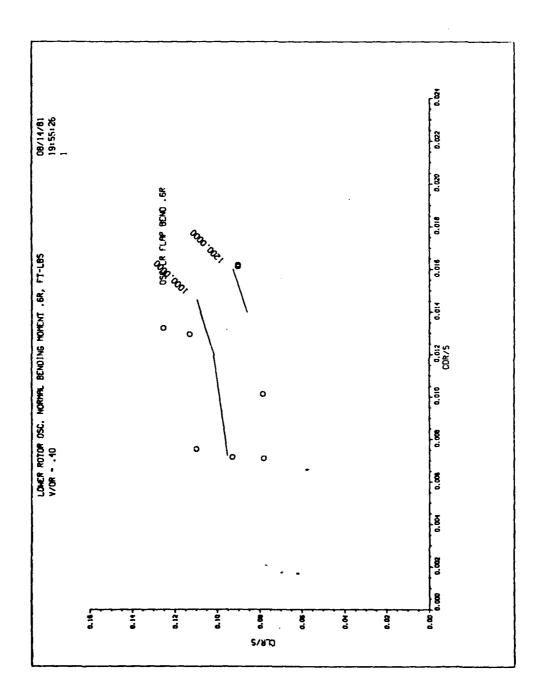


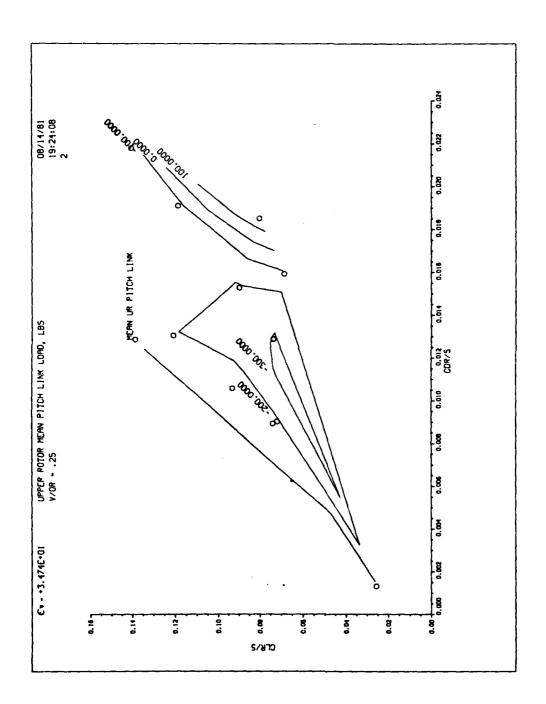


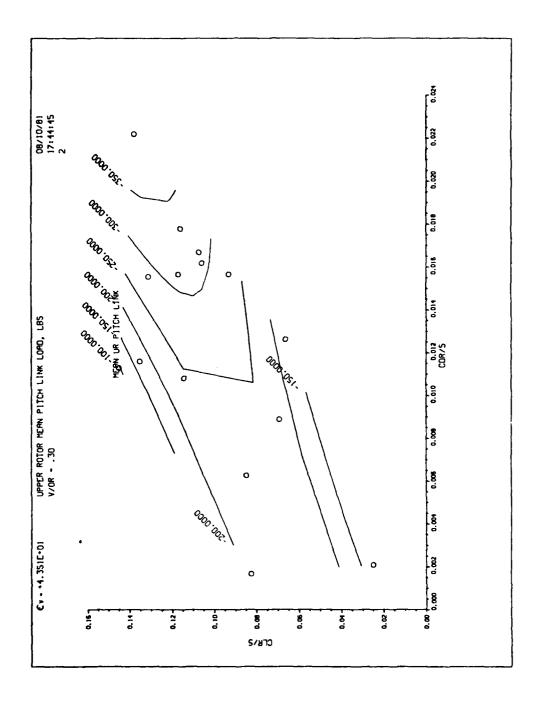


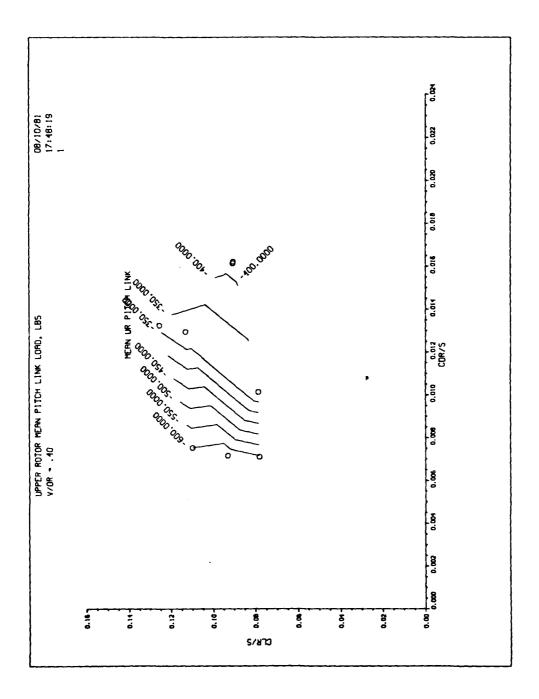


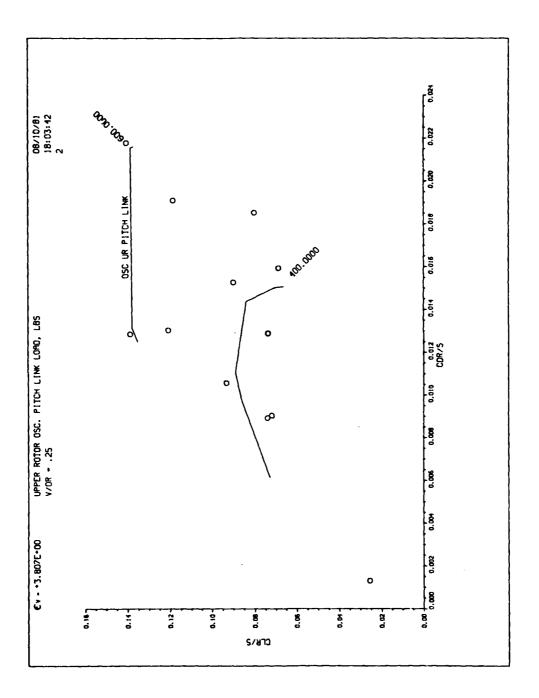


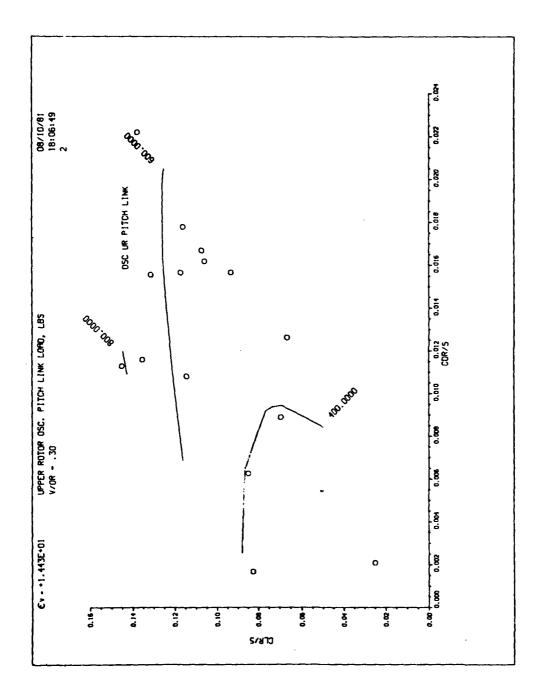


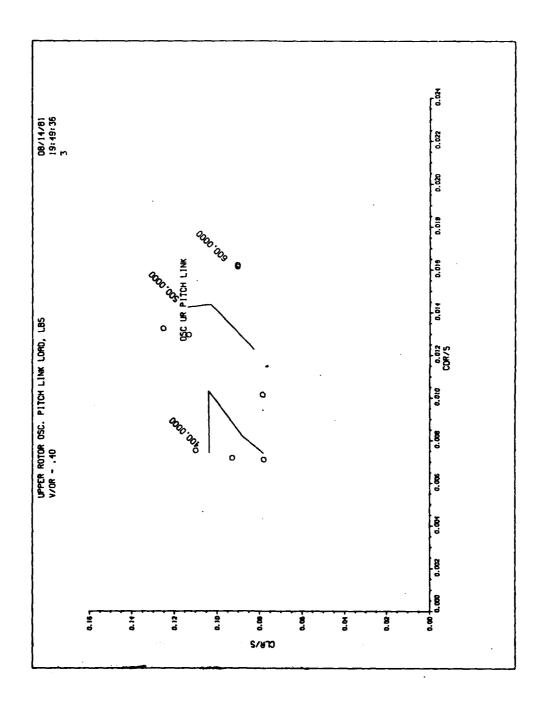


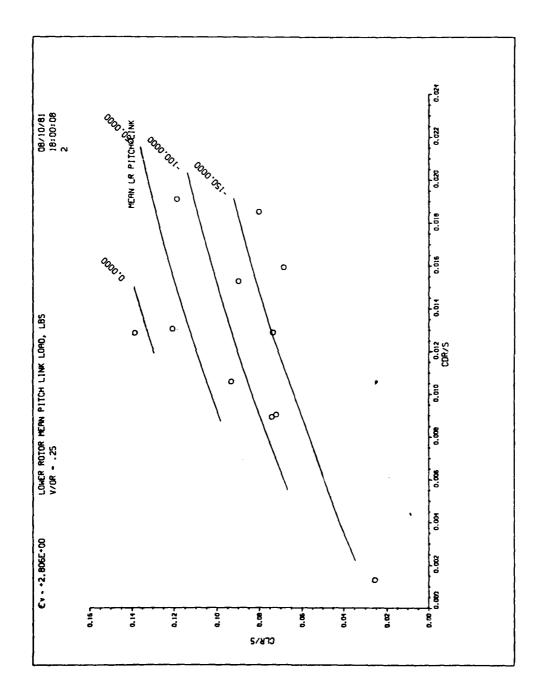




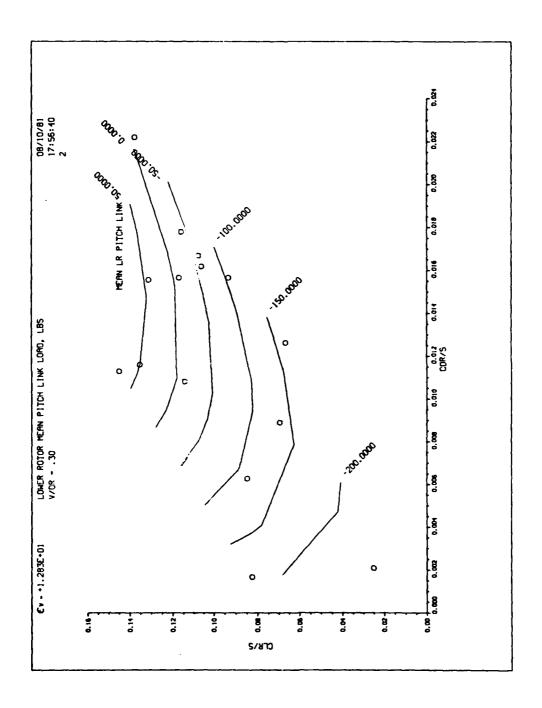


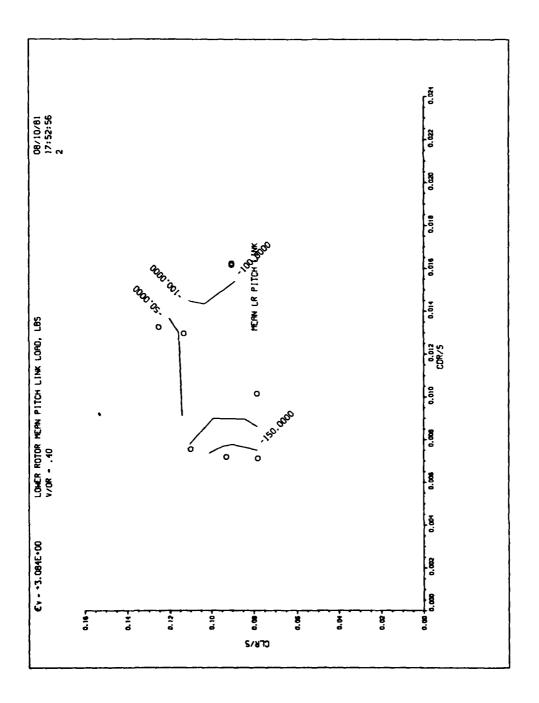


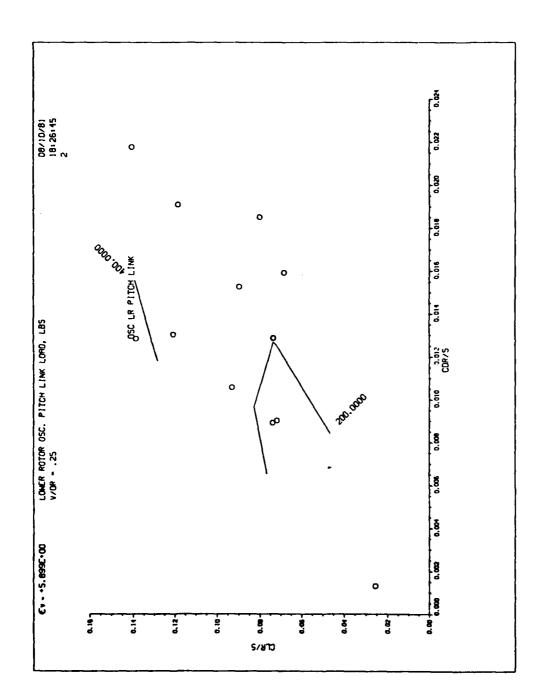


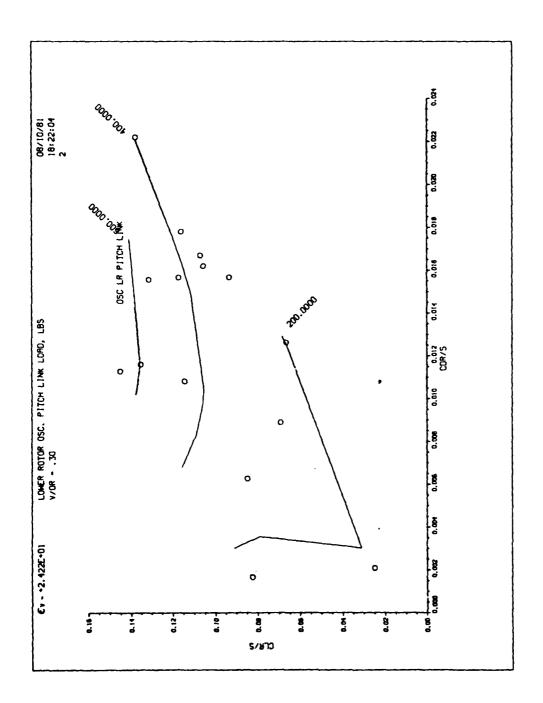


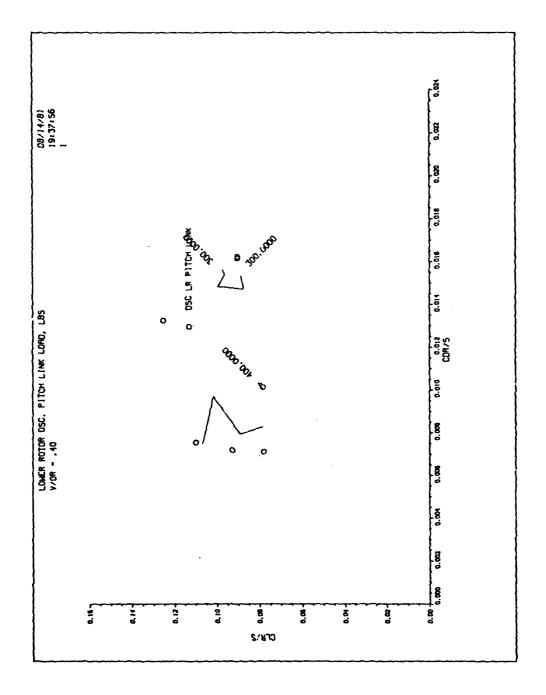
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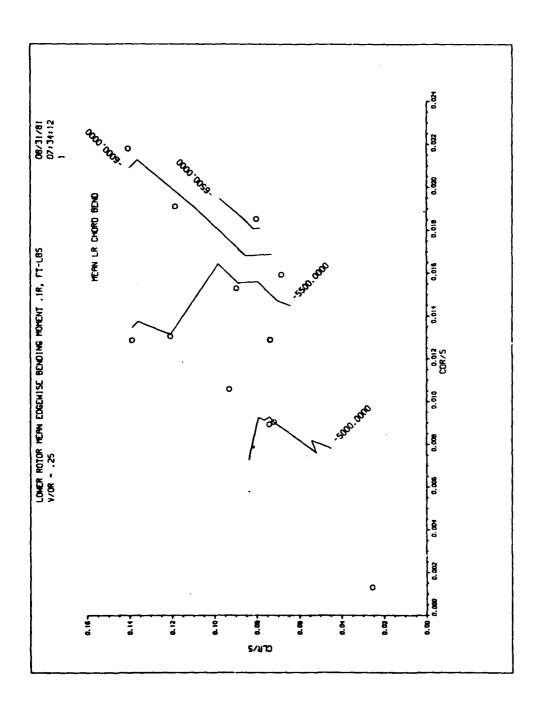


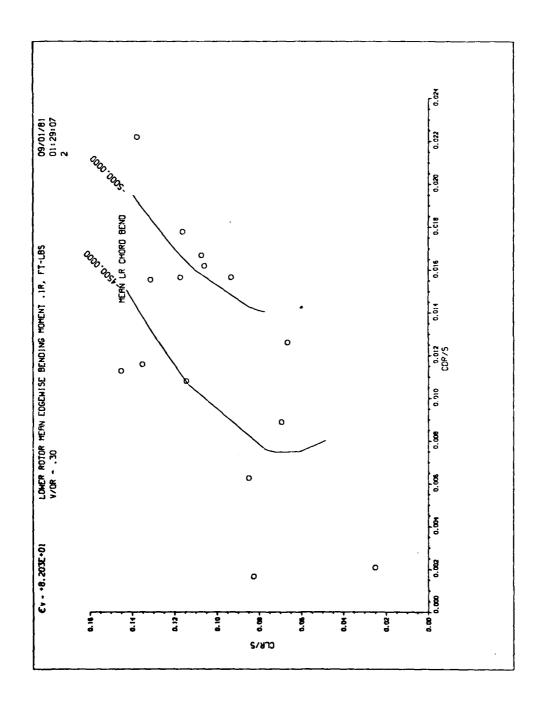


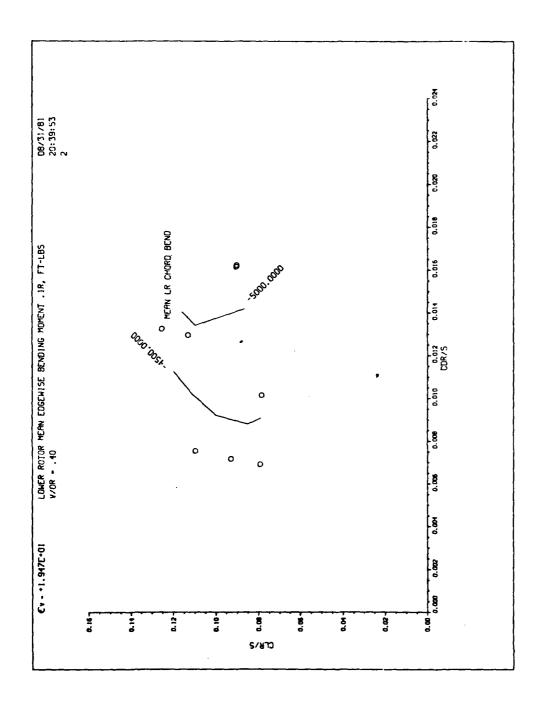




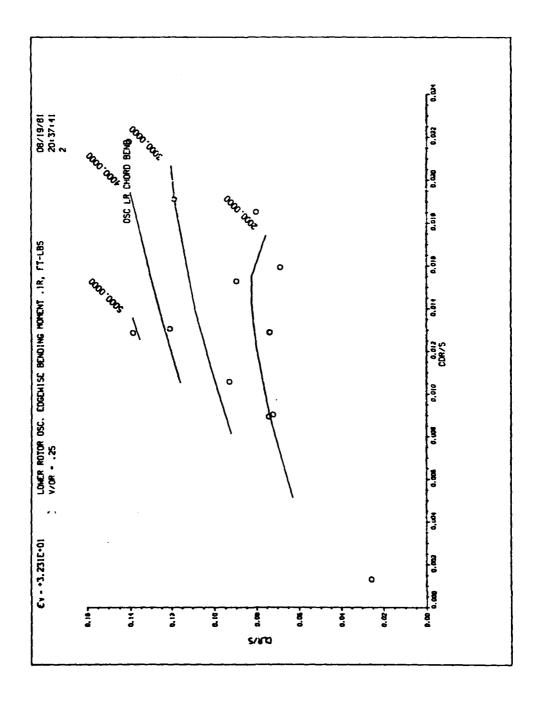


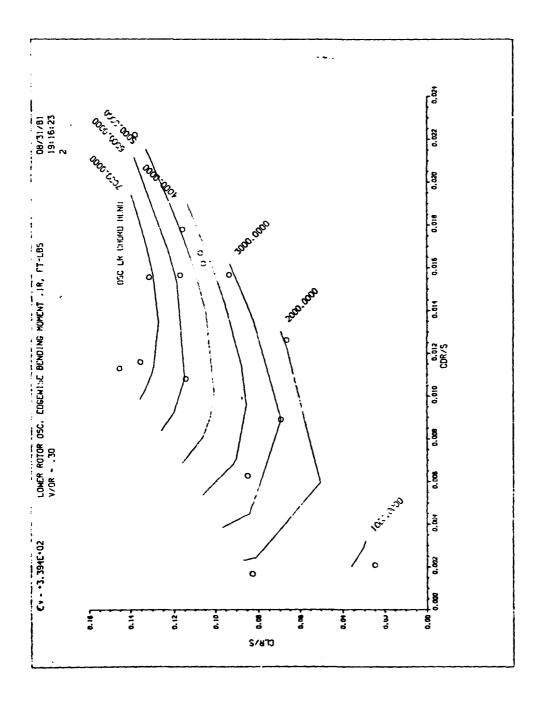




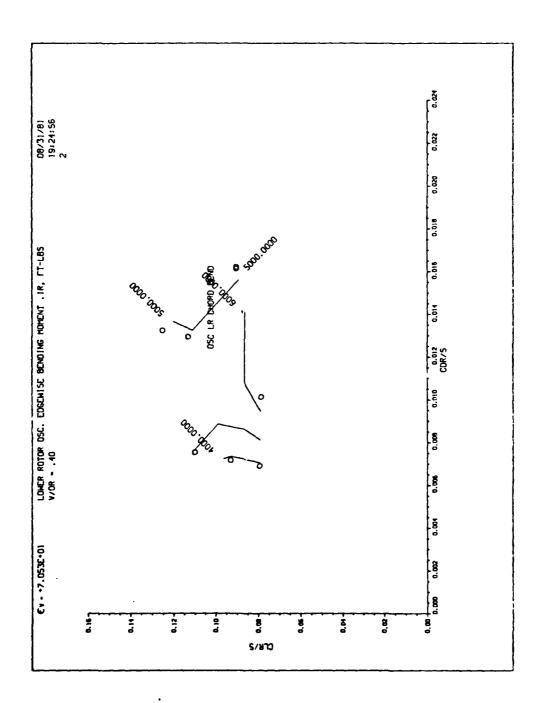


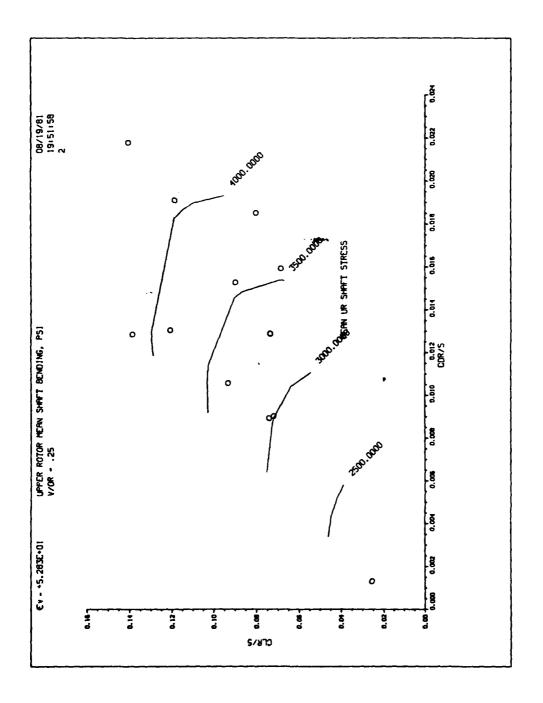
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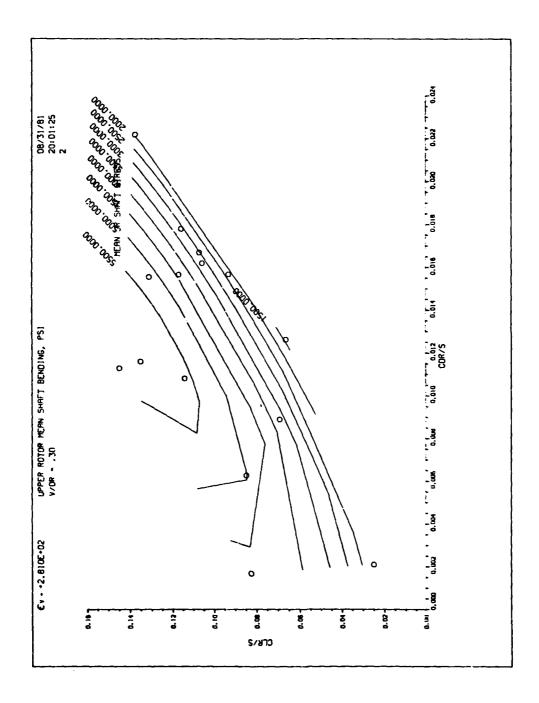


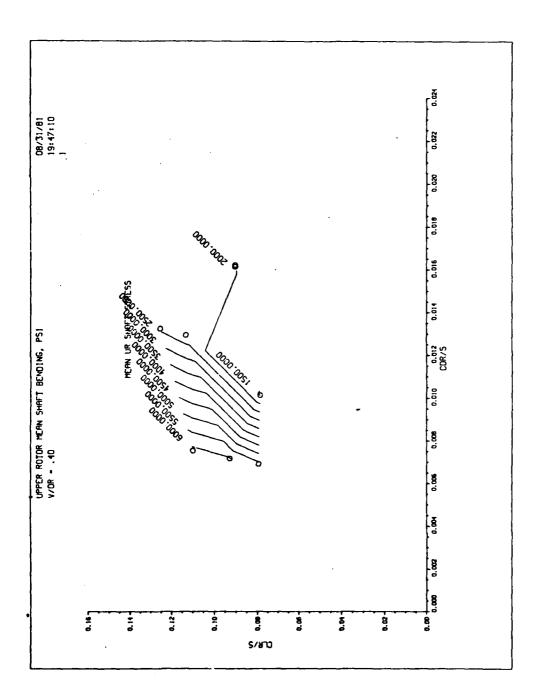


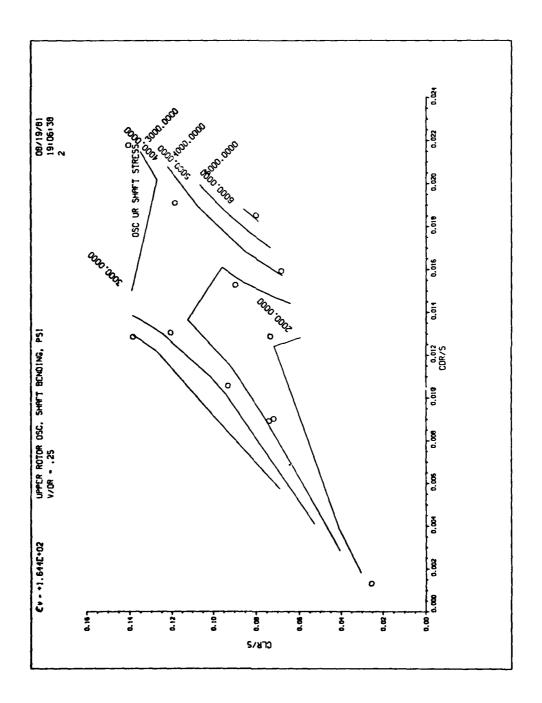
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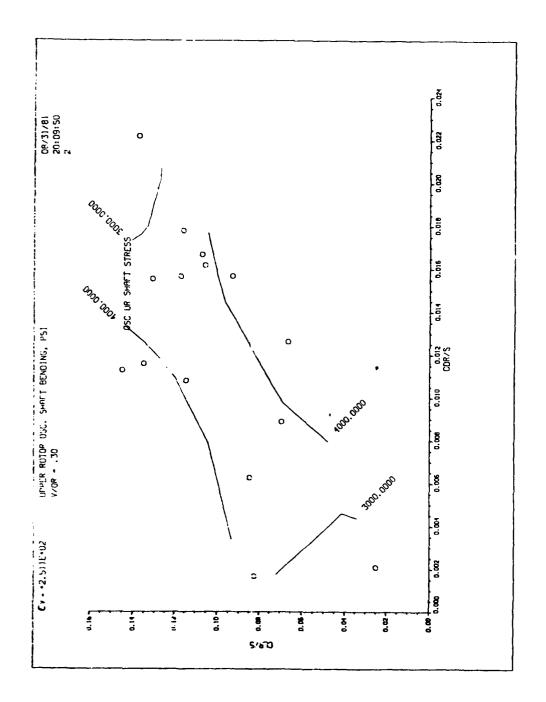


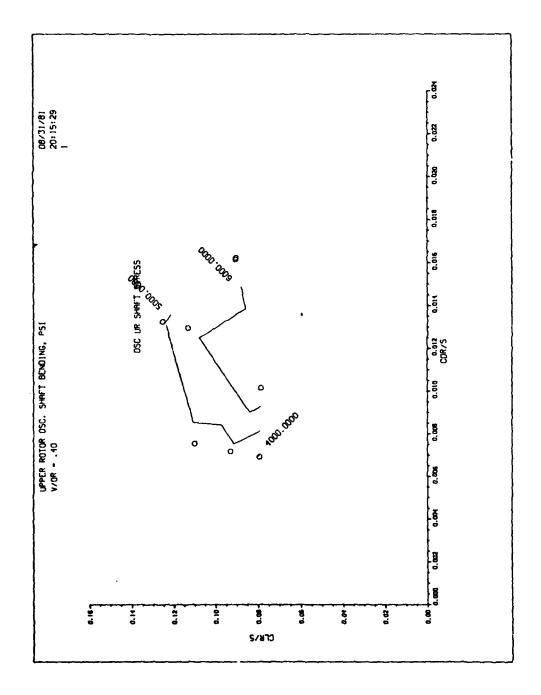


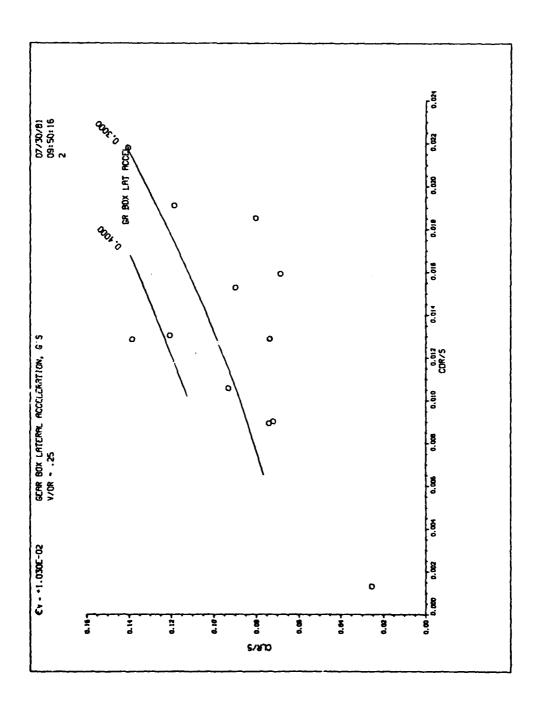




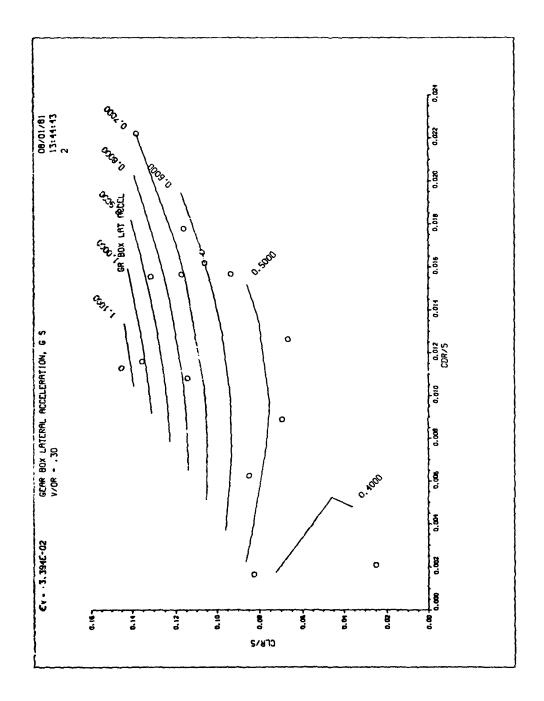


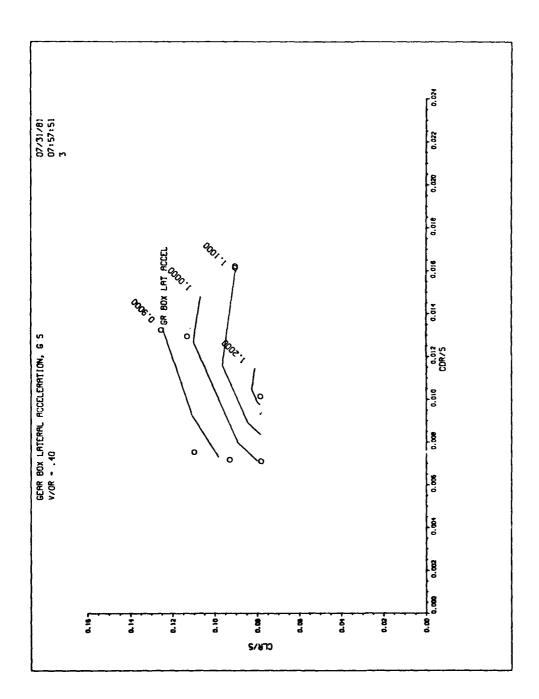


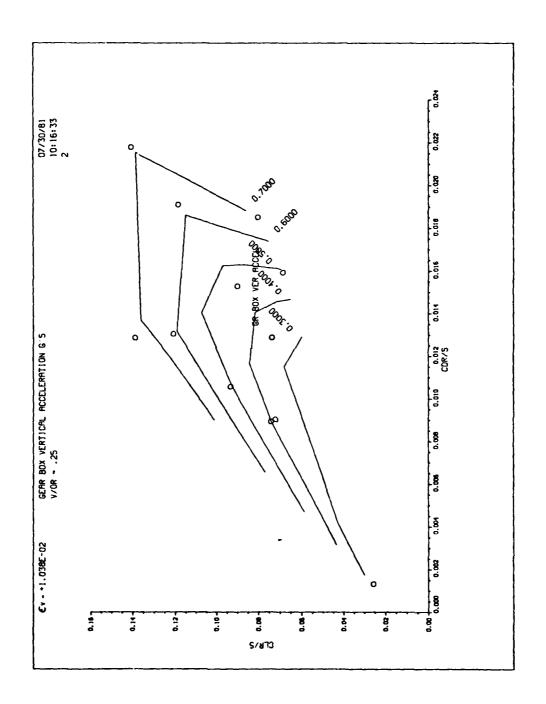


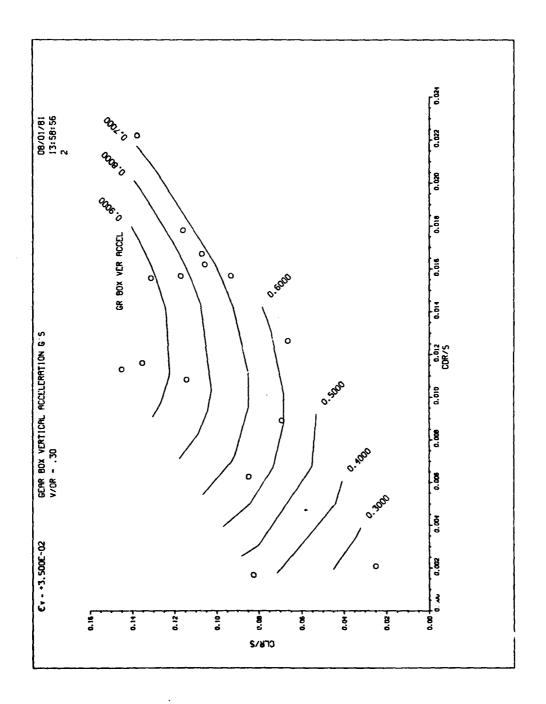


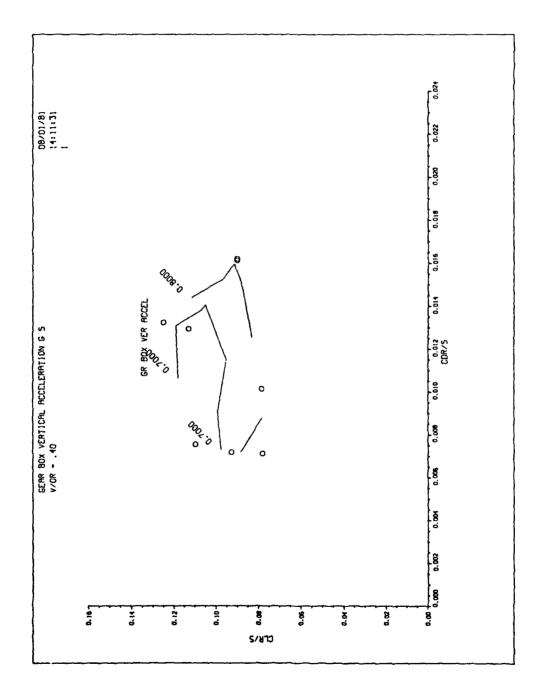
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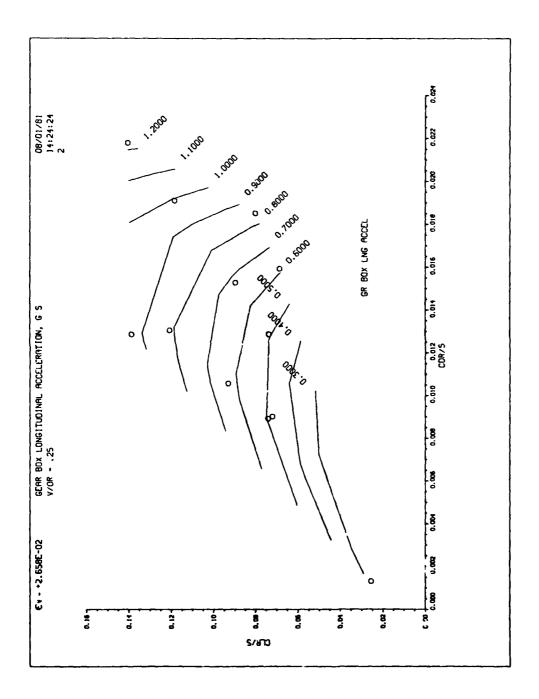


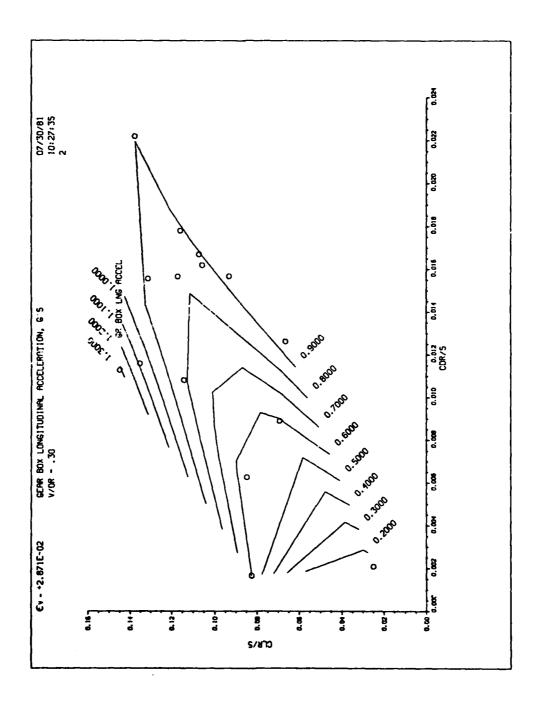




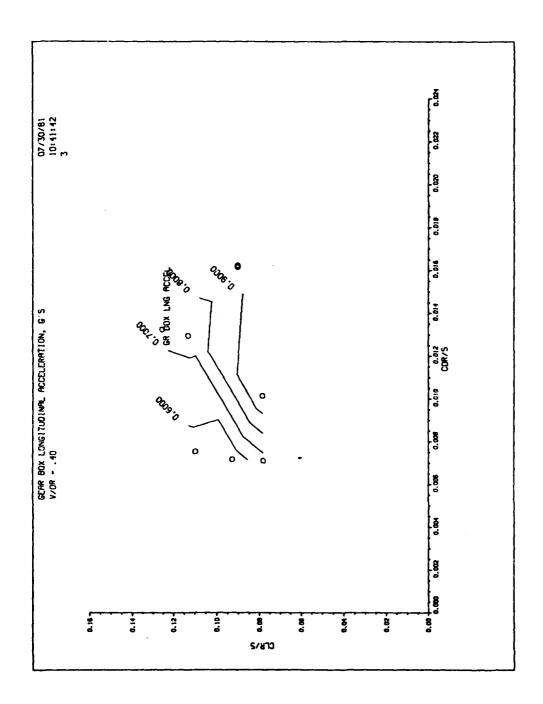








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16. Abstract				
A test of a full-scale XH-59A Advancing Blade Concept Helicopter was conducted in Ames Research Center's 40- by 80-Foot Wind Tunnel. The helicopter was tested with the rotor on and off, rotor hub fairings on and off, inter-rotor shaft fairing on and off, rotor instrumentation module on and off, and auxiliary propulsion thrust on and off. The investigation was accomplished over an advance ratio range of 0.25 and 0.45 with the rotor on and from 60 to 180 knots with the rotor off. This report presents data on aerodynamic forces and moments, rotor loads, rotor control positions and vibration for the XH-59A as well as the aerodynamic performance of the isolated rotor.				
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